

COMPUTER BLAST DESIGN FOR LARGE DIAMETER BLASTHOLE STOPES UNDERGROUND - FINAL REPORT -

PREPARED FOR

**DEPARTMENT OF
SUPPLY AND SERVICES CANADA**

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1.0 SUMMARY

This report presents a computer program prepared by Mining Resource Engineering Limited which is capable of designing underground blasts using large diameter blastholes. The program produces designs for either large diameter blasthole bench blasting or for the vertical crater retreat method. In particular, the program takes into account the blasthole wander that has proved a significant problem in these types of blast design.

The input to the program includes three dimensional descriptions of the blasthole locations in the blast, geological data such as cratering results, powder factor requirements, etc. for different material types, standard explosives data on strength, density, etc. and information on points in the mine requiring protection from excessive vibrations.

The output gives horizontal and/or vertical projections of the blastholes, plans and cross-sections of the blast and complete loading instructions for the blaster.

1.0 SOMMAIRE

Ce rapport présente un programme d'ordinateur capable de faire le design d'explosions souterraines utilisant des trous d'explosifs de grand diamètre. Le programme a été préparé par Mining Resource Engineering Limited. Il produit des designs d'explosion soit pour des trous d'explosifs de grand diamètre, pour des explosions par étage (bench blasting) ou pour la méthode de cratère refoulé verticalement (vertical crater retreat). En particulier le programme tient compte de la divagation des trous d'explosifs, ce qui s'est avéré un problème important dans le design de ces types d'explosions.

L'information requise par le programme comprend: une description tridimensionnelle de la position des trous d'explosifs, l'information géologique telle que les résultats sur la formation des cratères, la valeur du facteur poudre, etc. pour les différents types de matériau, l'information habituelle sur la force des explosifs, la densité, etc. et l'information sur les endroits dans la mine qui ne doivent pas être exposés à des vibrations excessives.

Le rapport du programme donne des projections horizontales et/ou verticales des trous d'explosifs, les plans et vues en coupe de l'explosion ainsi que les instructions de charge complètes pour le dynamiteur.

2.0 INTRODUCTION

The use of large diameter blastholes is becoming more common in underground operations to allow mines to take advantage of the economy of increased blast size and corresponding reduced operational delays and disruptions. To improve economy, high stope heights are more frequently being blasted. Following the initial development blasts, produced using slots or circular openings and/or undercutting, two main primary blasting methods are used, these being crater retreat and regular bench blasting. The crater retreat method utilizes single cratering charges near the bottom of each hole whereas the bench blast uses the entire hole for the blast usually loaded with multiple decks.

As bench heights, and thus hole depths, become larger, the degree of hole wander increases markedly. With depths of up to 30 m, hole sizes of from 125mm to 150mm exhibit some deviation, although not to such an extent that blast design is seriously affected. With increasing depth, however, hole wander becomes more significant. The result is erratic burdens and spacings being produced at the base of the blast. In some areas of the blast, where holes have converged, the blast may be greatly overloaded whereas elsewhere, where holes have diverged, burdens may be so large as to be nearly unmovable, or certainly of a size that would produce very poor fragmentation.

There is even the possibility of decks being fired out of sequence when holes converge excessively.

There are a number of instruments available which are already being used to determine the actual direction of the blastholes giving inclination and orientation with depth. These include the Gyroprobe produced by Humphries, San Diego, Ca. and the Abem Reflex Fotobar produced by Atlas Copco, Sweden. The typical accuracy of these units is of the order of 0.2 m per 100m of hole depth.

At present these measuring instruments typically have digital readout systems, but it will be a relatively simple process to provide direct computer input for the hole data, possibly by recording on magnetic tape.

Figure 1 shows a composite plan view of a blasthole layout for an actual bench blast illustrating both the locations of the blasthole collars and the blasthole toes. The hole wander is represented by the parallel dashed lines joining the top and bottom of the hole. As can be seen, there is generally no overall trend for hole direction from one hole to the next. The major contributing factors to the hole deviation are poor hole collaring, the drill and drilling techniques as well as the geological conditions.

Figure 2 highlights the result of the random hole directions. This figure presents a plan view of the bottom of the blastholes from Figure 1. The erratic spacings and burdens clearly indicate the difficulty in charge deck size determination and delay time selection.

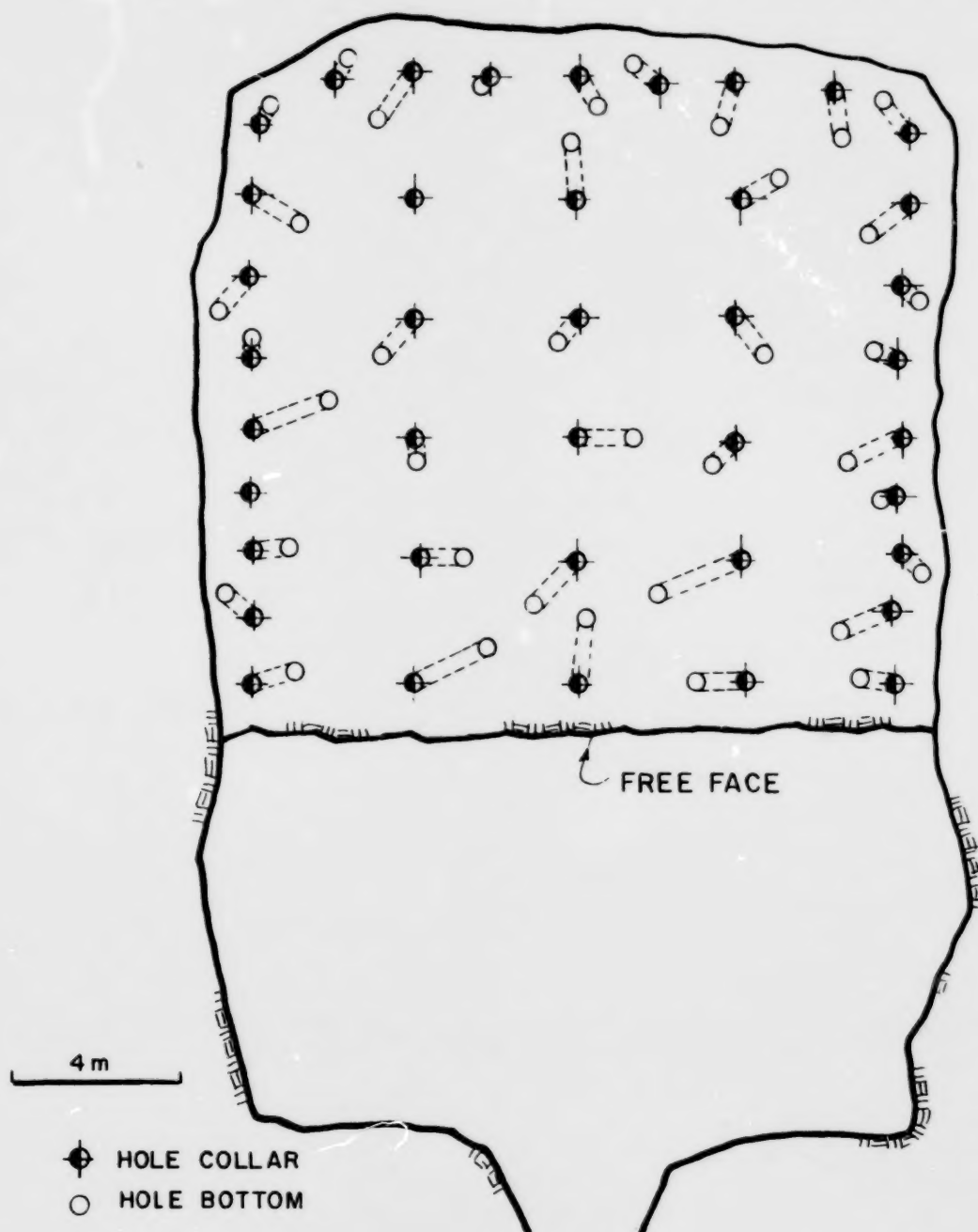


FIGURE 1 : COMPOSITE PLAN VIEW OF BLASTHOLE LAYOUT .

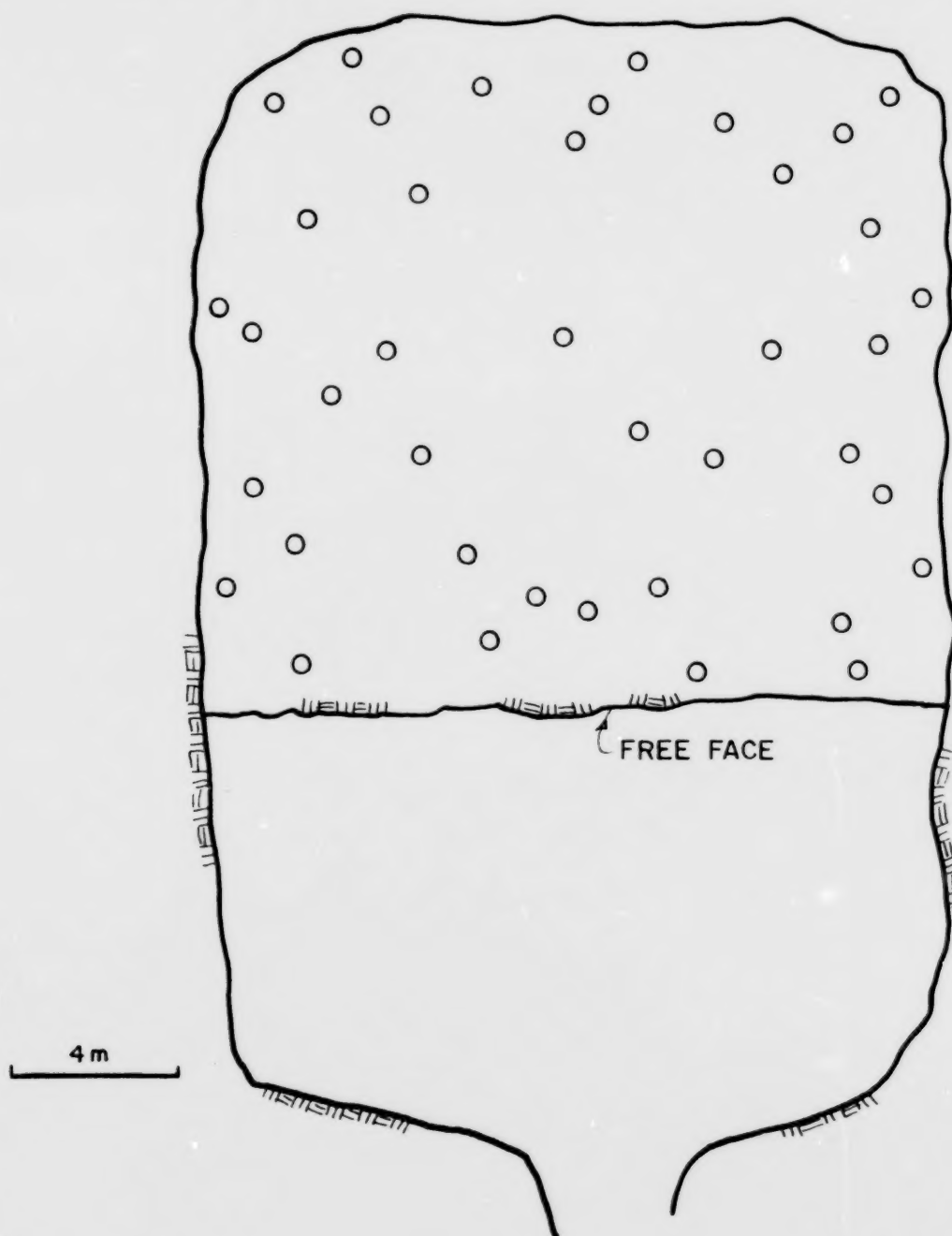


FIGURE 2 : PLAN VIEW OF THE LOCATIONS OF THE BOTTOM OF THE BLASTHOLES FROM FIGURE 1.

2.1 Blast Design Approach

A computer program has been written which will first produce a graphical model of the entire blast. The model is capable of including all of the relevant rock structure and geology. The program then calculates the optimum blast design for the particular hole layout and hole deviations. Computer output is both graphical, showing blast plans and sections with charge locations, and digital to present charge explosive type, size, delay period, etc.

One of the first advantages of the computer design approach is the speed at which the blast design can be prepared. The recorded blasthole data can be fed into the program during the drilling operation, the result being that in the extreme cases when extra holes are required, this is known almost immediately. The extra holes can then be drilled prior to the drill rig leaving the area, which therefore gets away from the costly business of returning a drill to the blast at a later time.

The use of the hole deviation measuring instrument is particularly useful for mines not operating with an undercut. At present these mines have virtually no knowledge of the actual explosive distribution at the base of their blasts.

The computer program will first design the development blasts for operations utilizing a benching technique. This blast can be designed to a circular opening or a rectangular raise with the charge weight being related to the standoff

distance which will also be related to the diameter or size of the opening. This is similar to the design to open up a drift round.

The computer program designs the primary blasts considering such factors as:

- (1) The maximum burden that can be broken for the given material and explosive type.
- (2) The maximum size of explosive deck which is dictated by the vibration experienced by pillars, etc.
- (3) The rock strength, work index, explosive consumption requirements given the required fragmentation desired and the preferred direction of shooting versus rock structure, etc.
- (4) Short burdens are checked for the requirement of extra decking.
- (5) Wall hole design is incorporated to produce acceptable stope sides.
- (6) Minimum deck separation distances are calculated.
- (7) A simulation of the blast firing is programmed to select interhole delays as well as interdeck delays. Figure 3 shows a three dimensional view of a typical blast. Blasthole wander can be seen to cause quite varying burdens near the bottom of the blastholes. Figure 4 shows the typical blasting sequence presently being used where one row is fired and only one hole is detonated at any one time. In this case the bottom deck of a hole would first be initiated, followed by the second, third, fourth deck, etc. and only when the entire hole has been fired would the bottom deck on the next hole be shot. This initiation method has the problem that long delays

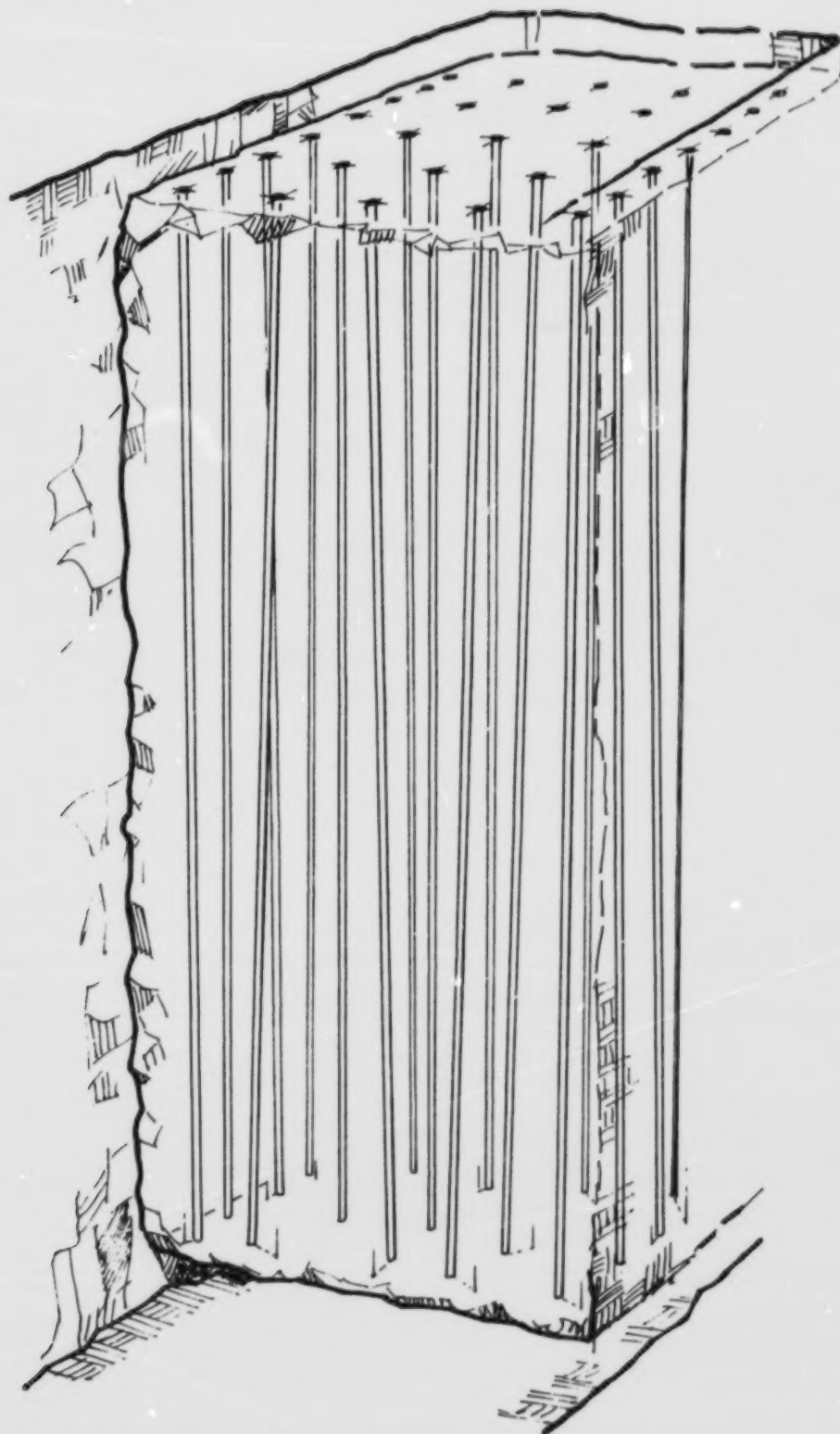


FIGURE 3: THREE DIMENSIONAL VIEW OF A TYPICAL BLAST.

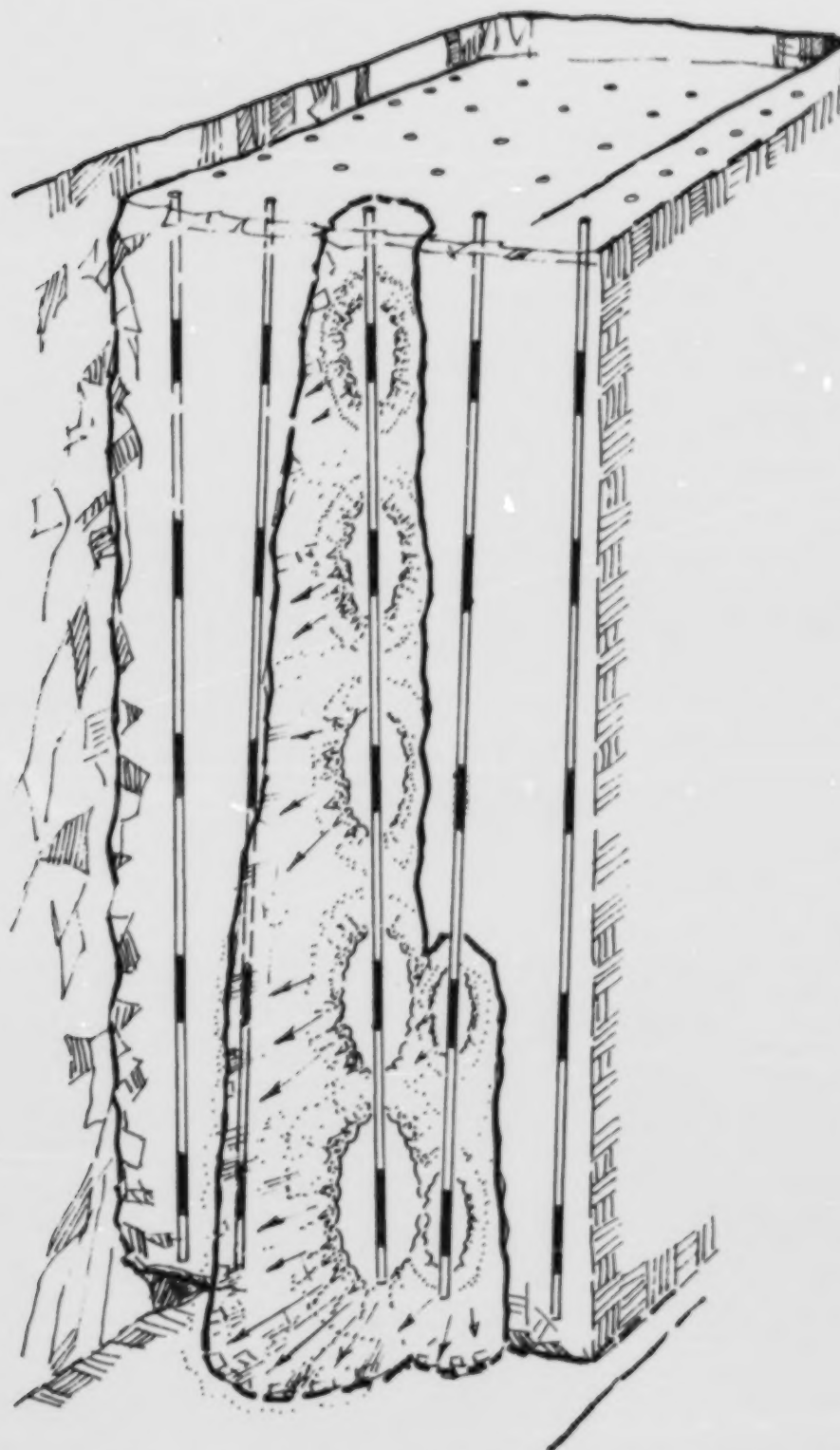


FIGURE 4 : THREE DIMENSIONAL VIEW OF A TYPICAL BLAST AS PRESENTLY DELAYED SHOWING EACH HOLE COMPLETELY FIRED PRIOR TO SUBSEQUENT HOLE FIRINGS.

may exist between adjacent explosive decks.

Figure 5 presents an alternative approach for a single row blast. After firing two decks in the initial cut hole the next three delay periods would fire the third deck in the cut hole followed by the bottom decks in each adjacent hole. This approach is used in the design program.

In open pit blasting it is frequently found that single row blasting gives poor fragmentation. It is therefore the approach that blasting schemes are developed to safely fire multiple row shots for this type of underground blasting.

(8) The design is performed to prevent overbreak at both the top and bottom of the shot.

(9) For crater retreat blasting, the charge sizes and locations are designed, using cratering curves, relative to the blasthole spacings. The appropriate charge delays are also selected.

This type of computer blast design program should prove to be an invaluable tool for the blasting engineer to first quickly determine if the blast has been adequately drilled off and then to give the complete layout of deck charge size, location and delay period.

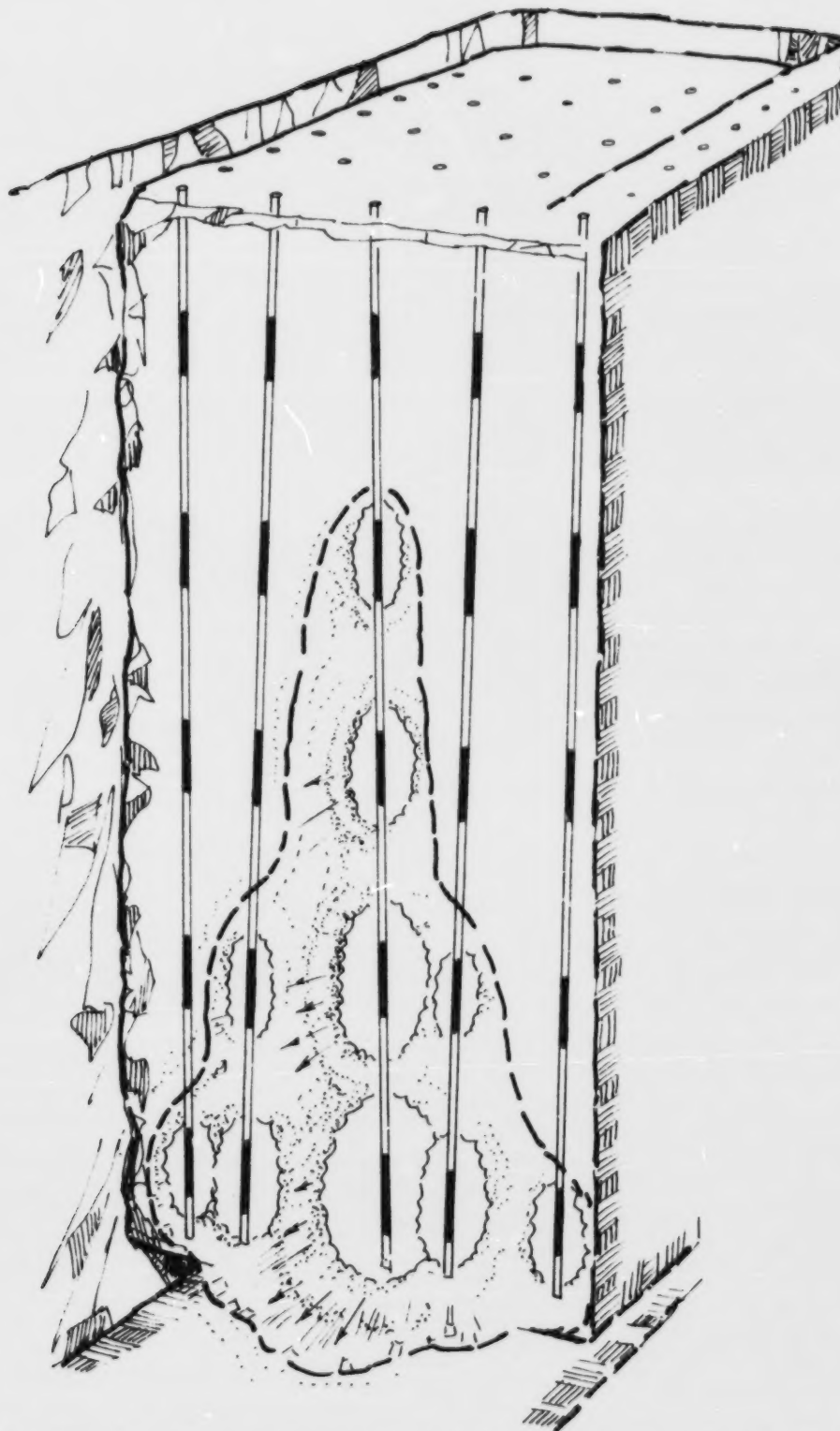


FIGURE 5: THREE DIMENSIONAL VIEW OF A BLAST SHOWING MORE THAN ONE HOLE FIRING AT ANY ONE TIME.

3.0 INSTRUMENTATION

Along with the current instrumentation presently being used in the field to measure and describe the position of the blasthole within the blast itself, the writing of this program identified the need for instrumentation that will also describe the burden on front row holes in the bench blasting operation.

The program, as presented, accepts two forms of input as regards front row burdens. These may be inputted from a specific measuring instrument, should one be developed. Alternatively a constant burden may be inputted in the form of a plane face, this being the one presented in this report.

This section describes the reasons for the requirement of a burden measuring instrument, the types of technology that may be employed in its development, and a recommendation as to the best approach for the instruments development in the opinion of the authors.

3.1 Background to the Instrumentation Requirement

This computerized approach to blast design will be considerably enhanced if all the major factors that influence the efficiency of a blast can be taken into account. One such major factor is the burden associated with the front row of drill holes immediately adjacent to the free face, as commonly only one row of blastholes may be fired at one time. Even if this is not the case, it is information that, if known, can greatly improve the blast design process. Owing to

the blasthole deviations and an uneven free face (often possessing overhangs), front-row burden values can vary significantly in a complex manner at various depths within the same hole and/or between adjacent holes. Complex variability can easily be accommodated using these computer design techniques provided that the required spatial relationships between hole location and topography of the free face are known. The acquisition of such data is, however, problematic unless a relatively rapid geophysical technique can be developed in order to suit this novel application. This section details an investigation to assess the viability of different geophysical techniques for providing data on front-row burdens in a compatible form that can be incorporated into the computer blast-design program that is now developed.

3.2 Benefits of the Instrumentation

Failure to adequately determine front-row burdens has obvious economic ramifications. Overestimations can lead to the uneconomic use of excessive explosive charge weights whereas underestimations are likely to cause poor fragmentation with a consequent need for subsequent blasting. It is clear that such potential errors serve to detract considerably from the major cost-saving advantage offered by the computerized approach to blast design.

3.3 Overview of Selected Geophysical Techniques

Four geophysical techniques were evaluated in order to assess their potential usefulness for determining front-row burdens. These techniques are:

- (i) seismic reflection
- (ii) radar reflection
- (iii) gravity, and
- (iv) acoustic reflection.

Owing to the likelihood of inaccessible mining faces (upon which targets for conventional surveying technique may not be placed), only borehole tools were considered suitable. Application of borehole seismic, radar and acoustic techniques would entail measuring the return travel time of an impulse signal which is generated in the drill hole and reflected at the rock/air interface. The gravity method, on the other hand, would involve the measurement of small differences in gravity caused by the irregular relief of the free face.

Relatively low frequency conventional seismic reflection is discounted owing to the very short travel times that are anticipated. For a distance of 4 to 8 metres between the blasthole and free face and, using an assumed average velocity of 6000 metres/sec, a two-way travel time of less than 3 millisecs is realized. Travel times of this small order cannot be resolved using current borehole seismic equipment.

Under conditions where conductive ore (of the order of 1 ohm-m resistivity) is being mined , use of the radar technique is inadvisable. Such conductive ores (ie. nickel ores) are essentially non-transparent to radar electromagnetic frequencies of an order of 100 mhz, penetration being less than approximately 0.6 metres.

Measurement precision of present borehole gravity tools is only ± 1 mgel. This order of precision is not sufficient to give an accurate picture of the 'irregularity' of the mine face. More over, localized changes in density of the ore close to the blasthole are likely to mask any variations that may be due to changes in relief of the mining face.

The acoustic technique is the most promising of the four geophysical techniques evaluated and does not suffer the limitations of the other three. Moreover, within recent years it has been used successfully in inter-borehole applications (eg. Wong et al, 1983; Aki et al, 1984, McCann et al, 1975) that are closely related to our proposed burden determination investigation.

It is therefore recommended that this be the approach taken in the development of a suitable burden measuring device to be used in conjunction with the computer blast design program as described in this report.

4.0 COMPUTER DESIGN THEORY AND COMPUTER EQUIPMENT

4.1 Theory Used

For the prediction of the craters which are formed because of the detonation of a charge, Livingston's crater theory was used, (Bauer, 1961 & Livingston, 1973). The basic points of this theory are given in the following. When an explosive charge of constant weight and shape is placed at different distances from a flat free face and detonated, the amount of material excavated changes with the depth of burial of the charge.

At deep depths the explosion is contained and all of the energy is used up in local crushing and seismic waves. As the depth of charge is reduced, surface slabbing is produced. Near the point where failure just starts, large pie-shaped fragments are formed in a massive material and the crater is quite shallow. As the depth of the charge is further reduced, the shape and depth of the crater change as does the degree of fragmentation. In addition to the tensile slabs, a series of radial cracks run out from the borehole. These are due to failures starting near the explosion and which run up through the material. There is also a series of concentric circular cracks with the borehole as center. The crater dimensions and the degree of fragmentation change continuously with the depth of burial of the charge. Associated with a certain degree of fragmentation there is also a certain level of noise and flyrock

associated with the shock. In addition as the depth of a given weight of charge is reduced, the quantity of material broken passes through a maximum and at this point the degree of fragmentation is good. It is this optimum point which is of interest for production shooting. At this point flyrock is minimized and there is little noise or airblast. That is there is a minimum of wasted energy. After obtaining the optimum point for a small weight of explosive, it is then necessary to scale up to a much larger charge weight and be able to predict the results.

The following parameters are of major importance to the theory:

(a) Depth of burial of the charge, (d_c). This is the distance from the centre of the charge to the free surface. The depth at which the surface failure just starts is called the critical depth of burial (N).

(b) Strain energy factor, (E). Livingston found that the critical depth of burial is proportional to the one-third power of the charge weight ($W^{1/3}$). The constant of proportionality (E) is called the strain energy factor. If the factor E is known the critical depth for any charge weight can be calculated.

$$\text{ie. } N \propto W^{1/3} \quad \text{and} \quad N = E W^{1/3} \dots\dots\dots (1)$$

(c) The depth ratio (Δ) is the ratio of the depth of burial to the critical depth for the same weight of charge.

$$\text{ie. } \Delta = d_c/N \quad \text{or} \quad d_c = \Delta N \dots\dots\dots (2)$$

Hence the general equation for charge depth of burial from equations (1) and (2) is given by:

$$d_c = \Delta N = \Delta E W^{1/3}$$

The depth ratio can be correlated to any scaled parameter of the crater such as the scaled crater depth or the scaled crater radius. The shape of the resulting curves is shown in Figure 6. This figure gives the scaled crater depth as a function of the depth ratio. It follows that the deepest crater results at a depth ratio of approximately 0.3. At this depth ratio the fragmentation is good and the use of the energy of the explosive optimum. It follows that for optimum blasting results the charge has to be such that the depth ratio is close to the optimum depth ratio.

4.2 Vibration Checks

In recent years the question of what constitutes a valid criterion for blasting damage has been discussed by a number of authors. Extensive statistical reviews have been made of published vibration data to determine which of the blast induced parameters, such as particle displacement, velocity or acceleration, best measures the damaging effects of a vibrational wave on a structure. The current conclusion is that damage can best be correlated with the peak particle velocity of the wave regardless of the direction of motion; longitudinal, vertical or transverse.

Historically several formulae have been developed to give peak particle velocity. The formula which is used in the programs is widely accepted and was developed by Devine, (Devine, 1966). According to this formula:

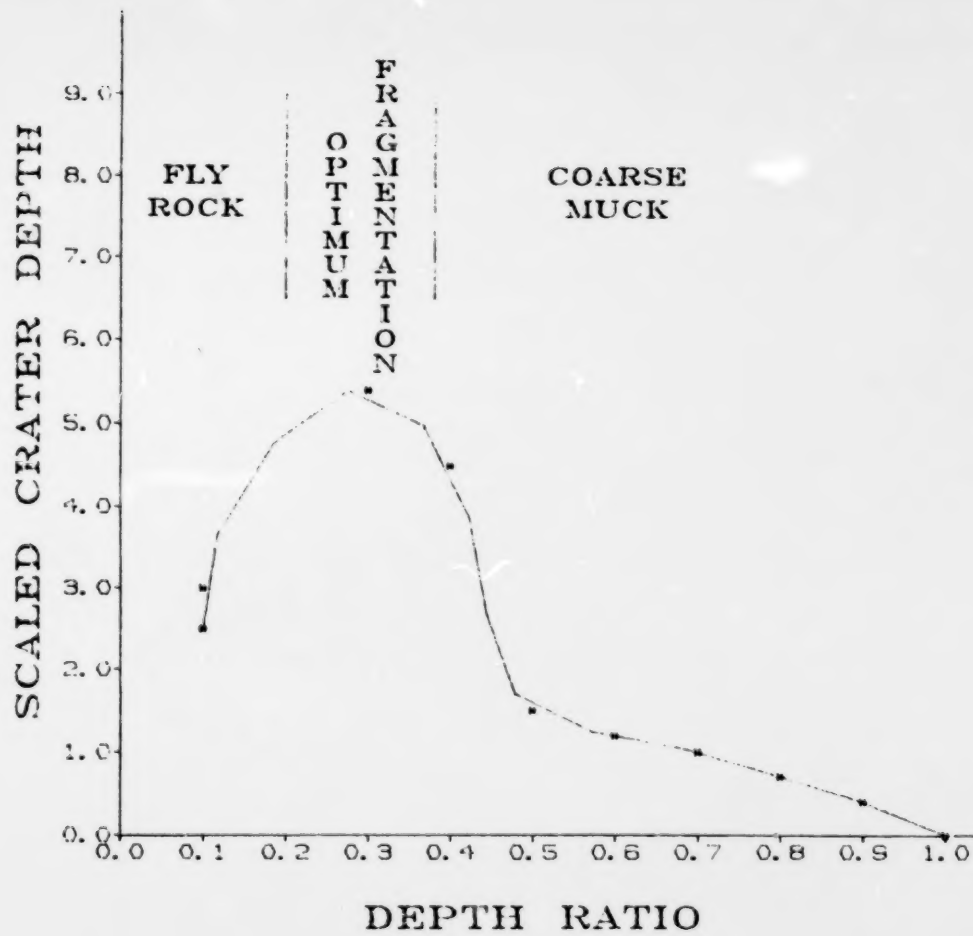


FIGURE 6 : TYPICAL SCALED CRATER DEPTH - DEPTH RATIO CURVE.

$$V = k(R/W^{1/3})^m$$

where V the peak particle velocity

 R the distance between the explosion and the recording site

 W the weight of the charge

 k, m site factors which must be determined at the particular mine site.

4.3 Comparison Between Usually Accepted Design Practice and Reality

One of the major disadvantages of the application of Livingston's theory today is that the generally accepted design practice tends to ignore the fact that a charge detonating at an earlier period creates a free face for the subsequent detonations. The generally accepted case which is shown at the top of Figure 7 assumes that the only active free face is the initial one.

However the actual case resembles the second drawing of Figure 7. Moreover if the charge detonating at a later period is very close to the free face created by an earlier detonation, the result will be flyrock and waste of energy. Therefore charge 2 (Figure 7 third drawing) will not break the volume of rock which it was supposed to break, leaving excessive burdens for the next charge.

In the programs presented in this report an attempt was made to simulate the reality.

At each depth of burial (AB) (depth from the closest free face) the crater radius can be calculated by using the

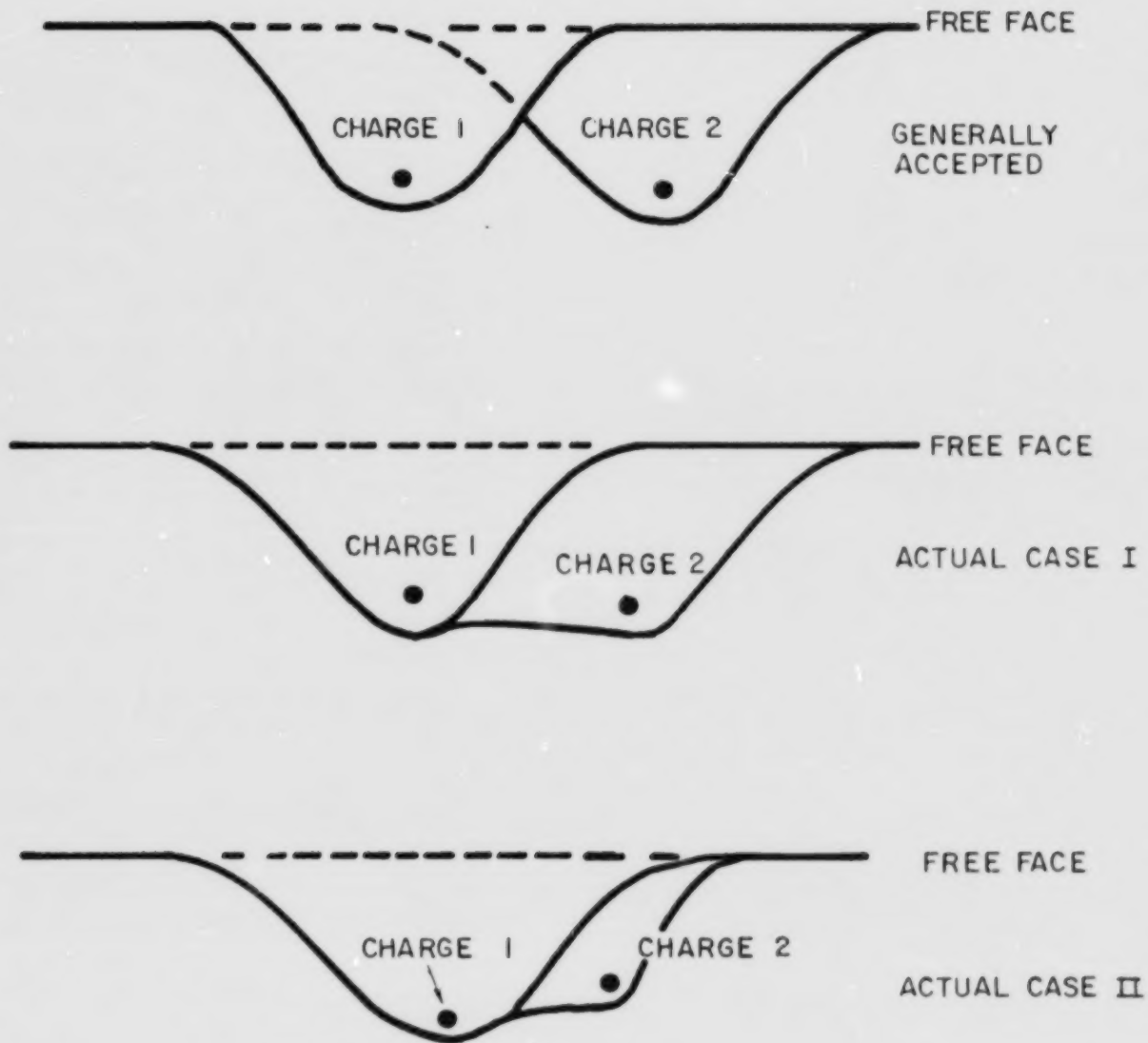


FIGURE 7 :
COMPARISON BETWEEN THE GENERALLY ACCEPTED DESIGN PRACTICE
AND TWO ACTUAL CASES .

scaled crater radius - depth ratio curve. Therefore the maximum distance at which rock is broken can be found (distance AC in Figure 8) for every position of the charge. This distance which is called slant distance indicates the maximum distance which the charge is going to break due to its position with respect to the free faces surrounding it.

It is believed that this approach is reasonable since the closest face offering a relief to the blast determines the dimensions of the resulting crater.

4.4 Blast Design Flowchart

The program is split into two main parts as regards the flowchart. These parts correspond to the large diameter blasthole benching operation and the vertical crater retreat method. They will be dealt with separately in this section.

Large Diameter Blasthole Benching

Figures 9(A) and 9(B) present the general flowchart for the large diameter blasthole benching portion of the program.

After the initialization of the variables, the input data are read. Data can be read in either metric or imperial units. Output from data read in metric units is produced in metric units while imperial unit input data generates output in imperial units.

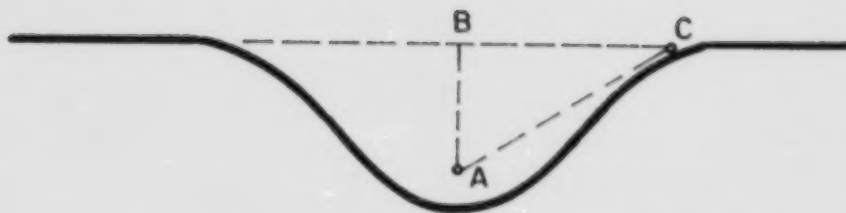


FIGURE 8 : MAXIMUM DISTANCE FROM A CHARGE IN WHICH
ROCK IS BROKEN.

PROGRAM LDBB — GENERAL FLOWCHART

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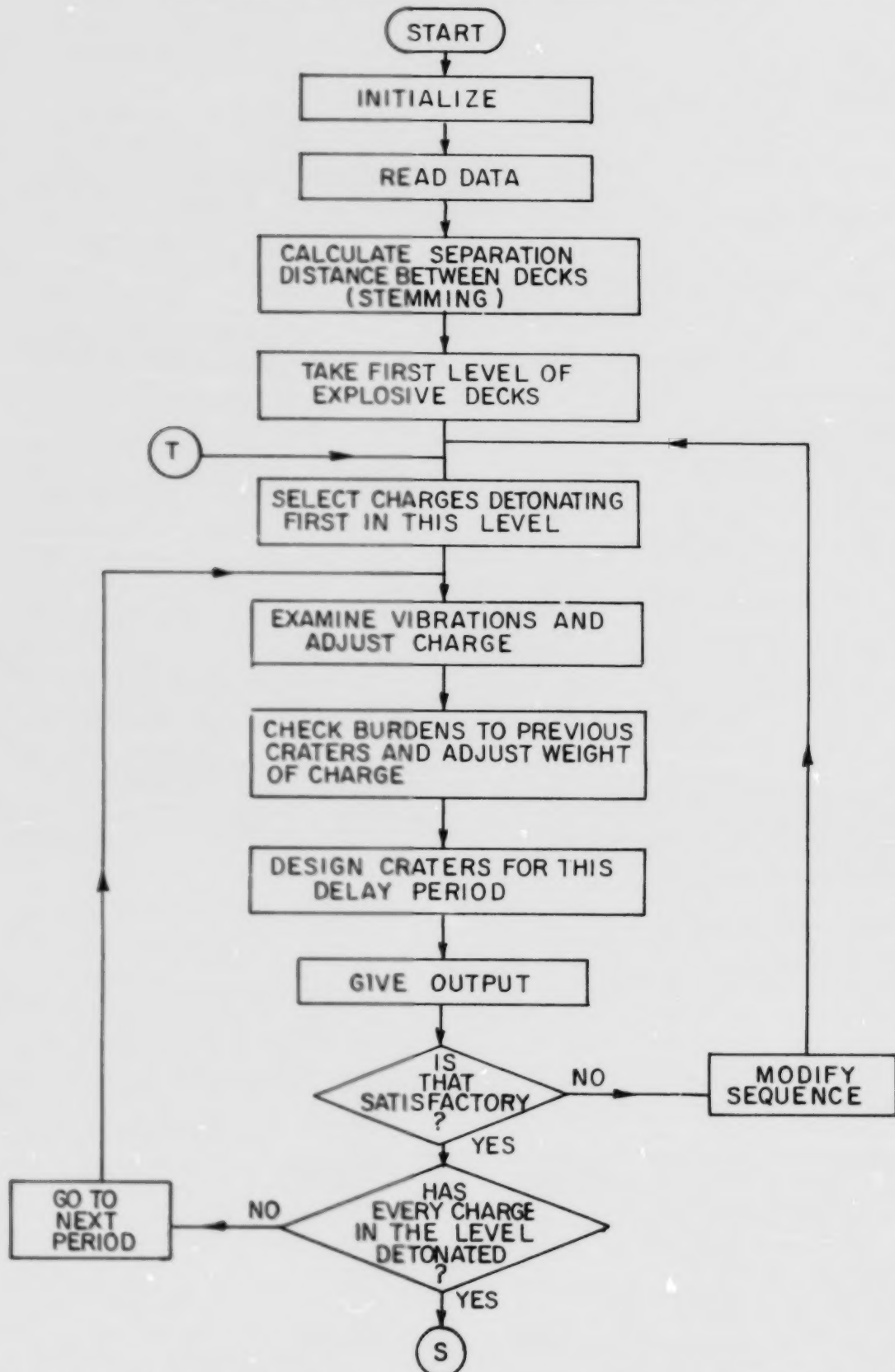


FIGURE 9(A): THE FIRST PART OF THE LARGE DIAMETER BLASTHOLE BENCH BLAST DESIGN PROGRAM FLOWCHART.

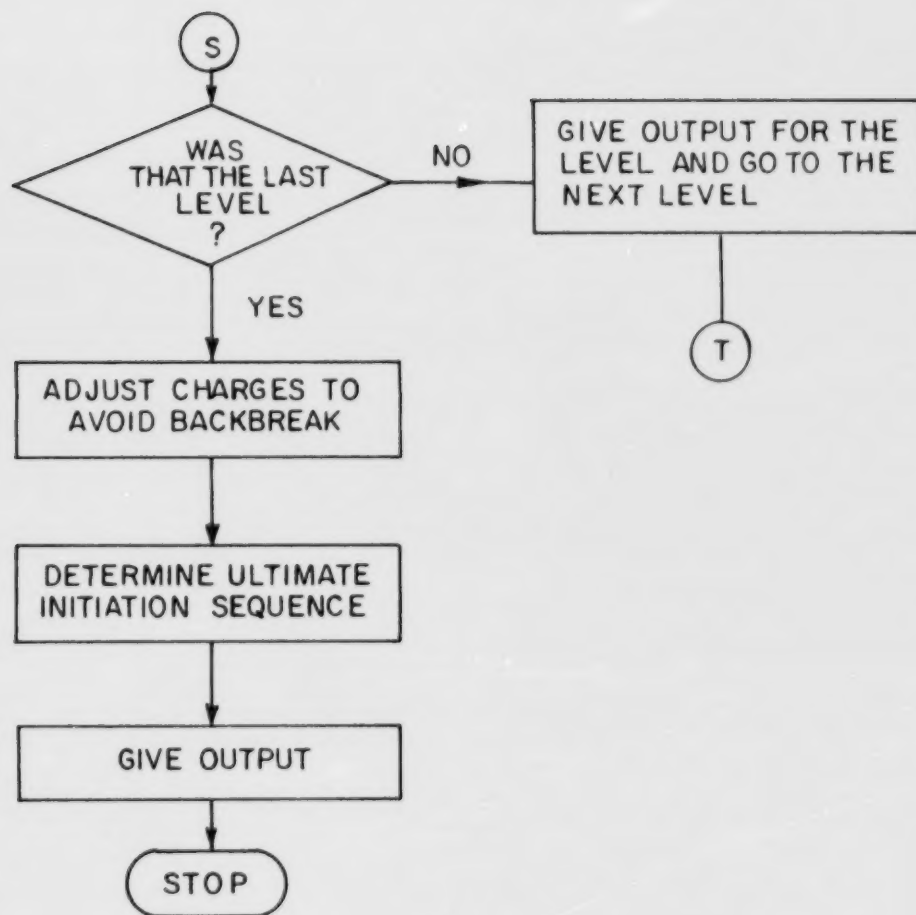


FIGURE 9(B) : THE SECOND PART OF THE LARGE DIAMETER BLASTHOLE BENCH BLAST DESIGN PROGRAM FLOWCHART.

The initial calculation of the separation between explosives decks is then made. Factors in the calculation include the rock type and other geological factors resulting in a required energy level for the material to produce good fragmentation. The influence of the different decks is accommodated by consideration of the fragmentation produced off the end of each deck charge, and in particular, the fragmentation produced by the end 8 charge diameters. This section of charge is considered separately as the shape of the stress wave form off the end of the charge is near spherical in shape and thus is typical of a spherical charge. The 8 charge diameter length is the longest charge that can be fired with results appearing to be similar to those that would be generated by an actual spherical charge itself.

Finally the deck separation is also considered in the light of the current experience which has shown the possibility of sympathetic detonation of delayed decks if the distance between them is too small. The best estimate available at the time of writing is that the deck separation should be no less than 16 times the hole diameter. This can be changed in the program later should a better relationship be established.

The next sequence of events is conducted on each successive charge and level of decks.

There are two methods of selecting the sequence of charge detonations. This may be inputted by the programmer or it may be generated by the program itself. The manual option has been introduced in the program to allow for overriding of the optimized self generated sequence should there be specific reasons for so doing by the mine engineer.

The charges are then examined for vibrations and adjustment is made if required. The burdens are checked to the previous craters and adjustments are made if necessary. The craters are then designed for these changes in the particular deck under consideration. The output for the process is then presented.

For the manual sequencing technique, the programmer is then asked if the output received to this point is satisfactory? if it is not the preceeding sequence of steps is repeated until the programmer is satisfied with the results. When the programmer is satisfied, or if the automatic mode is used, the program then checks to see if every charge in the level has been detonated. If they have not, again the preceeding sequence of events is repeated until all charges have been considered. Then the program proceeds.

The next question finds out if all of the different charge levels have been considered. If they have not the preceeding sequence is repeated for the next level, and so on, until all of the charges in the blast have been considered.

When all of the charges have been detonated the program then determines any special design with respect to wall control to avoid backbreak.

Finally the ultimate initiation sequence is determined and the output for the program is given.

Vertical Crater Retreat Method

Figure 10 presents the general flowchart for the vertical crater retreat method portion of the program.

Again the variables are initialized and the data are read. Again either metric or imperial units may be used.

A similar option to the one used in the bench blasting is available for the vertical crater retreat, this being the option to produce an optimized computer generated firing sequence for the charges, or to override this sequence and input a manual selection based on other factors.

The sequence of events in the vertical crater retreat design is now similar to a deck for the bench blasting program. The charge is examined for vibrations and adjusted if required. The burdens are then checked to previous craters and any adjustments in charge weight and delay are made. The new crater is then designed using, in this case, a three dimensional block model.

The program then checks if this is the last period to be detonated, if not the process is repeated. Once all of the charges have been detonated the blast is complete and the output is supplied.

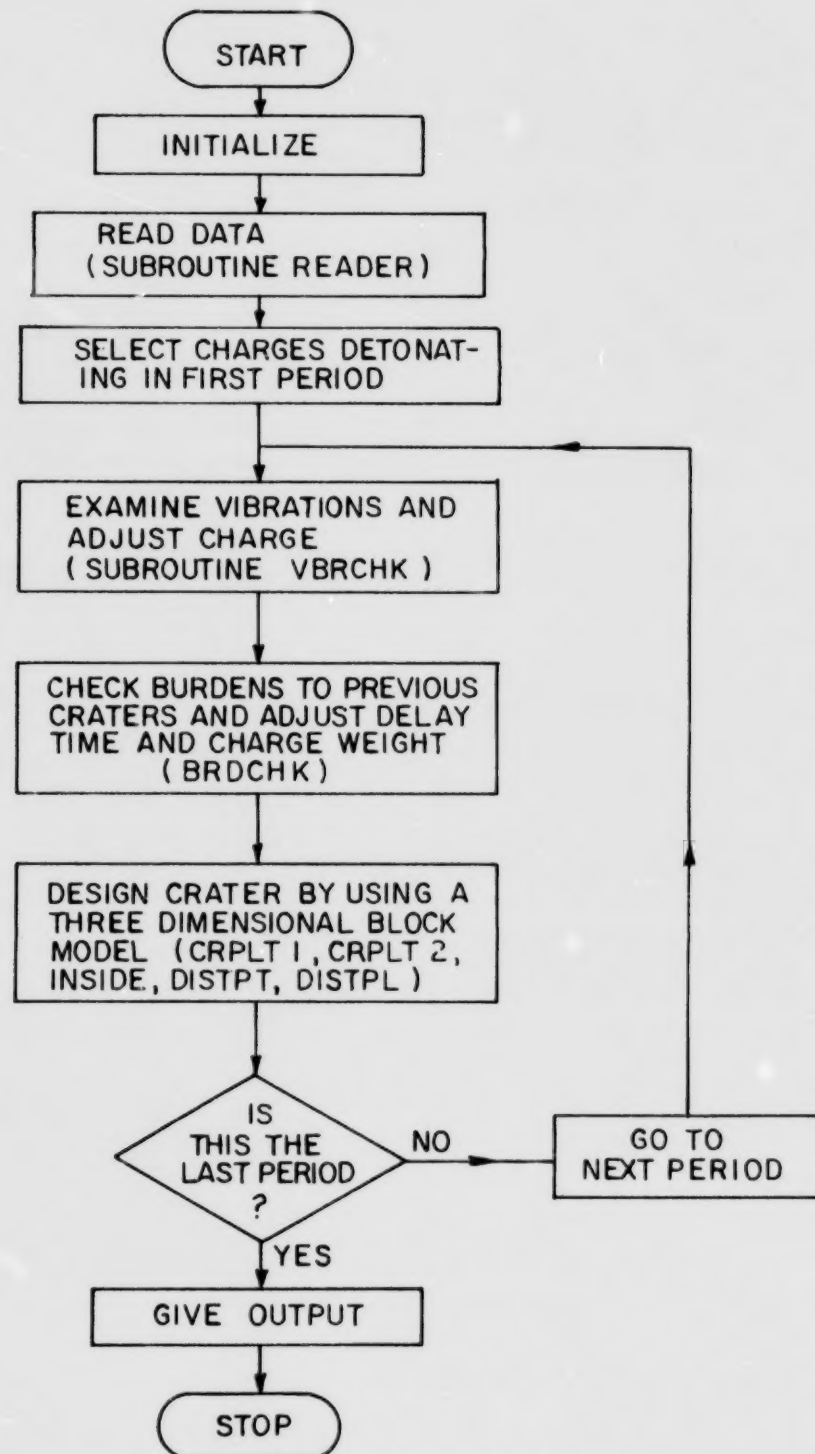
PROGRAM VCRM - GENERAL FLOWCHART

FIGURE 10: THE VERTICAL CRATER RETREAT METHOD BLAST DESIGN PROGRAM FLOWCHART.

Program Listing

A full listing of the program, split into four parts is presented in the Appendix A. The four parts are:

1. Vertical Crater Retreat Method Design
2. Large Diameter Bench Blast Design
3. Graphics Output Generator Program for Both Design Programs
4. Graphics Output Generator for the Vertical Crater Retreat after Blast Profile

4.5 Computer Software and Hardware

The programming language is VS FORTRAN which is compatible with most micro computers currently available.

The graphics used is the DI 3000 package prepared by Precision Visuals.

The computer used is the IBM 3081.

The graphics terminal used is the Tektronix 4107.

The plotter used is the Tektronix 4663S.

The program can be easily modified for use on most other currently available computers.

5.0 USERS MANUAL

This section shows how data are inputted into the program as well as presents the necessary exec files to run the program.

5.1 Input Data

The input data to the programs can be divided into four categories:

(a) Data related to the geometry of the blast.

These data are:

- The coordinates of the holes
- The location of the free face
- The coordinates of the points in which vibrations will be checked.

(b) Data related to Livingston's crater theory.

Data of this kind are:

- The scaled crater depth - depth ratio curve
- The scaled crater radius - depth ratio curve.

(c) Data related to the explosive. These data are:

- The weight strength of the explosive used in the tests and the explosive used in the blasting operations in the stope
- The density of the explosive.

(d) Other data such as:

- The diameter of the blastholes
- The number of the blastholes
- The site factors for the vibration checks
- The maximum acceptable levels of the peak particle velocity at different points.

Most of these data are fed in the program interactively. In the following it will be explained how to create the data files needed for the use of the program.

5.2 Data for the VCRM Program

The exec file (for the execution of the program) and the data files are shown in the Appendix B.

In the following the data files are described.

Unit 07: Data given interactively. The user has to respond to the questions of the program.

Unit 51: (INCOSTOP DATA) Data file containing the title and information regarding the geometry of the stope.

Line 1: Title (80 characters)

Line 2: FORMAT (3F10.2) x, y, z coordinates of reference point.

Line 3: FORMAT (3F10.2) stope length, stope width, stope depth.

Line 4: FORMAT (F10.2) angle of local axis x with mine axis x.

Unit 61: (INCO61 DATA) Coordinates of the holes at several elevations.

Line 1: FORMAT (4I5, F10.2) Hole number, number of points along the hole at which measurements were taken, row number, column number, hole diameter.

Subsequent lines: FORMAT (3F10.2) x, y, z coordinate

After the last point the procedure is repeated.

The end of the file is marked with the number 99.

Unit 62: (PCH3 DATA) File containing information about the position of the charges in the boreholes. This file is created by the computer.

Unit 08: (CRCURV DATA) File generated interactively. It contains the data from the cratering curves. Once this file is created it does not have to be generated at each run of the program.

Unit 11: (VIBRAT DATA) File generated interactively. It contains data for the vibration checks.

Unit 70: (CHLOC DATA) Intermediate data file created by the computer.

Unit 77: (PLBLD DATA) Data file generated by the computer. It is used as data to the plotting program.

5.3 Data for Program LDBB

The exec file (for the execution of the program) and the data files are shown in the Appendix B. In the following a brief description of the data files will be given:

Unit 07: Data given interactively. The user has to respond to the programs questions.

Unit 08: (BCURV DATA) File generated interactively. It contains the data for the cratering curves. Once this file is created it can be used for the subsequent runs.

Unit 09: (BBLAST DATA) File containing geometrical data for the position of the free face.

Line 1: FORMAT (I5) Number of points defining the free face.

Subsequent Lines: FORMAT (2F10.2) x, y coordinates of each point.

Unit 11: (VIBRAT DATA) File generated interactively. It contains the data for the vibration checks. This file can be used in the subsequent runs.

Unit 12: (TOP DATA) File containing coordinates of points beyond which backbreak should not occur.

Line 1: FORMAT (I5) Number of segments defining the limit.

Subsequent Lines: FORMAT (4F10.2) x1, y1, x2, y2 coordinates of points defining each segment.

Unit 51: (INCOSTOP DATA) Data file containing the title and information regarding the geometry of the stope.

Line 1: FORMAT (A80) Title (80 characters)

Line 2: FORMAT (3F10.2) x, y, z coordinates of the reference point.

Line 3: FORMAT (3F10.2) stope length, stope width, depth.

Line 4: FORMAT (F10.2) angle of local axis x with mine axis x.

Unit 61: Intermediate data file created by the computer.

Unit 66: (INCO62 DATA) Coordinates of the holes at several elevations.

Line 1: FORMAT (4I5, F10.2) Hole number, number of points along the hole at which measurements were taken, row number, column number, hole diameter.

Line 2: FORMAT (3F10.2) x, y, z coordinates of the collar.

Subsequent Lines: FORMAT (3F10.2) x, y, z coordinates of the point. After the last point the procedure is repeated.

The end of the file is marked with number 99.

Unit 70: Intermediate file created by the computer.

Unit 62: (PCH3 DATA) File created by the computer. It contains the input data for the plotting program (PGRAPH).

Unit 72: (OUTLINE DATA) Data giving the outline of the stope.

Line 1: FORMAT (I5) Number of points giving outline.

Subsequent Lines: FORMAT (2F10.2) x, y coordinates of each point.

5.4 Data for Graphics Programs

Graphics output is given by using programs PGRAPH and PLBLAST. PGRAPH provides cross-sections and plan views at the blast block while PLBLAST gives the after blast profile of the VCR stope. The exec files for the use of these programs can be found in Appendix B. The input data for the programs are prepared by the programs used for the design of the blast (VCRM, LDBB). The user has to respond to a few questions asked by the programs.

6.0 TYPICAL PROGRAM OUTPUT

This section presents typical computer output for both the graphics and hard copy output for the blaster.

Figures 11 and 12 present the blasthole vertical and horizontal projections. This can be produced for any blasthole, whether the bench blasting or vertical crater retreat method is being used.

Figure 13 presents a typical stope plan. Plans can be produced for any level that may be desired.

Figures 14 through 17 present cross-sections of rows and columns of blastholes with the blasters information superimposed. The charge depth, charge size and required delay period are listed.

Figure 18 is a plan view of a VCR stope and Figures 19 and 20 are a typical row and column respectively with the blasthole loading information.

Appendix C presents typical output from the LDBB and VCR programs.

The large diameter blasthole bench output first presents the initiation sequence and explosive charge weights for each deck level. A plan view is provided of the broken material which is an aid for the manual operated initiation sequence only. It need not be reproduced if it is not desired.

A summary of the explosives required and number of the different delay periods follows. Finally the individual loading instructions for all of the blastholes is presented.

The vertical crater retreat output first presents the final modified blasthole initiation sequence, followed by the charge weight per hole. The blast fragmentation is illustrated in plan view either in a shaded form or using a digital presentation ready for contouring.

A summary of the explosives required and number of the different delay periods follows. Finally the individual loading instructions for all of the blastholes is presented.

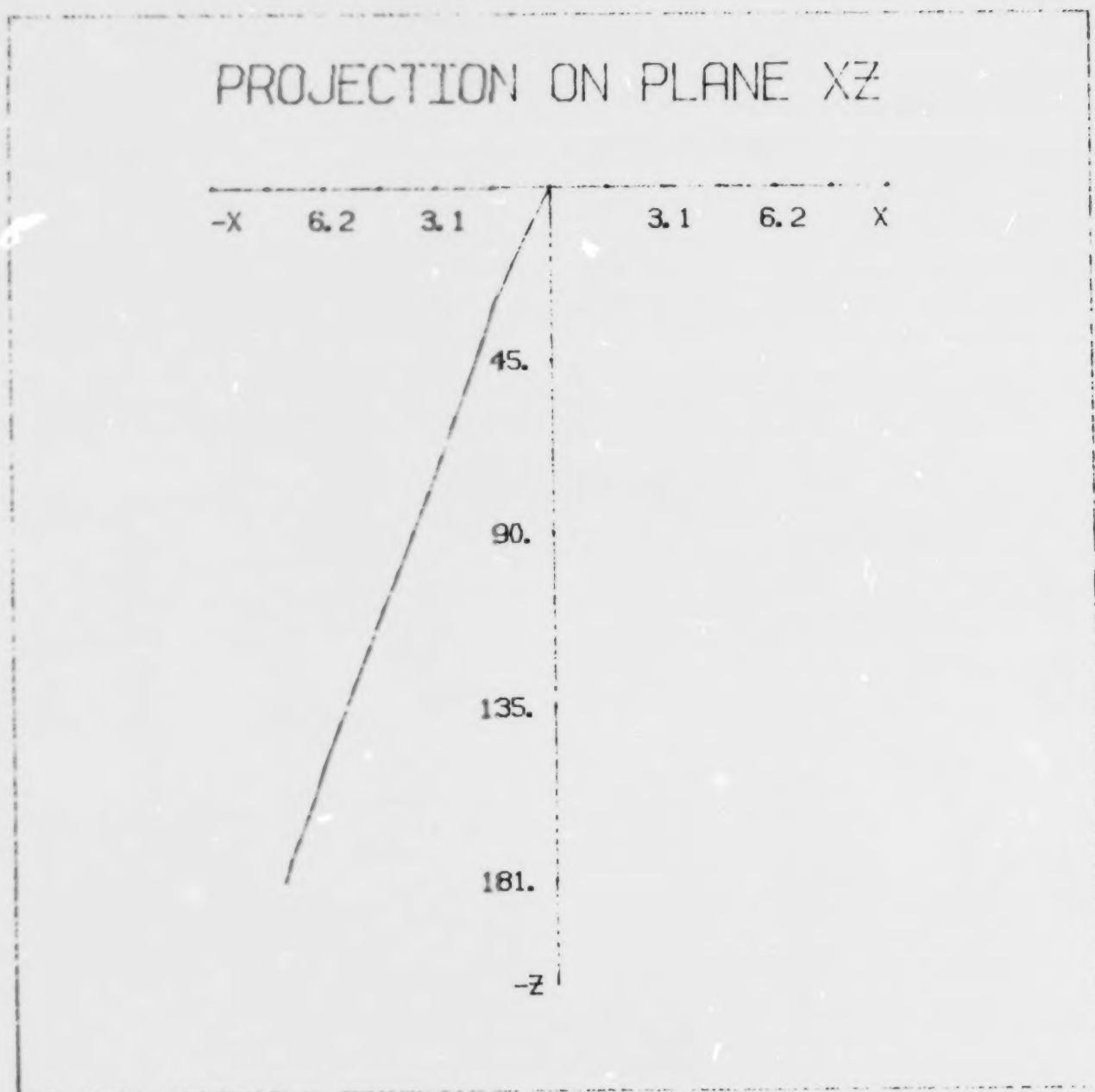


FIGURE 11: TYPICAL COMPUTER OUTPUT SHOWING BLASTHOLE PROJECTION ON PLANE XZ.

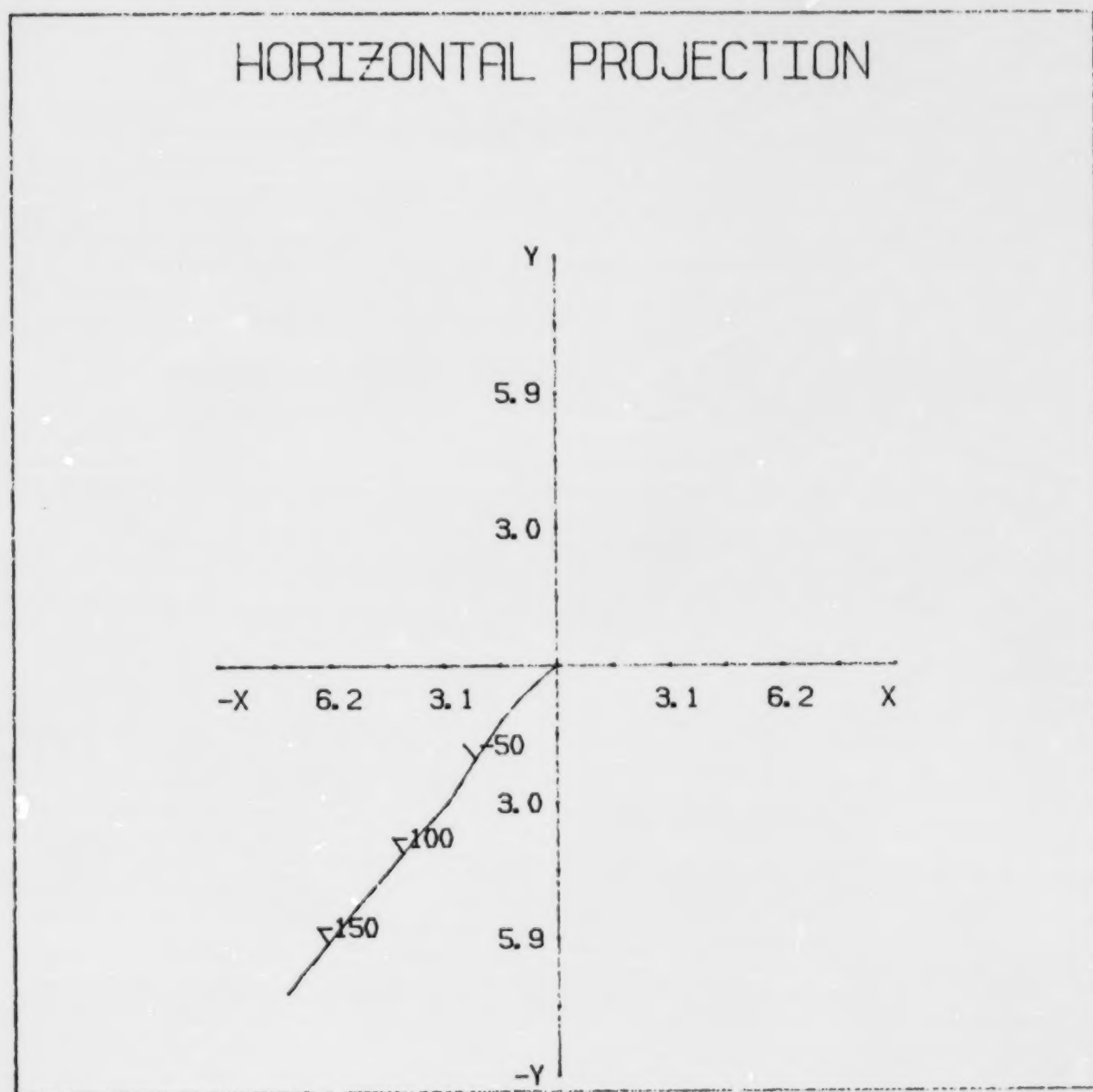


FIGURE 12: TYPICAL COMPUTER OUTPUT SHOWING HORIZONTAL BLASTHOLE PROJECTION.

SAMPLE STOPE FROM INCO
PLAN ON ELEVATION 9520

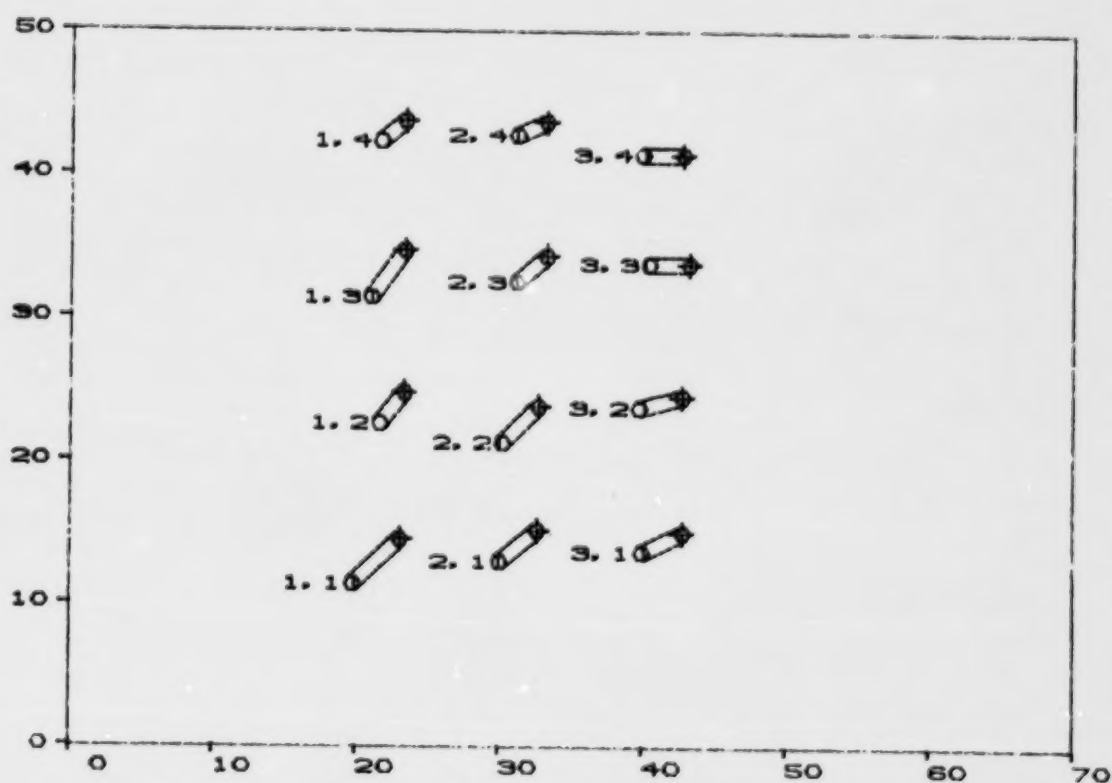


FIGURE 13: TYPICAL COMPUTER OUTPUT FOR THE LDBB PROGRAM SHOWING
PLAN VIEW OF A STOPE.

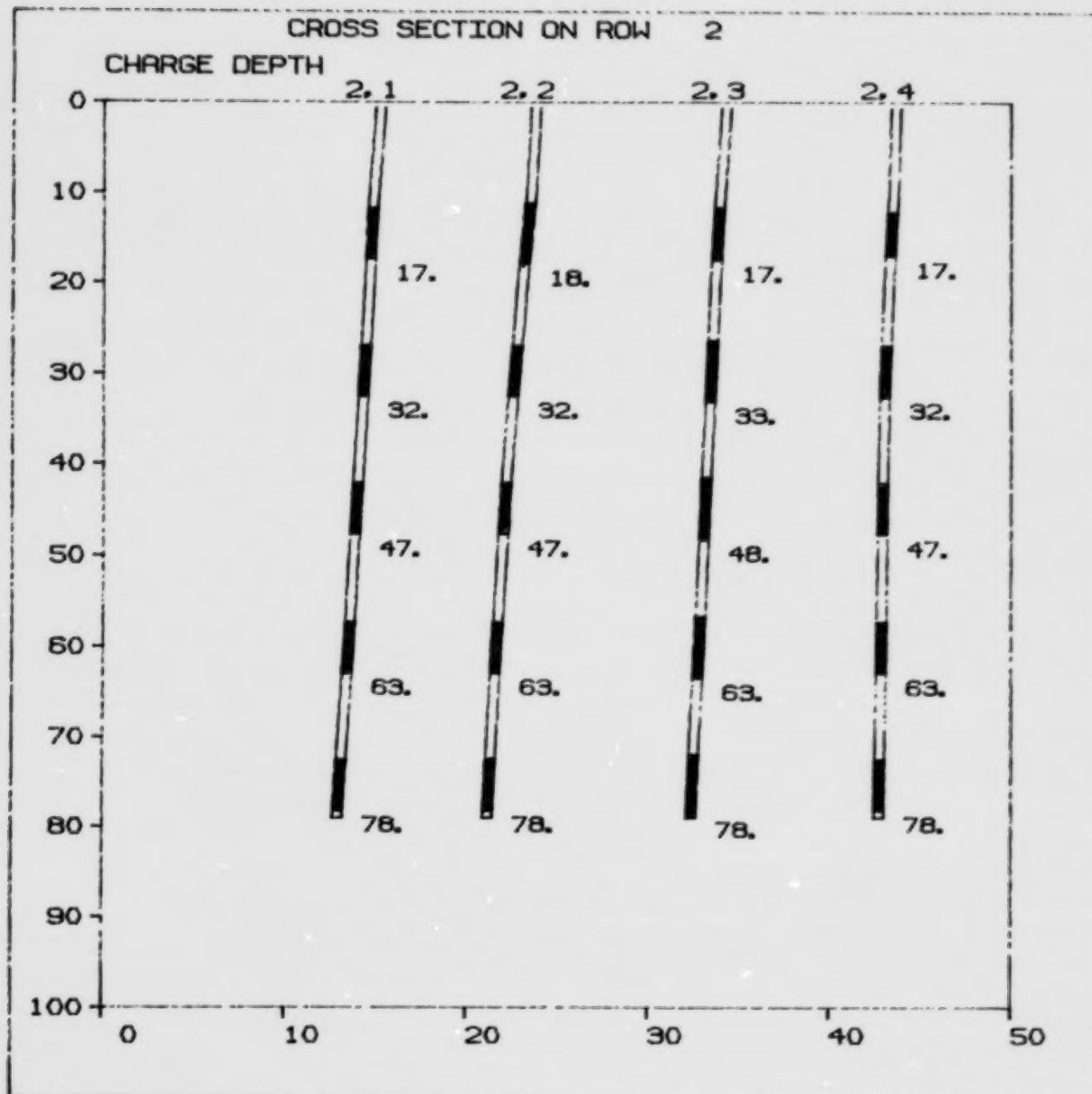


FIGURE 14: TYPICAL COMPUTER OUTPUT FOR THE LDBB PROGRAM
SHOWING A ROW CROSS-SECTION WITH CHARGE DEPTHS.

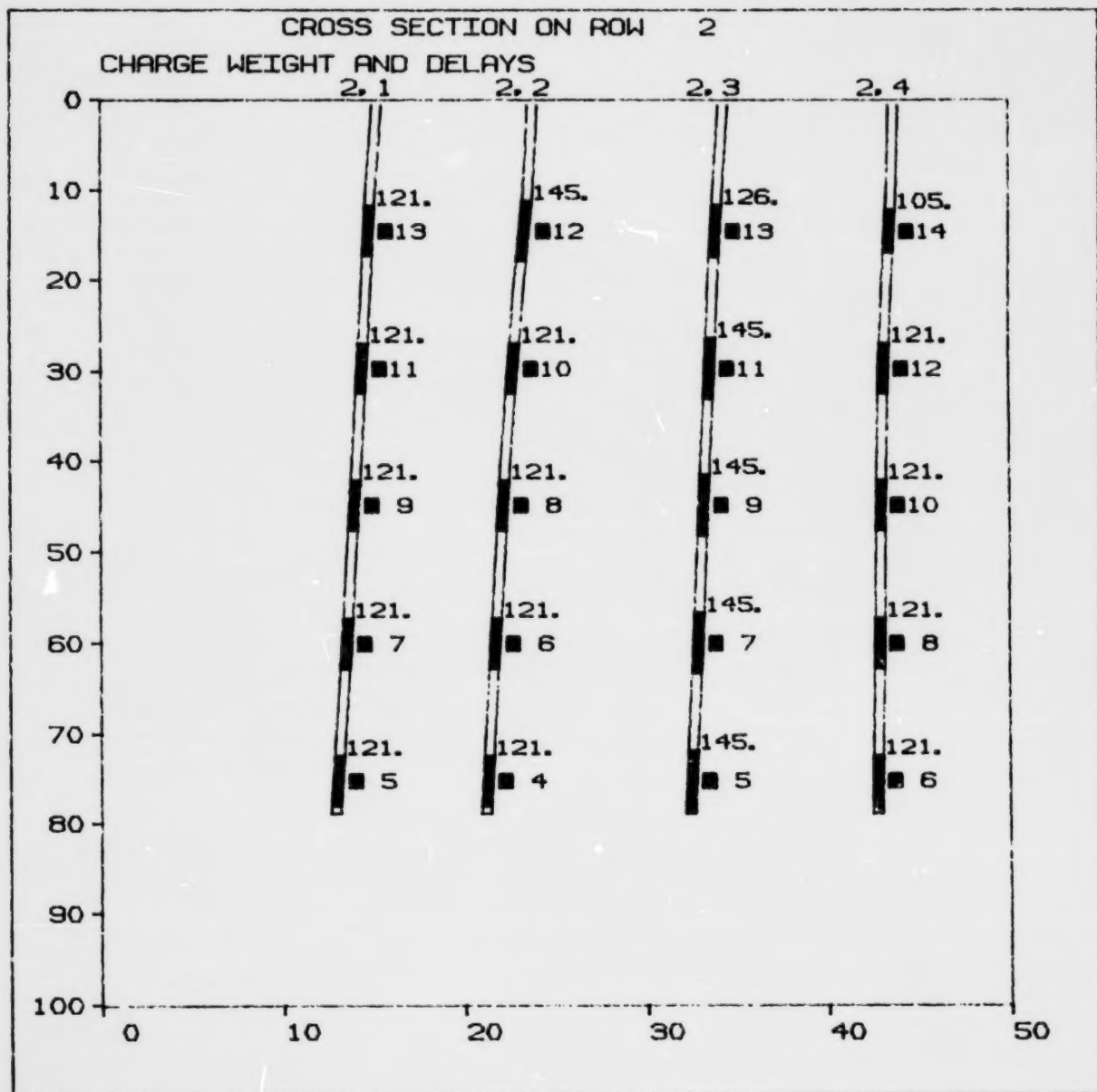


FIGURE 15: TYPICAL COMPUTER OUTPUT FOR THE LDBB PROGRAM SHOWING A ROW CROSS-SECTION WITH CHARGE WEIGHTS AND DELAYS.

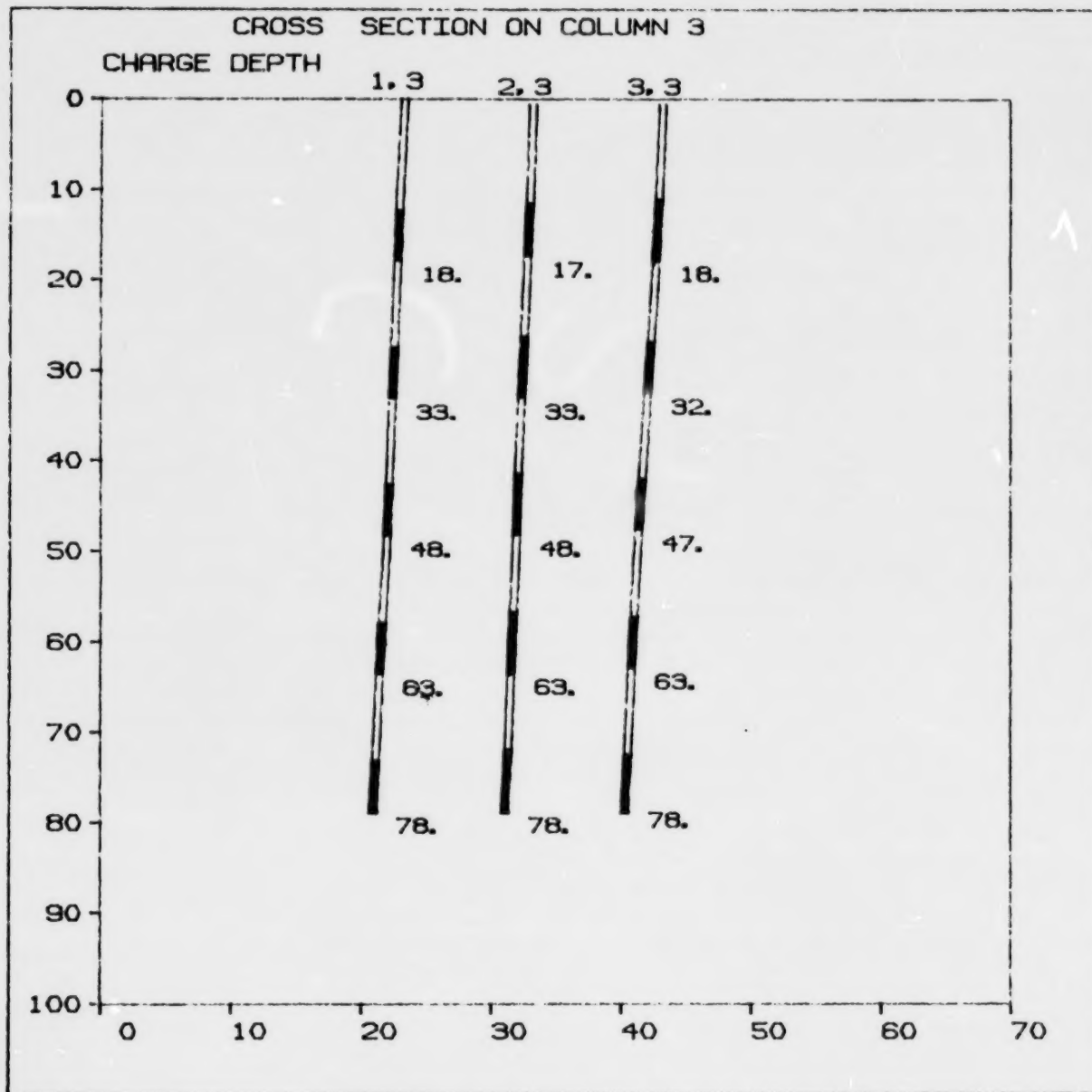


FIGURE 16: TYPICAL COMPUTER OUTPUT FOR THE LDBB PROGRAM SHOWING A COLUMN SECTION WITH CHARGE DEPTHS.

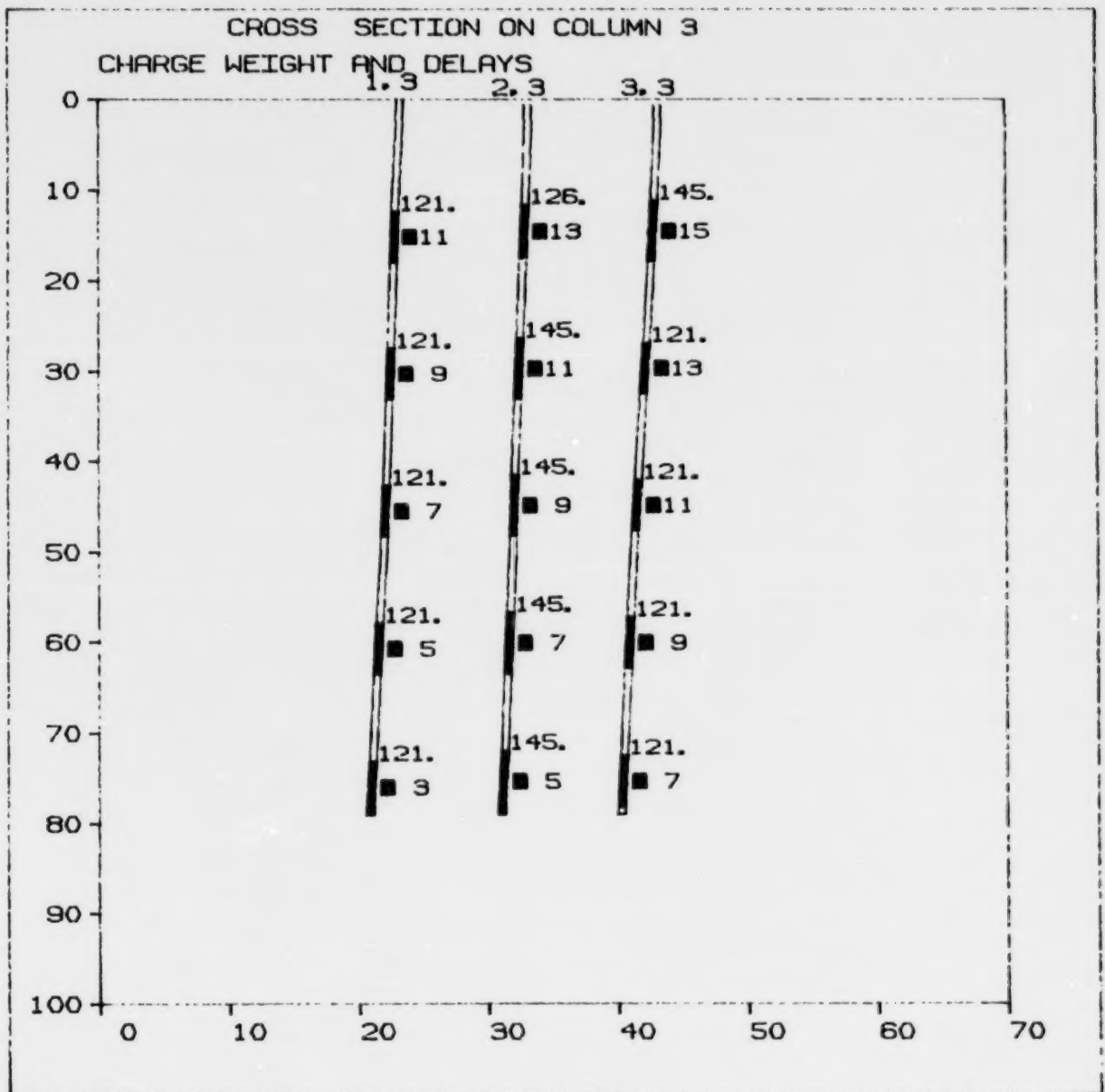


FIGURE 17: TYPICAL COMPUTER OUTPUT FOR THE LDBB PROGRAM SHOWING A COLUMN SECTION WITH CHARGE WEIGHTS AND DELAYS.

SAMPLE STOPE FROM INCO
PLAN ON ELEVATION 9600

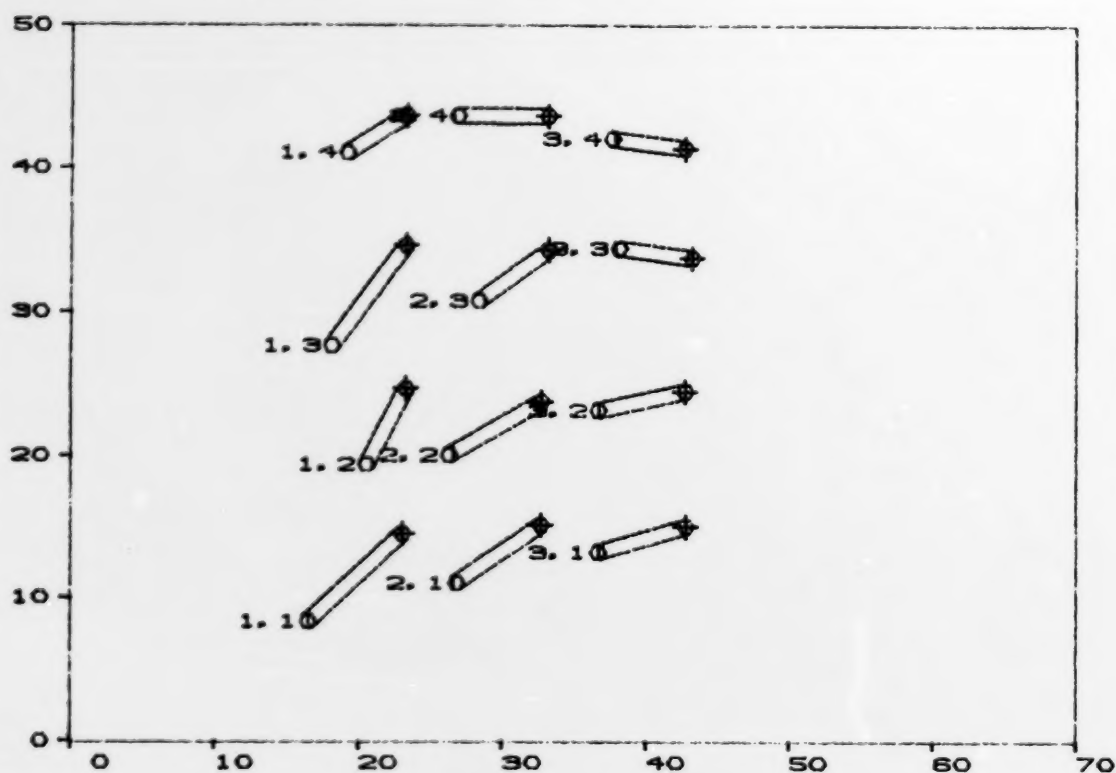


FIGURE 18: TYPICAL COMPUTER OUTPUT FOR THE VCRM PROGRAM
SHOWING STOPE PLAN.

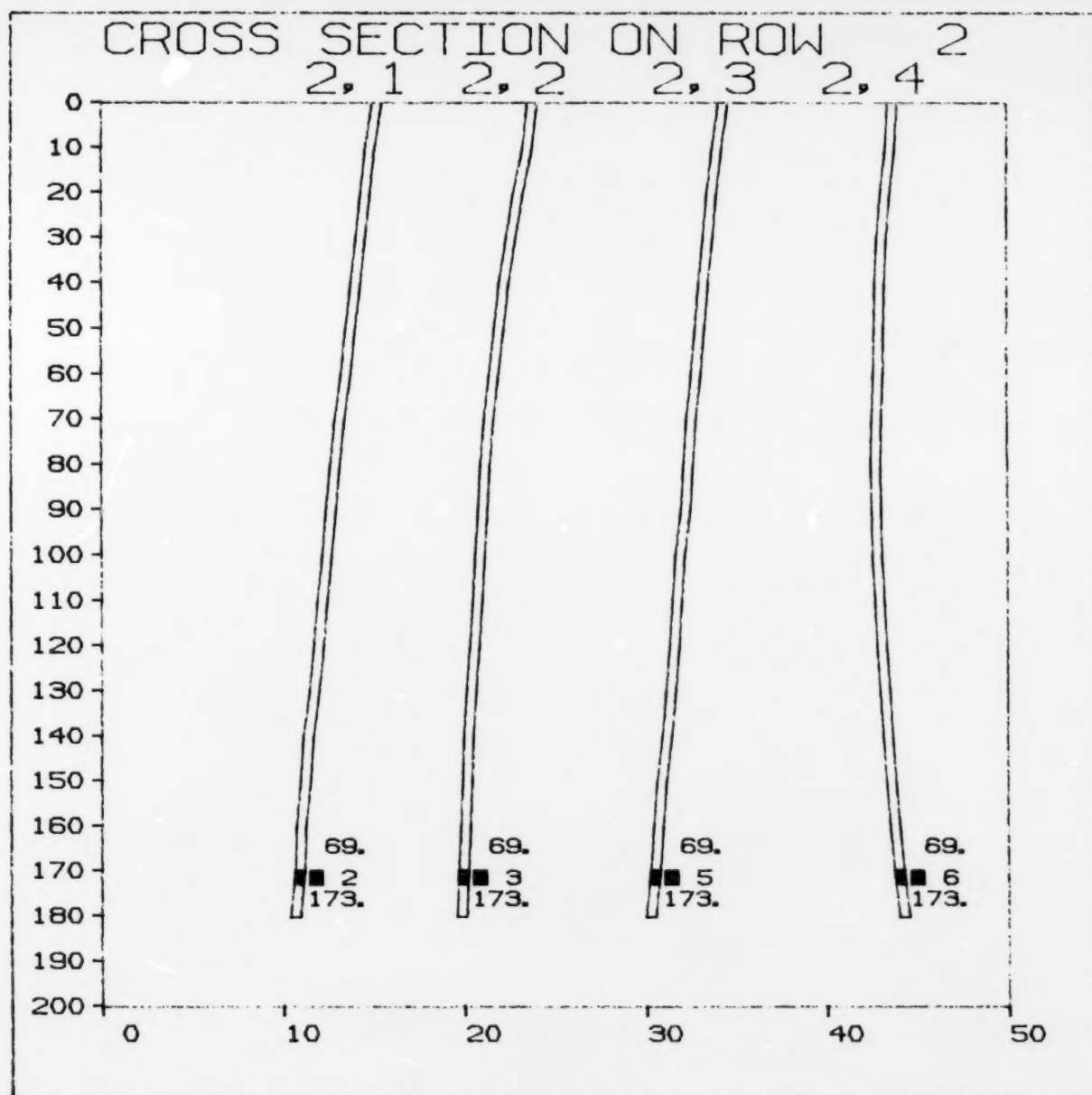


FIGURE 19: TYPICAL COMPUTER OUTPUT FOR THE VCRM PROGRAM SHOWING A ROW SECTION WITH CHARGE WEIGHTS, DELAYS AND CHARGE DEPTHS.

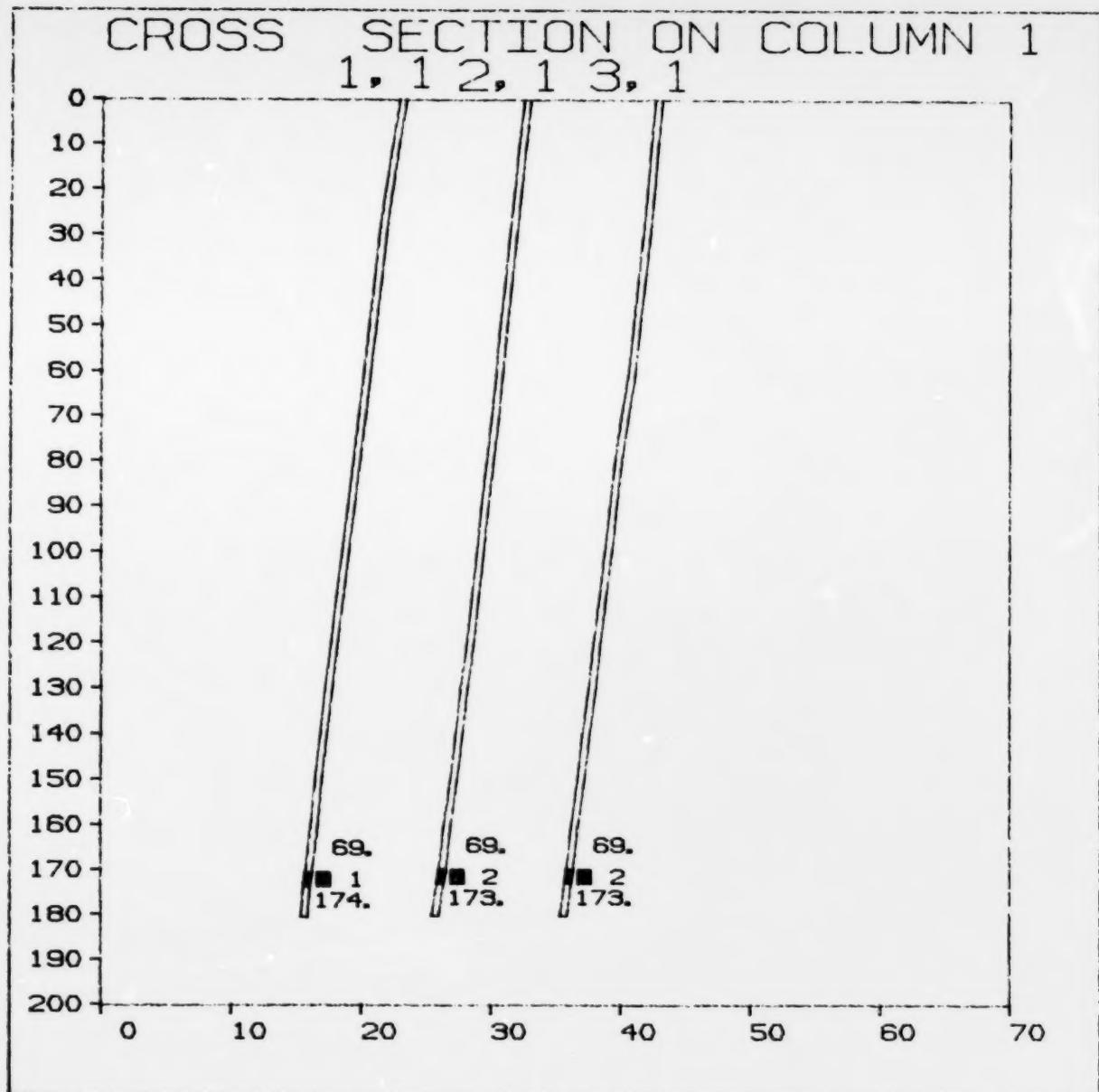


FIGURE 20: TYPICAL COMPUTER OUTPUT FOR THE VCRM PROGRAM
SHOWING A COLUMN SECTION WITH CHARGE WEIGHTS,
DELAYS AND CHARGE DEPTHS.

7.0 CONCLUSION

1. Two programs (VCRM and LDBB) have been developed to design and calculate a blast for a particular hole layout for VCR stopes, benches, circular and rectangular openings.

These programs consider:

- The effect of the multiple free faces on the blast.
- The effects of the delay sequencing on the blast.
- The properties of the rock and the explosive.
- The powder factor with respect to the desired fragmentation.
- The vibrations experienced in different points of the mine.
- The minimum deck separation distance to avoid sympathetic initiation.
- The minimization of backbreak.

2. The programs simulate the blast and give graphics output as well as a hard copy of the expected result.

3. The programs give instructions for the loading of the boreholes.

4. The programs provide a graphic model of the blast block.

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APPENDIX A

COMPUTER PROGRAM PRINTOUTS

1. VERTICAL CRATER RETREAT METHOD DESIGN
2. LARGE DIAMETER BENCH BLAST DESIGN
3. GRAPHICS OUTPUT GENERATOR PROGRAM FOR BOTH
DESIGN PROGRAMS
4. GRAPHICS OUTPUT GENERATOR FOR THE VERTICAL
CRATER RETREAT AFTER BLAST PROFILE.

1. VERTICAL CRATER RETREAT METHOD DESIGN

PROGRAM VCRN

```

C
C  THIS PROGRAM DESIGNS THE BLAST FOR A VCR STOPS WHEN THE POSITION
C  OF THE HOLES AND THE CRATERING CHARACTERISTICS ARE KNOWN. THE
C  PROGRAM GIVES AN OUTPUT INDICATING PROBLEMS DUE TO THE DEVIATION
C  OF THE HOLES

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LAST EDITION : NOVEMBER 1984

VARIABLES :

```

C      ALONG : LENGTH OF THE EXPLOSIVE COLUMN
C      DCNCH : DEPTH OF CONTAINED CHARGE (SPHERICAL)
C      DRDOPD : CHARGE LOCATION IN THE BOREHOLE
C      DELTA : DEPTH RATIO
C      DELTAK : DEPTH RATIO
C      DELTO : OPTIMUM DEPTH RATIO
C      DEPTH : DEPTH OF CRATER
C      DHOLE : DIAMETER OF BOREHOLE
C      DHOLEI : INCREASED DIAMETER OF BOREHOLE (FOR GRAPHICS)
C      DOPT(I) : DEPTH OF BURIAL
C      ELACTK : STRAIN ENERGY FACTOR FOR SPHERICAL CHARGES
C      ELEV : ELEVATION OF THE FREE FACE
C      EXPTYP : EXPLOSIVE TYPE
C      EXPTYP : EXPLOSIVE TYPE
C      IBLOCK(I,J,K) : IF GREATER THAN ZERO BLOCK (I,J) TAKEN
C                      OTHERWISE BLOCK IS NOT TAKEN
C      IPER(I) : DELAY PERIOD OF CHARGE I
C      ITIME(I,J,K) : ARRAY INDICATING PERIOD IN WHICH BLOCK (I,J)
C                      WAS REMOVED
C      INR(I,J) : ARRAY FOR PLOTTING OF OUTPUT
C      NSYSN : 1 METRIC
C              2 IMPERIAL
C      NP1 : NUMBER OF POINTS IN SCALED CRATER DEPTH - DEPTH
C              RATIO CURVE (SPHERICAL)
C      NP2 : NUMBER OF POINTS IN SCALED CRATER RADIUS - DEPTH
C              RATIO CURVE (SPHERICAL)
C
C      NUNH : NUMBER OF HOLES IN THE BLAST
C      RHOE : DENSITY OF THE EXPLOSIVE
C      SCDEPT : SCALED DEPTH OF BURIAL FOR SPHERICAL CHARGES
C      SCRAD : SCALED RADIUS FOR SPHERICAL
C      SCROP : OPTIMUM SCALED RADIUS
C      TITLE : TITLE
C      WEIGHT : WEIGHT OF EXPLOSIVE CHARGE
C      WSTR : WEIGHT STRENGTH
C      WTKRG : WEIGHT OF CHARGE IN TESTS (SPHERICAL)
C      X(I) : X COORDINATE OF HOLE I
C      XB(I) : X COORDINATE OF POINT (BLOCK) (I,J,K)
C      XMAX : MAX LOCAL LENGTH (USED TO DETERMINE LENGTH OF BLOCK)
C      XMIN : MIN LOCAL LENGTH
C      Y(I) : Y COORDINATE OF HOLE I

```

```

C      YB(J) : Y COORDINATE OF POINT (BLOCK) (I,J,K)          VCR00560
C      YMAX : MAX LOCAL WIDTH (USED TO DETERMINE LENGTH OF BLOCK) VCR00570
C      YMIN : MIN LOCAL WIDTH                                   VCR00580
C      Z(1) : Z COORDINATE OF HOLE 1                           VCR00590
C      ZC(K) : Z COORDINATE OF POINT (BLOCK) (I,J,K)          VCR00600
C                                                                VCR00610
C                                                                VCR00620
C                                                                VCR00630
C      INTEGER A4 CLTIME, TCPU, LUS, INCH, FT                  VCR00640
C      CHARACTER A15 EXPTYP, EXPTYR                             VCR00650
C      CHARACTER A80 TITLE                                       VCR00660
C      CHARACTER A8 QDATE, QTIM                                   VCR00670
C      CHARACTER A1 IFANCY(120)                                  VCR00680
C      COMMON /RDRDT1/ DCONCH, WTCHRG, WSTRTH, SCDEPT(50), DELTA(50),
XSCRAD(50), DHOLE, X(50), Y(50), Z(50), XVCHK(10), YVCHK(10), ZVCHK(10) VCR00690
X, PPVALL(10), AKEAC, AMEAC, XPIL1(10), XPIL2(10), XPIL3(10), YPIL1(10), VCR00700
XPIL2(10), YPIL3(10), ZPIL1(10), ZPIL2(10), ZPIL3(10), PPVPAL, WSTR, VCR00710
XXMAX, XMIN, YMAX, YMIN, ZMAX, ZMIN, DELTAR(50), RHOE           VCR00720
COMMON /RDRDT2/ NP1, NP2, NUMBH, NCHK, NUMPIL, INIT(50), MSYSUN VCR00730
COMMON /IBLK/ IBLOCK(100,100,5), ITIME(100,100,5)             VCR00740
COMMON /DXDYDZ/ DX, DY, DZ                                     VCR00750
COMMON /DELT/ DELTO, EFACR                                     VCR00760
COMMON /XBLK/ XB(100), YB(100), ZB(5)                          VCR00770
COMMON /ISEQ/ IPER(50), KK                                     VCR00780
COMMON /FLY/ IFLY(50)                                          VCR00790
COMMON /CHARGE/ WEIGHT(50), DUPT(50), RCR(50), DEPTH(50), SCROP VCR00800
COMMON /BURDEN/ BURDEN(50,50)                                  VCR00810
COMMON /TYPE/ EXPTYP, EXPTYR                                   VCR00820
COMMON /TT/ TITLE                                              VCR00830
COMMON /REFER/ XREFER, YREFER, ZREFER, STANGR, STLENG, STWIDT VCR00840
X, STDEPT                                                       VCR00850
COMMON /UNALP/ LUS, INCH, FT                                  VCR00860
DIMENSION IWR(133,140), ZROUT(5), ALENG(50), UDOUPD(50)       VCR00870
----- VCR00880
C  **      INITIALIZE DATA      **                             VCR00890
C----- VCR00900
      PI = 3.14159                                             VCR00910
      DO 1901 I= 1,133                                         VCR00920
      DO 1900 J= 1,140                                         VCR00930
      IWR(I,J) = 0                                             VCR00940
1900 CONTINUE                                                  VCR00950
1901 CONTINUE                                                  VCR00960
      DO 9000 I=1,50                                           VCR00970
      INIT(I)=0                                                VCR00980
9000 CONTINUE                                                  VCR00990
C----- VCR01000
C  **      READ DATA      **                                   VCR01010
C----- VCR01020
      CALL READER                                              VCR01030
C----- VCR01040
C  **      FIND LIVINGSTON'S STRAIN ENERGY FACTOR      **    VCR01050
C----- VCR01060
      EFACR = DCONCH / WTCHRG ** (1.0/3.0)                    VCR01070
C----- VCR01080
C  **      FIND OPTIMUM DEPTH RATIO      **                    VCR01090
C----- VCR01100

```

```

DO 10 I = 1, NP1
  IF (SCDEPT(I+1).GE.SCDEPT(I)) GO TO 10
  DELTO = DELTA(1)
  IOPT = I
  GO TO 14
10 CONTINUE
14 CONTINUE
C-----
C  ** FIND SCALED RADIUS AT OPTIMUM DEPTH RATIO **
C-----
DO 15 I = 2, NP2
  IF((DELTAR(I).GE.DELTO).AND.(DELTAR(I-1).LE.DELTO)) GO TO 16
15 CONTINUE
16 SCROP = SCRAD(I-1) + (DELTO - DELTAR(I-1))/(DELTAR(I) - DELTAR(I-1))
  X *(SCRAD(I)-SCRAD(I-1))
C-----
C  ** DETERMINE INITIATION SEQUENCE **
C-----
CALL SEQUEN
C-----
C  ** GET HOLE DETONATING IN PERIOD #1 **
C-----
11 DO 19 I = 1, NUMBH
  IF (IPER(I).GT.1) GO TO 19
  IFIRST = I
  GO TO 20
19 CONTINUE
20 CONTINUE
  IN = IFIRST
  CALL VBRCHK (IFIRST)
C-----
C  ** GO TO NEXT PERIOD **
C-----
  ID = 0
250 CONTINUE
  DO 280 I = 1, NUMBH
  IF (IPER(I).NE.(IPER(IFIRST) + 1)) GO TO 280
  IN = I
  GO TO 281
280 CONTINUE
281 IFIRST = IN
  CALL VBRCHK (IFIRST)
C-----
C  ** CHECK FOR MINIMUM BURDENS ( FLYROCK ) **
C-----
  CALL BROCHK (IFIRST,KIND,INEXT)
  IF (KIND.NE.2) GO TO 400
  DO 390 I = 1, NUMBH
  IF(IPER(I).NE.IPER(INEXT)) GO TO 390
  IN = I
  GO TO 281
390 CONTINUE
C-----
C  ** CHECK IF WE ARE IN THE LAST DELAY PERIOD **
C-----

```

VCR01110
VCR01120
VCR01130
VCR01140
VCR01150
VCR01160
VCR01170
VCR01180
VCR01190
VCR01200
VCR01210
VCR01220
VCR01230
VCR01240
VCR01250
VCR01260
VCR01270
VCR01280
VCR01290
VCR01300
VCR01310
VCR01320
VCR01330
VCR01340
VCR01350
VCR01360
VCR01370
VCR01380
VCR01390
VCR01400
VCR01410
VCR01420
VCR01430
VCR01440
VCR01450
VCR01460
VCR01470
VCR01480
VCR01490
VCR01500
VCR01510
VCR01520
VCR01530
VCR01540
VCR01550
VCR01560
VCR01570
VCR01580
VCR01590
VCR01600
VCR01610
VCR01620
VCR01630
VCR01640
VCR01650

A6

```

400 MAXPER = 0
DO 425 I11 = 1, NUMBH
IF (MAXPER.GT.IPER(I11)) GO TO 425
MAXPER = IPER(I11)
425 CONTINUE
IF (IPER(IFIRST).LT.MAXPER) GO TO 250
C-----
C  AA  DESIGN CRATERS  CRATERS  AA
C-----
ZMAX = Z(1)
ZMIN = 1000000.0
DO 431 IT = 1, NUMBH
ZZZ = ZMAX - DEPTH(IT)
IF (ZMIN.LE.ZZZ) GO TO 431
ZMIN = ZZZ
431 CONTINUE
CALL BLMOD( MAXPER)
C-----
C  AA  DESIGN CRATERS CREATED IN FIRST PERIOD  AA
C-----
DO 450 ICR = 1, NUMBH
IF (IPER(ICR).EQ.1) CALL CRPLT1 (ICR,1)
450 CONTINUE
C-----
C  AA  CRATERS CREATED AFTER THE FIRST DELAY PERIOD  AA
C-----
IPECR = 1
475 IPECR = IPECR + 1
DO 500 ICR = 1, NUMBH
IF (IPEX(ICR).NE.IPECR) GO TO 500
CALL CRPLT2(ICR)
CALL CRPLT1(ICR,IPECR)
500 CONTINUE
IF (IPECR.LT.MAXPER) GO TO 475
C-----
C  AAAA  O U T P U T  AAAA
C-----
WRITE(6,510)
510 FORMAT(1H1,//////////,40X,'P R O G R A M  V C R N ',//VCR02040
X 40X,' ',//VCR02050
X 30X,'W R I T T E N  F O R  T H E  D E S I G N  O F  T H E ',VCR02060
X //,30X,'B L A S T  I N  A N  U N D E R G R O U N D  S T O P ',VCR02070
X,'E',//,30X,'U S I N G  T H E  V E R T I C A L  C R A T E R ',VCR02080
X//,30X,'R E T R E A T  M E T H O D . ',//)
WRITE(6,511) TITLE
CALL QTIME(QDATE,QTIM,CLTIME,TCPU)
511 FORMAT(1H1,33X,A80,//)
WRITE(6,690) QDATE,QTIM
690 FORMAT(//////////,15X,'DATE : ',A8,//15X,'TIME : ',A8)VCR02140
WRITE(6,512) EXPTYP
512 FORMAT(1H0,' EXPLOSIVE USED : ',A15)VCR02150
WRITE(6,513) RHOE,LBS,INCH
513 FORMAT(1H0,' DENSITY : ',F6.4,2X,A4,'/CUBIC',A4)VCR02170
WRITE(6,590) DHOLE,INCH
590 FORMAT(1H0,' DIAMETER : ',F6.4,2X,A4)VCR02190

```



```

      WRITE(6,496)
496  FORMAT(' ',/////,51X,'MODIFIED INITIATION SEQUENCE',/
      X      51X,'-----',//
      X 40X,'HOLE NUMBER',30X,'DELAY PERIOD',/
      X 40X,'-----',30X,'-----',//)
      DO 498 I=1,NUMBH
      WRITE(6,497) I,IPER(I)
497  FORMAT(45X,12,38X,12,/)
498  CONTINUE
      WRITE(6,499) LBS
499  FORMAT(' ',/////,51X,'WEIGHT OF CHARGES IN THE BLAST',/
      X      51X,'-----',//
      X 40X,'HOLE NUMBER',30X,'WEIGHT (' ,A4,')',/
      X 40X,'-----',30X,'-----',//)
      DO 880 I = 1,NUMBH
      WRITE(6,881) I,WEIGHT(I)
881  FORMAT(45X,12,34X,F12.0)
880  CONTINUE
      DO 710 I = 1,NUMBH
      ALENG(I) = WEIGHT(I)/(12.0*PI*HOLE**2.0/4.0)
      IF(MSYSUN.EQ.1) ALENG(I) = ALENG(I)*12.0/0.1
      Z(I) = Z(I) - DOPT(I)
710  CONTINUE
      LONE = 1
      WRITE(70,701) NUMBH,LONE
701  FORMAT(15I5)
      DHOLE1 = 10*ADHOLE
      WRITE(70,702) DHOLE1
702  FORMAT(F10.2)
      WRITE(70,703) (Z(I),I=1,NUMBH)
      WRITE(70,703) (WEIGHT(I),I=1,NUMBH)
703  FORMAT(8F10.2)
      WRITE(70,703) (ALENG(I),I=1,NUMBH)
      WRITE(70,704) (IPER(I),I=1,NUMBH)
704  FORMAT(15I5)
      DO 1234 IOUT = 1,5
1234 ZBOUT(IOUT) = ZB(IOUT)
      WRITE(6,436) ZMAX
436  FORMAT(1H1,/////, ' ',50X,'PLAN VIEW OF THE BLAST',/
      X      51X,'-----',//
      X40X,'ELEVATIONS REPRESENTED BY THE PRINTOUT',/
      X40X,'-----',//
      X50X,' ',F12.1,' FT',//)
      WRITE(6,501) ZBOUT(1)
501  FORMAT(1H ,50X,'.....',F12.1,' FT',//)
      WRITE(6,502) ZBOUT(2)
502  FORMAT(1H ,50X,'::::::::::',F12.1,' FT',/
      X1H+,50X,'.....',//)
      WRITE(6,503) ZBOUT(3)
503  FORMAT(1H ,50X,'XXXXXXXXXX',F12.1,' FT',/
      X1H+,50X,'::::::::::',/
      X1H+,50X,'.....',//)
      WRITE(6,504) ZBOUT(4)
504  FORMAT(1H ,50X,'00000000',F12.1,' FT',/
      X1H+,50X,'XXXXXXXXXX',/

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VCR0221
 VCR0222
 VCR0223
 VCR0224
 VCR0225
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 VCR0240
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 VCR0256
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 VCR0260
 VCR0261
 VCR0262
 VCR0263
 VCR0264
 VCR0265
 VCR0266
 VCR0267
 VCR0268
 VCR0269
 VCR0270
 VCR0271
 VCR0272
 VCR0273
 VCR0274
 VCR0275
 VCR0276
 VCR0277
 VCR0278
 VCR0279
 VCR0280

X1H+,50X,':::':,/,	VCR02760
X1H+,50X,'.....',//)	VCR02770
WRITE(6,505) ZBOUT(5)	VCR02780
505 FORMAT(1H,50X,'AAAAAAAA',F12.1,' IT',/	VCR02790
X1H+,50X,'#####',/	VCR02800
X1H+,50X,'00000000',/	VCR02810
X1H+,50X,'XXXXXXXX',/	VCR02820
X1H+,50X,':::':,/,	VCR02830
X1H+,50X,'.....',//)	VCR02840
WRITE(6,437) XB(1),XB(11),XB(21),XB(31),XB(41),XB(51),XB(61),	VCR02850
XXB(71),XB(81),XB(91),XB(100)	VCR02860
437 FORMAT(8X,11(F4.0,6X))	VCR02870
WRITE(6,438)	VCR02880
438 FORMAT(10X,'+-----+-----+-----+-----+-----+-----+-----+-----+-----+-----+')	VCR02890
X'-----+-----+-----+-----+-----+-----+-----+')	VCR02900
DO 602 K = 1,5	VCR02910
DO 601 I = 1,100	VCR02920
DO 600 J = 1,100	VCR02930
C DO 550 K = 1, 5	VCR02940
IF (IBLOCK(I,J,K).EQ.0) GO TO 550	VCR02950
IWR(I,J) = K	VCR02960
C GO TO 600	VCR02970
550 CONTINUE	VCR02980
600 CONTINUE	VCR02990
601 CONTINUE	VCR03000
602 CONTINUE	VCR03010
DO 670 JP = 1,90,10	VCR03020
DO 610 I = 1, 100	VCR03030
IF(IWR(I,JP).NE.5) IFANCY(I)=' '	VCR03040
IF(IWR(I,JP).EQ.5) IFANCY(I)='A'	VCR03050
610 CONTINUE	VCR03060
WRITE(6,611) YB(JP),(IFANCY(I),I=1,100)	VCR03070
DO 620 I = 1, 100	VCR03080
IF(IWR(I,JP).NE.3) IFANCY(I)=' '	VCR03090
IF(IWR(I,JP).EQ.3) IFANCY(I)='#'	VCR03100
620 CONTINUE	VCR03110
WRITE(6,612) (IFANCY(I),I=1,100)	VCR03120
DO 613 I = 1,100	VCR03130
IF(IWR(I,JP).GE.4) IFANCY(I) = '0'	VCR03140
IF(IWR(I,JP).LT.4) IFANCY(I) = ' '	VCR03150
613 CONTINUE	VCR03160
WRITE(6,612) (IFANCY(I),I=1,100)	VCR03170
DO 614 I = 1,100	VCR03180
IF(IWR(I,JP).GE.3) IFANCY(I) = 'X'	VCR03190
IF(IWR(I,JP).LT.3) IFANCY(I) = ' '	VCR03200
614 CONTINUE	VCR03210
WRITE(6,612) (IFANCY(I),I = 1,100)	VCR03220
DO 615 I = 1,100	VCR03230
IF(IWR(I,JP).GE.2) IFANCY(I) = ':'	VCR03240
IF(IWR(I,JP).LT.2) IFANCY(I) = ' '	VCR03250
615 CONTINUE	VCR03260
WRITE(6,612) (IFANCY(I),I= 1,100)	VCR03270
DO 616 I = 1,100	VCR03280
IF(IWR(I,JP).GE.1) IFANCY(I) = '.'	VCR03290
IF(IWR(I,JP).LT.1) IFANCY(I) = ' '	VCR03300

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616 CONTINUE
      WRITE(6,612) (IFANCY(I),I = 1,100)
611 FORMAT(1H ,F4.0,' ' ,100A1)
612 FORMAT(1H+,4X ,' ' ,100A1)
      JF=JP+1
      JL=JP+9
      DO 660 JJP = JF,JL
      DO 640 I = 1, 120
        IF(IWR(I,JJP).NE.5) IFANCY(I)=' '
        IF(IWR(I,JJP).EQ.3) IFANCY(I)='A'
640 CONTINUE
      WRITE(6,641) (IFANCY(I),I=1,100)
      DO 694 I = 1, 100
        IF(IWR(I,JJP).NE.5) IFANCY(I)=' '
        IF(IWR(I,JJP).EQ.5) IFANCY(I)='#'
694 CONTINUE
      WRITE(6,642) (IFANCY(I),I=1,100)
      DO 643 I = 1,100
        IF(IWR(I,JJP).GE.4) IFANCY(I) = '0'
        IF(IWR(I,JJP).LT.4) IFANCY(I) = ' '
643 CONTINUE
      WRITE(6,642) (IFANCY(I),I=1,100)
      DO 644 I = 1,100
        IF(IWR(I,JJP).GE.3) IFANCY(I) = 'X'
        IF(IWR(I,JJP).LT.3) IFANCY(I) = ' '
644 CONTINUE
      WRITE(6,642) (IFANCY(I),I = 1,100)
      DO 645 I = 1,100
        IF(IWR(I,JJP).GE.2) IFANCY(I) = ':'
        IF(IWR(I,JJP).LT.2) IFANCY(I) = ' '
645 CONTINUE
      WRITE(6,642) (IFANCY(I),I= 1,100)
      DO 646 I = 1,100
        IF(IWR(I,JJP).GE.1) IFANCY(I) = '.'
        IF(IWR(I,JJP).LT.1) IFANCY(I) = ' '
646 CONTINUE
      WRITE(6,642) (IFANCY(I),I = 1,100)
641 FORMAT(1H ,4X ,' ' ,100A1)
642 FORMAT(1H+,4X ,' ' ,100A1)
660 CONTINUE
670 CONTINUE
      WRITE(6,9436) ZMAX,(ZBOUT(IOUT),IOUT=1,5)
9436 FORMAT(1H1,////////,' ',50X,'PLAN VIEW OF THE BLAST',/
      X
      X1X,'-----',///
      X40X,'ELEVATIONS REPRESENTED BY THE NUMBERS OF THE PRINTOUT',/
      X40X,'-----',///
      X50X,'NUMBER 0',F12.1,' FT',//
      X50X,'NUMBER 1',F12.1,' FT',//
      X50X,'NUMBER 2',F12.1,' FT',//
      X50X,'NUMBER 3',F12.1,' FT',//
      X50X,'NUMBER 4',F12.1,' FT',//
      X50X,'NUMBER 5',F12.1,' FT',///)
      WRITE(6,9437) XB(1),XB(11),XB(21),XB(31),XB(41),XB(51),XB(61),
      XXB(71),XB(81),XB(91),XB(100)
9437 FORMAT(8X,11(F4.0,6X))

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VCR03310
 VCR03320
 VCR03330
 VCR03340
 VCR03350
 VCR03360
 VCR03370
 VCR03380
 VCR03390
 VCR03400
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 VCR03770
 VCR03780
 VCR03790
 VCR03800
 VCR03810
 VCR03820
 VCR03830
 VCR03840
 VCR03850

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WRITE(6,9438)
9438 FORMAT(10X,'-----')
X'-----'
DO 9602 K = 1,5
DO 9601 I = 1,100
DO 9600 J = 1,100
C DO 550 K = 1, 5
IF (IBLOCK(I,J,K).EQ.0) GO TO 9550
IWR(I,J) = K
C GO TO 600
9550 CONTINUE
9600 CONTINUE
9601 CONTINUE
9602 CONTINUE
DO 9670 JP = 1,90,10
WRITE(6,9655) YB(JP),(IWR(I,JP),I=1,100)
9655 FORMAT(1H,F4.0,' + ',100I1)
WRITE(6,9660) ((IWR(I,J),I=1,100),J=JP+1,JP+9)
9660 FORMAT(1H,4X,' | ',100I1)
9670 CONTINUE
DO 9995 J = 1,100
WRITE(77,7777) (IWR(I,J),I=1,100)
C WRITE(77,777) (IWR(I,J),J=81,100)
C 777 FORMAT(20I1)
7777 FORMAT(80I1)
9995 CONTINUE
C -----
C ** GIVE SUMMARY OF THE REQUIRED SUPPLIES **
C -----
TW = 0.0
DO 9100 I = 1,NUMBH
TW = TW + WL1GHT(I)
9100 CONTINUE
WRITE(6,9101) TW,LBS
9101 FORMAT(1H1,45X,'SUMMARY',/45X,'-----',///,25X,'TOTAL WEIGHT OF'
X,' EXPLOSIVE :',F10.0,2X,A4)
WRITE(6,9102)
9102 FORMAT(1H0,25X,'DELAY NUMBER',40X,'QUANTITY',/
X',25X,'-----',40X,'-----')
MAXPER = 0
DO 9105 I = 1,NUMBH
IF(IPER(I).GT.MAXPER) MAXPER=IPER(I)
9105 CONTINUE
DO 9110 I = 1,MAXPER
MM = 0
DO 9109 J = 1,NUMBH
IF(IPER(J).EQ.I) MM = MM + 1
9109 CONTINUE
WRITE(6,9115) I,MM
9115 FORMAT(1H0,30X,12.48X,12)
9110 CONTINUE
CALL CHARGE1(MDOUPD)
WRITE(6,9200) FT,LBS
9200 FORMAT(1H1,45X,'INSTRUCTIONS FOR LOADING',/
X',45X,'-----',///

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All

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X10X,'HOLE NUMBER',10X,'CHARGE LOCATION',10X,'CHARGE WEIGHT',10X, VCR04410
X'DELAY NUMBER',/10X,'',10X,'',10X,'',10X,'',10X,'',10X,'', VCR04420
XA4.'',/10X,'',10X,'',10X,'',10X,'',10X,'',10X,'',10X,'', VCR04430
X'-----',10X,'-----') VCR04440
DO 9260 I = 1,NUMBH VCR04450
WRITE(6,9250) I,BBOUPO(I),WEIGHT(I),IPER(I) VCR04460
9250 FORMAT(1H0,15X,12,19X,F5.0,19X,F5.0,17X,12) VCR04470
9260 CONTINUE VCR04480
1000 STOP VCR04490
END VCR04500
SUBROUTINE READER VCR04510
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC VCR04520
C VCR04530
C PURPOSE : TO READ GENERAL DATA FOR THE DESIGN OF THE VCR BLAST VCR04540
C THE DATA ARE READ FROM THE FOLLOWING UNITS : VCR04550
C UNIT 7 - TERMINAL ( INTERACTIVELY ) VCR04560
C UNIT 8 - DISK FILE WITH THE DATA FOR THE CRATERING CURVES VCR04570
C UNIT 9 - DISK FILE WITH DATA FOR THE SLOPE VCR04580
C UNIT 10 - INITIATION SEQUENCE VCR04590
C UNIT 11 - DISK FILE WITH DATA FOR THE VIBRATION CHECKS. THIS FILE VCR04600
C IS CREATED BY THE COMPUTER IN A PREVIOUS RUN. VCR04610
C VCR04620
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC VCR04630
C VCR04640
C VARIABLES : VCR04650
C BBOUCH : DEPTH OF CONTAINED CHARGE (SPHERICAL) VCR04660
C BBOUPO : CHARGE LOCATION IN THE BOREHOLE VCR04670
C DELTA : DEPTH RATIO VCR04680
C DELTAK : DEPTH RATIO VCR04690
C DHOLE : DIAMETER OF BOREHOLE VCR04700
C ELEV : ELEVATION OF THE FREE FACE VCR04710
C EXPTYB : EXPLOSIVE TYPE VCR04720
C EXPTYP : EXPLOSIVE TYPE VCR04730
C IPER(I) : DELAY PERIOD OF CHARGE I VCR04740
C MSYSUN : 1 METRIC VCR04750
C 2 IMPERIAL VCR04760
C NP1 : NUMBER OF POINTS IN SCALED CRATER DEPTH - DEPTH VCR04770
C RATIO CURVE (SPHERICAL) VCR04780
C NP2 : NUMBER OF POINTS IN SCALED CRATER RADIUS - DEPTH VCR04790
C RATIO CURVE (SPHERICAL) VCR04800
C VCR04810
C NUMBH : NUMBER OF HOLES IN THE BLAST VCR04820
C KBOUL : DENSITY OF THE EXPLOSIVE VCR04830
C SCDEPT : SCALED DEPTH OF BURIAL FOR SPHERICAL CHARGES VCR04840
C SCRAD : SCALED RADIUS FOR SPHERICAL VCR04850
C SCROP : OPTIMUM SCALED RADIUS VCR04860
C TITLE : TITLE VCR04870
C X(I) : X COORDINATE OF HOLE I VCR04880
C XMAX : MAX LOCAL LENGTH (USED TO DETERMINE LENGTH OF BLOCK) VCR04890
C XMIN : MIN LOCAL LENGTH VCR04900
C XPIL1,XPIL2,XPIL3 : X COORD OF POINTS DEFINING PILLAR VCR04910
C Y(I) : Y COORDINATE OF HOLE I VCR04920
C YMAX : MAX LOCAL WIDTH (USED TO DETERMINE LENGTH OF BLOCK) VCR04930
C YMIN : MIN LOCAL WIDTH VCR04940
C YPIL1,YPIL2,YPIL3 : Y COORD OF POINTS DEFINING PILLAR VCR04950

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A12

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C      Z(1) : Z COORDINATE OF HOLE 1
C      ZMAX : MAX LOCAL DEPTH (USED TO DETERMINE LENGTH OF BLOCK)
C      YMIN : MIN LOCAL DEPTH
C      ZPIL1,ZPIL2,ZPIL3 : Z COORD OF POINTS DEFINING PILLAR
C
C      CHARACTER A1 KODE1
C      CHARACTER A4 LBS,INCH,FT
C      CHARACTER A15 EXPTYP,EXPTYB
C      CHARACTER A80 TITLE
C
C-----
C      **      INCLUDE COMMONS      **
C-----
C      COMMON /RDRDT1/ DCONCH,WTCRGS,WSTRTN,SCDEPT(50),DELTA(50),
XSCRAP(50),DHOLE,X(50),Y(50),Z(50),XVCHK(10),YVCHK(10),ZVCHK(10),
X,PPVALL(10),AKFAC,AMEAC,XPIL1(10),XPIL2(10),XPIL3(10),YPIL1(10),
XPIL2(10),YPIL3(10),ZPIL1(10),ZPIL2(10),ZPIL3(10),PPVPAL,WSTR,
XXMAX,XMIN,YMAX,YMIN,ZMAX,ZMIN,DELTA(50),RHOE
C      COMMON/RDRDT2/ NP1,NP2,NUMBH,NCHK,NUMPIL,INIT(50),MSYSUN
C      COMMON/ISEQ/ IPER(50),KK
C      COMMON/CHARGE/ WEIGHT(50),DOPT(50),RCR(50),DEPTH(50),SCRUP
C      COMMON/TYPE/EXPTYP,EXPTYB
C      COMMON/TT/TITLE
C      COMMON/REFER/ XREFER,YREFER,ZREFER,STANGR,STLENG,STWIDT
X,STDEPT
C      COMMON/UNALF/ LBS,INCH,FT
C-----
C      **      READ CRACKING CHARACTERISTICS      **
C-----
C      NUMPIL=0
C      WRITE (7,9)
C      9 FORMAT(' ENTER TYPE OF EXPLOSIVE USED IN THE TESTS :')
C      READ (7,1009) EXPTYP
C      1009 FORMAT(A15)
C      WRITE (7,1010)
C      1010 FORMAT(' ENTER SYSTEM OF UNITS YOU ARE USING :',/
X'      (1) M E T R I C',/
X'      (2) I M P E R I A L ')
C      READ(7,A) MSYSUN
C      IF (MSYSUN.EQ.1) GO TO 1020
C      LBS=' LBS'
C      FT = ' FT '
C      INCH = ' INCH'
C      GO TO 1030
C      1020 LBS = ' KG '
C      FT = ' M '
C      INCH = ' CM '
C      1030 WRITE (7,10) FT,LBS
C      10 FORMAT (' ENTER DEPTH OF CONTAINED CHARGE ('.A4,')',/
X'      WEIGHT OF EXPLOSIVE ('.A4,')')
C      READ (7,A) DCONCH, WTCRGS
C      WRITE (7,11)

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11 FORMAT (' WHAT IS THE WEIGHT STRENGTH OF THE EXPLOSIVE',/
X      ' RELATIVE TO AN/FO ?')
      READ (7,A) WSTRTH
C-----
C  **      READ CRATERING CURVES      **
C-----
      WRITE (7,12)
12 FORMAT (' DO YOU WANT TO INPUT NEW CRATERING CURVES ? ')
      READ (7,13) KODE
13 FORMAT (1A1)
      IF (KODE.EQ.'N') GO TO 30
      WRITE (7,14)
14 FORMAT (' ENTER NUMBER OF POINTS TO DESIGN THE ',/
X      ' SCALED CRATER DEPTH - DEPTH RATIO',/
X      ' CURVE : ')
      READ (7,A) NP1
      WRITE (8,15) NP1
15 FORMAT (I5)
      WRITE (7,16)
16 FORMAT(' ENTER SCALED DEPTH, DEPTH RATIO ',/
X      ' FOR EACH POINT OF THE CURVE.')
      DO 19 I = 1, NP1
      READ (7,A) SCDEPT(I), DELTA(I)
      WRITE(8,18) SCDEPT(I), DELTA(I)
18 FORMAT(2F10.4)
19 CONTINUE
      WRITE(7,20)
20 FORMAT(' ENTER NUMBER OF POINTS TO DESIGN ',/
X      ' THE SCALED CRATER RADIUS - DEPTH RATIO',/
X      ' CURVE.')
      READ (7,A) NP2
      WRITE(8,15) NP2
      WRITE(7,26)
26 FORMAT(' ENTER SCALED CRATER RADIUS, DEPTH RATIO',/
X      ' FOR EACH POINT OF THE CURVE.')
      DO 29 I = 1, NP2
      READ (7,A) SCRAD(I), DELTAR(I)
      WRITE(8,18) SCRAD(I), DELTAR(I)
29 CONTINUE
      GO TO 40
C-----
C  **      READ CURVES FROM FILE  **
C-----
30 READ (8,15) NP1
      READ (8,18) ((SCDEPT(I), DELTA(I)), I=1, NP1)
      READ (8,15) NP2
      READ (8,18) ((SCRAD(I), DELTAR(I)), I=1, NP2)
40 CONTINUE
C-----
C  **      READ DATA OF THE SLOPE  **
C-----
      WRITE(7,201) INCH
201 FORMAT (' ENTER THE DIAMETER OF THE BLASTHOLES (' ,A4,') :')
      READ (7,A) DHOLE
      WRITE(7,202)

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VCR05510

VCR05520

VCR05530

VCR05540

VCR05550

VCR05560

VCR05570

VCR05580

VCR05590

VCR05600

VCR05610

VCR05620

VCR05630

VCR05640

VCR05650

VCR05660

VCR05670

VCR05680

VCR05690

VCR05700

VCR05710

VCR05720

VCR05730

VCR05740

VCR05750

VCR05760

VCR05770

VCR05780

VCR05790

VCR05800

VCR05810

VCR05820

VCR05830

VCR05840

VCR05850

VCR05860

VCR05870

VCR05880

VCR05890

VCR05900

VCR05910

VCR05920

VCR05930

VCR05940

VCR05950

VCR05960

VCR05970

VCR05980

VCR05990

VCR06000

VCR06010

VCR06020

VCR06030

VCR06040

VCR06050


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202 FORMAT(' ENTER NUMBER OF HOLES IN THE BLAST :')
      READ (7,A) NUMBH
C-----
C  AA  READ X,Y COORDINATES OF THE HOLES AT A PARTICULAR LEVEL Z  AA
C-----
      WRITE(7,209)
209 FORMAT(' ENTER THE ELEVATION OF THE FREE FACE OF THE BLAST :')
      READ(7,A) ELEV
      REWIND 51
      READ(51,519) TITLE
      READ(51,520) XREFLX,YREFLX,ZREFLX
      READ(51,520) STLENG,STWIDT,STDEPT
      READ(51,520) STANGR
      STANGR=3.14159*STANGR/180.0
519 FORMAT(A80)
520 FORMAT(4F10.2)
      CALL PLVIEW(LELV,X,Y,Z,NUMBH)
      WRITE(9,210) ((X(I),Y(I),Z(I)), I = 1, NUMBH)
210 FORMAT (3F15.5)
C-----
C  AA  READ DATA FOR VIBRATION CHECKS  AA
C  SPECIFY POINTS OF PARTICULAR INTEREST AND ACCEPTABLE
C  VIBRATIONS IN THESE POINTS.
C-----
      WRITE (7,250)
250 FORMAT(' THE FOLLOWING DATA ARE FOR CHECKING VIBRATION',/
X      ' LEVELS AT PILLARS AND OTHER PARTICULAR POINTS',/
X      ' OF INTEREST ....',/
X      ' ARE THESE NEW OR PREVIOUS DATA ?')
      READ (7,13) KODE
      IF (KODE.EQ.'P') GO TO 490
      WRITE(7,270)
270 FORMAT(' ENTER THE NUMBER OF POINTS IN WHICH VIBRATIONS ARE',/
X      ' TO BE CHECKED:')
      READ (7,A) NCHK
      IF(NCHK.EQ.0) GO TO 331
      WRITE(11,280)
280 FORMAT(15)
      WRITE(7,300)
300 FORMAT(' ENTER SPECIFIC POINTS IN WHICH VIBRATIONS WILL BE',/
X      ' CHECKED.',/
X      ' ( EACH POINT MUST BE SPECIFIED BY ITS COORDINATES SEPARATED',/
X      ' BY COMMAS, AND THE MAXIMUM ACCEPTABLE LEVEL OF PEAK PARTICLE',/
X      ' VELOCITY. E.G. 12.4,12.6,14.2,10.0)')
      DO 315 I = 1, NCHK
      READ (7,A) XVCHK(I), YVCHK(I), ZVCHK(I), PPVALL(I)
C-----
C  AA  CONVERT TO LOCAL COORDINATES  AA
C-----
      XVCHK(I) = XVCHK(I) - XREFLX
      YVCHK(I) = YVCHK(I) - YREFLX
      ZVCHK(I) = ZVCHK(I) - ZREFLX
      XC = XVCHK(I)*ACOS(STANGR) + YVCHK(I)*ASIN(STANGR)
      YC = -XVCHK(I)*ASIN(STANGR) + YVCHK(I)*ACOS(STANGR)
      XVCHK(I) = XC

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VCR06060
VCR06070
VCR06080
VCR06090
VCR06100
VCR06110
VCR06120
VCR06130
VCR06140
VCR06150
VCR06160
VCR06170
VCR06180
VCR06190
VCR06200
VCR06210
VCR06220
VCR06230
VCR06240
VCR06250
VCR06260
VCR06270
VCR06280
VCR06290
VCR06300
VCR06310
VCR06320
VCR06330
VCR06340
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VCR06360
VCR06370
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VCR06390
VCR06400
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VCR06490
VCR06500
VCR06510
VCR06520
VCR06530
VCR06540
VCR06550
VCR06560
VCR06570
VCR06580
VCR06590
VCR06600

A15

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      YVCHK(I) = YC
      WRITE(11,310) XVCHK(I), YVCHK(I), ZVCHK(I), PPVALL(I)
310  FORMAT(4F15.5)
      CONTINUE
      WRITE(7,320)
320  FORMAT(' ENTER THE SITE FACTORS K, M FOR THE CALCULATION OF THE
      X' PEAK PARTICLE',// VELOCITY :')
      READ (7,A) AKEAC, AMEAC
      WRITE(11,330) AKEAC, AMEAC
330  FORMAT (2F15.5)
331  CONTINUE
C-----
C  AA      ENTER DATA FOR PILLARS      AA
C-----
      WRITE (7,430)
430  FORMAT(' ARE THERE ANY PILLARS IN WHICH YOU WOULD LIKE TO CHECK
      X, 'VIBRATIONS ?')
      READ (7,431) KODE1
431  FORMAT (1A1)
      IF (KODE1.EQ.'N') GO TO 490
      WRITE(7,440)
440  FORMAT(' ENTER NUMBER OF PILLARS :')
      READ (7,A) NUMPIL
      WRITE(11,450) NUMPIL
450  FORMAT(I5)
      DO 480 I = 1, NUMPIL
      WRITE(7,460) I
460  FORMAT(' ENTER X, Y, Z, COORDINATES OF THE 1ST POINT OF PILLAR',
      X' NO.', 13)
      READ (7,A) XPIL1(I), YPIL1(I), ZPIL1(I)
C-----
C  AA      CONVERT TO LOCAL COORDINATES      AA
C-----
      XPIL1(I) = XPIL1(I) - XKLEEK
      YPIL1(I) = YPIL1(I) - YKLEEK
      ZPIL1(I) = ZPIL1(I) - ZREFER
      XC = XPIL1(I)*ACOS(STANGK) + YPIL1(I)*ASIN(STANGK)
      YC = -XPIL1(I)*ASIN(STANGK) + YPIL1(I)*ACOS(STANGK)
      XPIL1(I) = XC
      YPIL1(I) = YC
      WRITE(11,470) XPIL1(I), YPIL1(I), ZPIL1(I)
470  FORMAT (3F15.5)
      WRITE(7,471) I
471  FORMAT(' ENTER X, Y, Z, COORDINATES OF THE 2ND POINT OF PILLAR',
      X' NO.', 13)
      READ (7,A) XPIL2(I), YPIL2(I), YPIL2(I)
C-----
C  AA      CONVERT TO LOCAL COORDINATES      AA
C-----
      XPIL2(I) = XPIL2(I) - XREFER
      YPIL2(I) = YPIL2(I) - YREFER
      ZPIL2(I) = ZPIL2(I) - ZREFER
      XC = XPIL2(I)*ACOS(STANGK) + YPIL2(I)*ASIN(STANGK)
      YC = -XPIL2(I)*ASIN(STANGK) + YPIL2(I)*ACOS(STANGK)
      XPIL2(I) = XC

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```

      YPIL2(I) = YC
      WRITE(11,470) XPIL2(I), YPIL2(I), ZPIL2(I)
      WRITE(7,473) I
473  FORMAT(' ENTER X, Y, Z, COORDINATES OF THE 3RD POINT OF PILLAR',
      X' NO.', I3)
      READ (7,A) XPIL3(I), YPIL3(I), ZPIL3(I)
C-----
C  AA  CONVERT TO LOCAL COORDINATES  AA
C-----
      XPIL3(I) = XPIL3(I) - XREFER
      YPIL3(I) = YPIL3(I) - YREFER
      ZPIL3(I) = ZPIL3(I) - ZREFER
      XC = XPIL3(I)*ACOS(STANGK) + YPIL3(I)*ASIN(STANGK)
      YC = -XPIL3(I)*ASIN(STANGK) + YPIL3(I)*ACOS(STANGK)
      XPIL3(I) = XC
      YPIL3(I) = YC
      WRITE(11,470) XPIL3(I), YPIL3(I), ZPIL3(I)
480  CONTINUE
      WRITE(7,482)
482  FORMAT(' ENTER MAXIMUM ACCEPTABLE LEVEL FOR PEAK PARTICLE ',
      X' VELOCITY ',/ ' IN THE PILLAR')
      READ (7,A) PPVAL
      WRITE(11,484) PPVAL
484  FORMAT(I5)
      GO TO 500
C-----
C  AA  READ FROM FILE  AA
C-----
490  IF (KODE.NE.'P') GO TO 500
      READ (11,280) NCHK
      DO 420 I = 1, NCHK
      READ (11,310) XVCHK(I), YVCHK(I), ZVCHK(I), PPVALL(I)
420  CONTINUE
      READ(11,450) NUNPIL
      DO 498 I = 1, NUNPIL
      READ(11,470) XPIL1(I), YPIL1(I), ZPIL1(I)
      READ(11,470) XPIL2(I), YPIL2(I), ZPIL2(I)
      READ(11,470) XPIL3(I), YPIL3(I), ZPIL3(I)
498  CONTINUE
      READ(11,484) PPVAL
500  CONTINUE
C-----
C  AA  ENTER DATA FOR THE EXPLOSIVE WHICH IS USED  AA
C-----
      WRITE(7,509)
509  FORMAT(' ENTER TYPE OF EXPLOSIVE TO BE USED :')
      READ(7,1509) EXPTYP
1509  FORMAT(A15)
      WRITE(7,507)
507  FORMAT(' WHAT IS THE WEIGHT STRENGTH OF THE EXPLOSIVE YOU ARE',
      X' USING ?')
      READ (7,A) WSTK
C-----
      WRITE(7,508)
508  FORMAT(' WHAT IS THE DENSITY OF THE EXPLOSIVE YOU ARE USING ?',/

```


A18

[illegible]

[illegible]

C AA FIND CRATERS AT PERIOD L AA

C-----
 DO 70 NI = 1, NUMBH
 IF (IPER(NI).GT.L) GO TO 60
 BURMIN(NI) = BURDEN(ICK,N1)
 GO TO 70
 60 BURMIN(NI) = BIG
 70 CONTINUE

C-----
 C AA FIND MINIMUM BURDEN AA

C-----
 BMIN = BURMIN(1)
 DO 30 NI = 2, NUMBH
 IF (BMIN.GT.BURMIN(NI)) BMIN = BURMIN(NI)
 30 CONTINUE

C-----
 C AA IF BMIN GREATER THAN DEPTH OF CONTAINED CHARGE, POINT DOES NOT
 AFFECT DETONATION

C-----
 DCONT = EFAC1K * WEIGHT(ICK)AA(1.0/3.0)
 IF (BMIN.GT.DCONT) GO TO 2222

C-----
 C AA FIND CRATER RADIUS FOR MINIMUM BURDEN AA

C-----
 DEPR = BMIN / DCONT

C-----
 C AA FIND SCALED RADIUS AT THIS DEPTH RATIO AA

C-----
 DO 40 MI = 2, NP2
 IF ((DELTA(MI).GE.DEPR).AND.(DELTA(MI-1).LE.DEPR)) GO TO 35
 40 CONTINUE
 35 SCR = SCRAD(MI-1) + (DEPR - DELTA(MI-1))/(DELTA(MI)
 XDELTA(MI-1))A(SCRAD(MI)-SCRAD(MI-1))
 RADIUS = SCR * WEIGHT(ICK)AA(1.0/3.0)

C-----
 C AA CALCULATE SLANT DISTANCE AA

C-----
 SLANTD = (RADIUSAA2.0 + BMINAA2.0)AA0.5
 DO 2020 II = 2, 99
 DO 2010 JJ = 2, 99
 DO 2000 KKK = 1, 5

C-----
 C AA CHECK IF POINT (II,JJ,KKK) IN PERIOD L IS INSIDE THE MASS
 AND THEREFORE IT DOES NOT AFFECT THE DETONATION AA

C-----
 IF(1TIME(II,JJ,KKK).GT.L)GO TO 2000
 I11=II+1
 JJ1=JJ+1
 I1H=II-1
 JJH=JJ-1
 IF((IBLOCK(I11,JJ,KKK).NE.0).AND.(IBLOCK(II,JJ1,KKK).NE.0).AND.
 X(IBLOCK(I1H,JJ,KKK).NE.0).AND.(IBLOCK(II,JJH,KKK).NE.0))
 XGO TO 2000

C-----
 C AA POINT MAY AFFECT DETONATION. CALCULATE DISTANCE BETWEEN POINT

C AND THE CENTRE OF THE CHARGE.

C-----
 ZCHARG = Z(ICR)-DOPT(ICR)
 CALL DISTPT(X(ICR),Y(ICR),ZCHARG,XB(11),YB(JJ),ZB(KKK),
 X DIST)

C ** BLOCKS FURTHER THAN THE SLANT DISTANCE DO NOT AFFECT DETUNATION **

C-----
 IF(DIST.GT.SLANTD) GO TO 2010
 DO 1025 I1 = 1,100
 DO 1020 J1 = 1,100
 KK1 = 1
 IF((XB(11).GT.X(ICR)).AND.(XB(11).GT.(XB(11)+DX))) GO TO 1020
 IF((XB(11).GT.X(ICR)).AND.(XB(11).LT.(X(ICR)-DX))) GO TO 1020
 IF((XB(11).LT.X(ICR)).AND.(XB(11).LT.(XB(11)-DX))) GO TO 1020
 IF((XB(11).LT.X(ICR)).AND.(XB(11).GT.(X(ICR)+DX))) GO TO 1020
 IF((YB(JJ).GT.Y(ICR)).AND.(YB(J1).GT.(YB(JJ)+DY))) GO TO 1020
 IF((YB(JJ).GT.Y(ICR)).AND.(YB(J1).LT.(Y(ICR)-DY))) GO TO 1020
 IF((YB(JJ).LT.Y(ICR)).AND.(YB(J1).LT.(YB(JJ)-DY))) GO TO 1020
 IF((YB(JJ).LT.Y(ICR)).AND.(YB(J1).GT.(Y(ICR)+DY))) GO TO 1020
 CALL DISPLN(XB(11),YB(JJ),X(ICR),
 X Y(ICR),XB(11),YB(J1),DIS,IBUG)
 IF(IBUG.EQ.1) GO TO 2010

C-----
 C ** TAKE ZONE OF THICKNESS DX **

C-----
 IF (DIS.GT.(DX/2.)) GO TO 1020
 DO 1000 KK1 = 1,5
 IF(IBLOCK(I1,J1,KK1).NE.0) GO TO 1000

C-----
 C ** TRANSLATE COORDINATES **

C-----
 XS(1) = 0.0
 YS(1) = Z(ICR) - DOPT(ICR)
 XS(2) = 0.0
 YS(2) = Z(ICR)
 XS(3) = (ABS(X(ICR)-XB(11))**2.0+
 X ABS(Y(ICR)-YB(JJ))**2.0)**0.5
 AAAA=-XS(3)
 IF(XB(11).LT.X(ICR)) XS(3)=AAAA
 IF((XB(11).EQ.X(ICR)).AND.(YB(JJ).LT.Y(ICR))) XS(3)=AAAA
 YS(3) = Z(ICR)
 XS(4) = XS(3)
 YS(4) = ZB(KKK)
 XSO=(ABS(X(ICR)-XB(11))**2.0+ABS(Y(ICR)-YB(J1))**2.0)**0.5
 AAAA0=-XSO
 IF(XB(11).LT.X(ICR)) XSO = AAAA0
 IF((XB(11).EQ.X(ICR)).AND.(YB(J1).LT.YB(1CR))) XSO = AAAA0
 YSO = ZB(KK1)
 CALL INSIDE(4,XS,YS,XSO,YSO,KKODE)
 IF(KKODE.EQ.0) GO TO 1000
 IBLOCK(I1,J1,KK1) = KK1
 ITIME(I1,J1,KK1) = IPER(ICR)

1000 CONTINUE

1020 CONTINUE

VR09991
 VR09992
 VR09993
 VR09994
 VR09995
 VR09996
 VR09997
 VR09998
 VR09999
 VR10000
 VR10001
 VR10002
 VR10003
 VR10004
 VR10005
 VR10006
 VR10007
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 VR10045

A22

1025 CONTINUE	VCR10460
2000 CONTINUE	VCR10470
2010 CONTINUE	VCR10480
2020 CONTINUE	VCR10490
2222 RETURN	VCR10500
END	VCR10510
SUBROUTINE INSIDE (NPN,X,Y,XO,YO,KODE)	VCR10520
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC	VCR10530
C	VCR10540
C PURPOSE :	VCR10550
C TO DETERMINE IF A POINT LIES WITHIN A CLOSED	VCR10560
C	VCR10570
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC	VCR10580
C BOUNDARY	VCR10590
C NPN : THE NUMBER OF POINTS DEFINING THE CLOSED POLYGON	VCR10600
C X,Y : THE ARRAYS WITH THE ABOVE POINT COORDINATES	VCR10610
C KODE: =-1 THE POINT IS INSIDE BOUNDARY	VCR10620
C KODE: =0 THE POINT IS OUTSIDE BOUNDARY	VCR10630
C KODE: =1 THE POINT IS ON THE INSIDE BOUNDARY IN VECTOR (1-1,1)	VCR10640
C-----	VCR10650
C DIMENSION X(10),Y(10)	VCR10660
C	VCR10670
C MINIMUM POINTS 3 MAXIMUM POINTS 999	VCR10680
C-----	VCR10690
C IF (NPN.LE.2.OR.NPN.GT.1999) RETURN	VCR10700
PP=3.141592	VCR10710
KODE=-2	VCR10720
C	VCR10730
X1=X(NPN)-XO	VCR10740
Y1=Y(NPN)-YO	VCR10750
SUM=0.0	VCR10760
NTELOS=NPN	VCR10770
DO 401 KPN=1,NTELOS	VCR10780
ANGL=0.0	VCR10790
X2=X(KPN)-XO	VCR10800
Y2=Y(KPN)-YO	VCR10810
IF (X2.EQ.X1.AND.Y2.EQ.Y1) GO TO 401	VCR10820
ANOM=X1*Y2-X2*Y1	VCR10830
DENOM=X1*X2+Y1*Y2	VCR10840
IF (DENOM.NE.0.0) ANGL=ATAN(ANOM/DENOM)	VCR10850
IF (DENOM.EQ.0.0) ANGL=PP/2.	VCR10860
IF (DENOM.EQ.0.0.AND.ANOM.LT.0.0) ANGL=-PP/2.	VCR10870
X1=X2	VCR10880
Y1=Y2	VCR10890
IF (DENOM.LT.0.0.AND.ANGL.EQ.0.0) KODE=KPN	VCR10900
IF (KODE.EQ.KPN) RETURN	VCR10910
C-----	VCR10920
C IF ANGL=180. THE POINT FALLS ON THE AREA BOUNDARY	VCR10930
C-----	VCR10940
IF (ANGL.LT.0.0.AND.ANOM.GT.0.0) ANGL=ANGL+PP	VCR10950
IF (ANGL.GT.0.0.AND.ANOM.LT.0.0) ANGL=ANGL-PP	VCR10960
SUM=SUM+ANGL	VCR10970
401 CONTINUE	VCR10980
P22 = 2.0* PP	VCR10990
P44 = 4.0* PP	VCR11000

A23

[illegible]


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XSCRAD(50),DHOLE,X(50),Y(50),Z(50),XVCHK(10),YVCHK(10),ZVCHK(10) VCR12110
X,PPVALL(10),AKFAC,AMEAC,XPIL1(10),XPIL2(10),XPIL3(10),YPIL1(10), VCR12120
XPIL2(10),YPIL3(10),ZPIL1(10),ZPIL2(10),ZPIL3(10),PPVPAL,WSTR, VCR12130
XXMAX,XMIN,YMAX,YMIN,ZMAX,ZMIN,DELTAR(50),RHOE VCR12140
COMMON/RDRDT2/ NP1,NP2,NUMBH,NCHK,NUMPIL,INIT(50),MSYSUN VCR12150
COMMON/CHARGE/WEIGHT(50),DOPT(50),RCR(50),DEPTH(50),SCROP VCR12160
COMMON/FLY/IFLY(50) VCR12170
COMMON/DELT/DELTO,EFACTR VCR12180
COMMON/ISEQ/ IPER(50),KK VCR12190
COMMON/REFER/ XREFER,YREFER,ZREFER,STANGR,STLENG,STWIDT VCR12200
X .STDEPT VCR12210
DIMENSION ALOAD(50),PPV(10),PPVPIL(10),WEIGMX(50),ID(20) VCR12220
WEIGMX(1) = 100000.0 VCR12230
ICH = 0 VCR12240
DO 2 1 = 1, 20 VCR12250
ID(1)=0 VCR12260
2 CONTINUE VCR12270
C----- VCR12280
C ** FIND CHARGES DETONATING IN THE SAME PERIOD ** VCR12290
C----- VCR12300
KK = 0 VCR12310
DO 100 1A = 1, NUMBH VCR12320
IF (IPER(1A).NE.IPER(1FIRST)) GO TO 100 VCR12330
C----- VCR12340
C ** LOAD HOLE (LENGTH / DIAMETER = 6/1) ** VCR12350
C----- VCR12360
PI = 3.14159 VCR12370
ALOAD(1A) = (6 * DHOLE * PI * DHOLE ** 2.0 / 4.0) * RHOE VCR12380
IF(MSYSUN.EQ.1) ALOAD(1) = ALOAD(1)/1000.0 VCR12390
C----- VCR12400
C ** CALCULATE EQUIVALENT WEIGHT OF EXPLOSIVE ** VCR12410
C----- VCR12420
WEIGHT(1A) = ALOAD(1A) * WSTR / WSTRTH VCR12430
C----- VCR12440
C ** CHECK VIBRATION LEVELS ** VCR12450
C----- VCR12460
IF(NCHK.EQ.0) GO TO 32 VCR12470
C----- VCR12480
C ** CALCULATE DISTANCES FROM POINTS VCR12490
C----- VCR12500
DO 30 1 = 1, NCHK VCR12510
CALL DISTPT(XVCHK(1),YVCHK(1),ZVCHK(1),X(1A),Y(1A),Z(1A),DIST) VCR12520
C----- VCR12530
C ** CALCULATE PPV AT THIS POINT ** VCR12540
C----- VCR12550
PPV(1) = AKFAC*(DIST/WEIGHT(1A)**(1.0/3.0))*AMEAC VCR12560
C----- VCR12570
C ** FIND MAXIMUM WEIGHT FOR THIS PARTICULAR POINT ** VCR12580
C----- VCR12590
WEIGMX(1) = (AKFAC/PPVALL(1))*((3.0/AMEAC)*DIST**3.0 VCR12600
30 CONTINUE VCR12610
C----- VCR12620
C ** CALCULATE DISTANCE FROM PILLARS ** VCR12630
C----- VCR12640
32 IF (NUMPIL.EQ.0) GO TO 52 VCR12650

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DO 50 I = 1, NUMPIL                                VCR12660
CALL DISTPL(XPIL1(I),YPIL1(I),ZPIL1(I),XPIL2(I),YPIL2(I),ZPIL2(I),VCR12670
XXPIL3(I),YPIL3(I),ZPIL3(I),X(IA),Y(IA),Z(IA),DISTP) VCR12680
C-----VCR12690
C ** CALCULATE PPV AT THIS POINT **                VCR12700
C-----VCR12710
PPVPIL(I) = AREAC * (DISTP/WEIGHT(IA))** (1.0/3.0)** VCR12720
X AMEAL                                           VCR12730
C-----VCR12740
C ** FIND MAXIMUM WEIGHT BECAUSE OF THIS PARTICULAR PILLAR ** VCR12750
C-----VCR12760
WEIGMX(NCHK+1) = (AREAC/PPVPIL)** (3.0/AMEAL)*DISTP**3.0 VCR12770
50 CONTINUE                                         VCR12780
C-----VCR12790
C ** FIND MINIMUM ACCEPTABLE WEIGHTS **            VCR12800
C-----VCR12810
52 WMIN = 2000000.0                                VCR12820
NN = NCHK + NUMPIL                                VCR12830
IF (NN.EQ.0) GO TO 99                             VCR12840
DO 80 I = 1, NN                                    VCR12850
IF (WEIGMX(I).LT.WMIN) WMIN=WEIGMX(I)             VCR12860
80 CONTINUE                                         VCR12870
IF (WEIGHT(IA).LE.WMIN) GO TO 99                  VCR12880
WEIGHT(IA) = WMIN                                  VCR12890
99 KK = KK + 1                                     VCR12900
INIT(KK) = IA                                       VCR12910
C-----VCR12920
C ** CALCULATE OPTIMUM DEPTH OF BURIAL **           VCR12930
C-----VCR12940
DOPT(IA) = DELTA * CEACR * (WEIGHT(IA))** (1.0/3.0) VCR12950
DEPTH(IA) = DOPT(IA)                              VCR12960
C-----VCR12970
C ** CALCULATE CRATER RADIUS **                   VCR12980
C-----VCR12990
RCR(IA) = SCRCP * WEIGHT(IA) ** (1.0/3.0)         VCR13000
100 CONTINUE                                         VCR13010
IF(NN.EQ.0) GO TO 250                             VCR13020
C-----VCR13030
C CHECK VIBRATIONS DUE TO THE SIMULTANEOUS DETONATION OF VCR13040
C MANY CHARGES                                     VCR13050
C-----VCR13060
C-----VCR13070
C-----VCR13080
C ** FIND AN AVERAGE POSITION OF THE CONCENTRATED CHARGE ** VCR13090
C-----VCR13100
105 XM = 0.0                                         VCR13110
IF(KK.EQ.1) GO TO 200                             VCR13120
YM = 0.0                                             VCR13130
ZM = 0.0                                             VCR13140
WM = 0.0                                             VCR13150
DO 110 I = 1, KK                                   VCR13160
IM = INIT(I)                                        VCR13170
XM = XM + X(I)*WEIGHT(IM)                         VCR13180
YM = YM + Y(I)*WEIGHT(IM)                         VCR13190
ZM = ZM + Z(I)*WEIGHT(IM)                         VCR13200

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      WM = WM + WEIGHT(IM)
110 CONTINUE
      XM = XM / WM
      YM = YM / WM
      ZM = ZM / WM
C-----
C  **  CALCULATE DISTANCE FROM POINTS  **
C-----
      IF (NCHK.EQ.0) GO TO 131
      DO 130 I = 1, NCHK
      CALL DISTPT(XVCHK(I),YVCHK(I),ZVCHK(I),XM,YM,ZM,DISTM)
C-----
C  **  CALCULATE PPV AT THIS POINT  **
C-----
      PPV(I) = AKIACA(DISTM/WM**3.0) ** ANEAC
C-----
C  **  FIND MAXIMUM WEIGHT FOR THIS PARTICULAR POINT  **
C-----
      WEIGMX(I) = (AKIAC/PPVALL(I))**3.0/ANEAC*ADISTM**3.0
130 CONTINUE
C-----
C  **  SAME FOR PILLARS
C-----
131 IF (NUPIL.EQ.0) GO TO 151
      DO 150 I = 1, NUPIL
      CALL DISTPL(XPIL1(I),YPIL1(I),ZPIL1(I),XPIL2(I),YPIL2(I),ZPIL2(I),
      X XPIL3(I),YPIL3(I),ZPIL3(I),XM,YM,ZM,DISTM)
      PPVPIL(I) = AKIACA((DISTM)/WM**3.0) ** ANEAC
      WEIGMX(NCHK+I) = (AKIAC/PPVPAL)**3.0/ANEAC*ADISTM**3.0
150 CONTINUE
C-----
C  **  FIND MINIMUM OF ACCEPTABLE WEIGHTS  **
C-----
151 WMIN = 2000000.0
      NN = NCHK + NUPIL
      IF (NN.EQ.0) GO TO 200
      DO 180 I = 1, NN
      IF(WEIGMX(I).LT.WMIN) WMIN = WEIGMX(I)
180 CONTINUE
      IF (WM.LE.WMIN) GO TO 200
      IM = INIT(KK)
      KK = KK - 1
      ICH = ICH + 1
      ID(ICH) = IM
      GO TO 105
200 IF(ICH.LQ.0) GO TO 250
      DO 210 I = 1, NUMBH
      IF (IPER(I).LE.IFIRST) GO TO 210
      IPER(I) = IPER(I) + 1
210 CONTINUE
      DO 220 I = 1, ICH
      IC = ID(I)
      IPER(IC) = IFIRST + 1
220 CONTINUE
      DO 235 I = 1, NUMBH

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A29

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C-----
      DO 1190 IFF = 1,50
      1190 IFLY(IPP) = 0
C-----
C      **      FIND PREVIOUS CRATERS      **
C-----
      KPREV = 0
      DO 100 I = 1, NUMBH
      IF ( IPER(I).GE.IPER(IPREV)) GO TO 100
      KPREV = KPREV + 1
      IPREV(KPREV) = I
      100 CONTINUE
C-----
C      **      CHECK THE NEW CRATERS ONE BY ONE      **
C-----
      DO 500 I = 1, KK
      INEXT = INIT(I)
      DO 400 II = 1, KPREV
      IA = IPREV (II)
      DIST(IA,INEXT) = (ABS(Y(INEXT) - Y(IA))**2.0
      + ABS(X(INEXT)-X(IA))**2.0)
      X**0.5
      A1 = DEPTH(IA)
      B1 = RCR(IA)
      C1 = -RCR(IA)*DEPTH(IA)
      BURDEN(INEXT,IA) = ABS((A1A1DIST(IA,INEXT) + B1ADUPT(INEXT) +
      X C1 ) / (A1A12.0+B1A12.0) ** 0.5)
      RATIO = BURDEN(INEXT,IA) / DUPT(INEXT)
      IF (RATIO.LT.0.3) GO TO 1400
      400 CONTINUE
      500 CONTINUE
      KIND = 1
      RETURN
C-----
C      **      FLYROCK REGION      **
C-----
      1400 CONTINUE
C-----
C      **      DETONATE INEXT AT THE SAME DELAY PERIOD WITH IA      **
C-----
      IPERT = IPER(INEXT)
      KTEST = 0
      DO 1500 ITT = 1,NUMBH
      IF (IPER(ITT).EQ.IPERT) KTEST = KTEST + 1
      1500 CONTINUE
      IF (KTEST.EQ.1) GO TO 1510
      IPER(INEXT)=IPER(IA)
      GO TO 1521
      1510 DO 1520 ITT = 1,NUMBH
      IF(IPER(ITT).GE.IPERT) IPER(ITT)=IPER(ITT) - (IPERT -
      X IPER(IA))
      IF(IPER(ITT).GT.IPERT) IPER(ITT) = IPER(ITT) - 1
      IPER(INEXT) = IPER(IA)
      1520 CONTINUE
      1521 IFLY(INEXT) = IA

```

VCR1431
 VCR1432
 VCR1433
 VCR1434
 VCR1435
 VCR1436
 VCR1437
 VCR1438
 VCR1439
 VCR1440
 VCR1441
 VCR1442
 VCR1443
 VCR1444
 VCR1445
 VCR1446
 VCR1447
 VCR1448
 VCR1449
 VCR1450
 VCR1451
 VCR1452
 VCR1453
 VCR1454
 VCR1455
 VCR1456
 VCR1457
 VCR1458
 VCR1459
 VCR1460
 VCR1461
 VCR1462
 VCR1463
 VCR1464
 VCR1465
 VCR1466
 VCR1467
 VCR1468
 VCR1469
 VCR1470
 VCR1471
 VCR1472
 VCR1473
 VCR1474
 VCR1475
 VCR1476
 VCR1477
 VCR1478
 VCR1479
 VCR1480
 VCR1481
 VCR1482
 VCR1483
 VCR1484
 VCR1485

```
KIND = 2
RETURN
END
SUBROUTINE DISPLN(X1,Y1,X2,Y2,X,Y,DISTA,IBUG)
IBUG = 0
A1= Y1 - Y2
B1= X2 - X1
C1= X1AY2-X2AY1
A = ABS(A1)
B = ABS(B1)
DENOM = AAA2.0 + BAA2.0
IF(DENOM.LE.1.E-25) GO TO 10
DISTA=ABS(AIAX + BIAY + C1)/DENOMAAA0.5
RETURN
10 IBUG = 1
RETURN
END
SUBROUTINE SEQUEN
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC VCR14860
C PURPOSE : VCR14870
C      10 PROVIDE THE INITIATION SEQUENCE FOR AN UNDERGROUND VCR14880
C      BLAST USING THE VCR METHOD. VCR14890
C VCR14900
C VCR14910
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC VCR14920
C VARIABLES : REFER TO THE MAIN PROGRAM VCR14930
C VCR14940
C VCR14950
CHARACTERAI KKODE VCR14960
COMMON /RDRDT1/ DCONCH,WTCNRG,WSTRTH,SCDEPT(50),DELTA(50), VCR14970
XSCRAD(50),DHOLE,X(50),Y(50),Z(50),XVCHK(10),YVCHK(10),ZVCHK(10) VCR14980
X,PPVAL(10),AKFAC,AMEAC,XPIL1(10),XPIL2(10),XPIL3(10),YPIL1(10), VCR14990
XYPIL2(10),YPIL3(10),ZPIL1(10),ZPIL2(10),ZPIL3(10),PPVPAL,WSTRK, VCR15000
XXMAX,XMIN,YMAX,YMIN,ZMAX,ZMIN,DELTAR(50),RHOE VCR15010
COMMON/RDRDT2/ NP1,NP2,NUMBH.NCHK,NUMPIL,INIT(50),MSYSUN VCR15020
COMMON/IBLK/ IBLOCK(100,100,5),ITIME(100,100,5) VCR15030
COMMON/DXDYZ/ DX,DY,DZ VCR15040
COMMON/DELT/DELTU,LEACTK VCR15050
COMMON/XDLK/XB(100),YB(100),ZB(5) VCR15060
COMMON/ISEQ/ IPER(50),KK VCR15070
COMMON/ELY/ IFLY(50) VCR15080
COMMON/CHARGE/WEIGHT(50),DOFT(50),KCR(50),DEPTH(50).SCRUP VCR15090
COMMON/BURDEN/ BURDEN(50,50) VCR15100
COMMON/TPE/EXPTYP,EXPTYB VCR15110
COMMON/REFER/ XREFER,YREFER,ZREFER,STANGR,STLENG,STWIDT VCR15120
X ,STDEPT VCR15130
DIMENSION ID(50),IEXAN(50),ADIST(50) VCR15140
----- VCR15150
C AA INITIALIZE DATA AA VCR15160
----- VCR15170
DO 4 I=1,NUMBH VCR15180
IPER(I) = 0 VCR15190
IEXAN(I) = 0 VCR15200
4 CONTINUE VCR15210
```

```

      IDLT = 1
      PI = 3.14159
      RAD = SCROPA((GADHOLEAPIADHOLE**2.0/4.0)*RHOE*AWSTR/WSTRH)**.5
      X(1.0/3.0)
      IF(MSYSUN.EQ.1)
      XRAD=SCROPA((GADHOLEAPIADHOLE**2.0/4.0)*RHOE/1000.*AWSTR/WSTRH)**.5
      X(1.0/3.0)
      WRITE(7,10)
10  FORMAT('  ENTER (M) FOR MANUAL OR (A) FOR AUTOMATIC',/
      X          '          GENERATION OF THE INITIATION SEQUENCE.')
```

```

      READ(7,12) KKODE
12  FORMAT(1A1)
      IF(KKODE.EQ.'A') GO TO 40
      WRITE(7,14)
14  FORMAT(//////, '          MANUAL GENERATION OF SEQUENCE',/
      X          '          -----',///)
      WRITE(7,20)
20  FORMAT('  ENTER NUMBER OF HOLE AND INITIATION PERIOD :')
```

```

      DO 25 I = 1,NUMBH
      READ(7,A) NH,IPER(NH)
25  CONTINUE
      RETURN
40  WRITE(7,41)
41  FORMAT(//////, '          AUTOMATIC GENERATION OF SEQUENCE',/
      X          '          -----',///)
      WRITE(7,43)
43  FORMAT('  ENTER THE NUMBER OF THE HOLE WHICH DETONATES FIRST :')
```

```

      READ(7,A) IF
      IP = 1
      IPER(IF) = 1
45  ICHK1 = 0
      DISTH = 100000.0
      DO 46 I = 1,NUMBH
      ADIST(I) = 1000.0
46  CONTINUE
```

```

C  AA          FIND NEXT HOLE          AA
C  -----
      DO 50 I = 1, NUMBH
      IF ( IPER(I).NE.0 ) GO TO 50
      CALL DISTPT(X(IF),Y(IF),Z(IF),X(I),Y(I),Z(I),DIST)
      IF(DIST.GT.DISTH) GO TO 50
      DISTH = DIST
      IS = I
50  CONTINUE
      IF (DISTH.GE.10000.0) GO TO 120
      IP = IP + 1
      IPER(IS) = IP
      II = 1
      ICHECK = 0
      DO 70 I = 1, NUMBH
      CALL DISTPT(X(IF),Y(IF),Z(IF),X(I),Y(I),Z(I),DIST)
      IF((DIST.GT.(DISTH+RAD)).OR.(DIST.LT.DISTH).OR.(I.EQ.IS))
      X GO TO 70
      JEDAM(I) = 1
```



```

      PP = 3.1415926
27  FORMAT(4F10.2)
19  FORMAT(20A4)
20  FORMAT(4F10.2)
      REWIND 70
      READ(70,910) NUMBH,NCHRG5
910  FORMAT(15I5)
      READ(70,900) DIAMT
      DO 1000 I = 1,NCHRG5
      READ(70,900) (ZKNOWN(J,I),J=1,NUMBH)
900  FORMAT(8F10.2)
1000 CONTINUE
      DO 1050 I = 1,NCHRG5
      READ(70,900) (WEIGHT(J,I),J=1,NUMBH)
1050 CONTINUE
      DO 1100 I = 1,NCHRG5
      READ(70,900) (ALENGT(J,I),J=1,NUMBH)
1100 CONTINUE
      IEXP = 1
      DO 1200 I = 1,NCHRG5
      READ(70,910) (IPEK(J,I),J=1,NUMBH)
1200 CONTINUE
      REWIND 61
      DO 3000 IHOSLU = 1,NUMBH
      READ(61,100) LJUNK,N1,IHOROW,IHOCOL,00000,DIPN08
100  FORMAT(4I5,2F10.2)
      IF(LJUNK,00.99) GO TO 3008
      WRITE(62,21) NCHRG5,IHOROW,IHOCOL
21  FORMAT(15I5)
      READ(61,101) XCOLAK,YCOLAK,ZCOLAK
101  FORMAT(3F10.2)
      READ(61,101,END=3008) ((XDI(I),YDI(I),ZDI(I)),I=1,N1)
      DO 155 ICH = 1,NCHRG5
      X1 = XCOLAK
      Y1 = YCOLAK
      Z1 = ZCOLAK - ZKEFER
      D1 = 0
      DO 150 I = 1,N1
      Z2 = ZDI(I) - ZKEFER
      X2 = XDI(I)
      Y2 = YDI(I)
      IF(Z2.LT.ZKNOWN(IHOSLU,ICH)) GO TO 109
      ZLOCAL = ZKNOWN(IHOSLU,ICH)
      RATIO = (ZKNOWN(IHOSLU,ICH)-Z1)/(Z2-Z1)
      DX1X2 = RATIO*(X1-X2)
      DY1Y2 = RATIO*(Y1-Y2)
      DI=DI+(ABS(DX1X2)**2.0+ABS(DY1Y2)**2.0+ABS(Z1-ZKNOWN(IHOSLU,ICH))
      XAA2.0)AA0.5
      GO TO 200
109  ZLOCAL = Z2
      DI=DI + (ABS(X1-X2)**2.0+ABS(Y1-Y2)**2.0+ABS(Z1-Z2)**2.0)AA0.5
      X1 = X2
      Y1 = Y2
      Z1 = Z2
150  CONTINUE

```

VCR16510
 VCR16520
 VCR16530
 VCR16540
 VCR16550
 VCR16560
 VCR16570
 VCR16580
 VCR16590
 VCR16600
 VCR16610
 VCR16620
 VCR16630
 VCR16640
 VCR16650
 VCR16660
 VCR16670
 VCR16680
 VCR16690
 VCR16700
 VCR16710
 VCR16720
 VCR16730
 VCR16740
 VCR16750
 VCR16760
 VCR16770
 VCR16780
 VCR16790
 VCR16800
 VCR16810
 VCR16820
 VCR16830
 VCR16840
 VCR16850
 VCR16860
 VCR16870
 VCR16880
 VCR16890
 VCR16900
 VCR16910
 VCR16920
 VCR16930
 VCR16940
 VCR16950
 VCR16960
 VCR16970
 VCR16980
 VCR16990
 VCR17000
 VCR17010
 VCR17020
 VCR17030
 VCR17040
 VCR17050


```

200 DUP = DI - ALENGT(IHSEQ,ICH)/2.0          VCR17060
DDO = DI + ALENGT(IHSEQ,ICH)/2.0          VCR17070
DDOUPD(IHSEQ) = DDO                        VCR17080
ZDO = ZCOLAR-ZREFER-(ZKNOWN(IHSEQ,ICH)+ALENGT(IHSEQ,ICH)/2.0) VCR17090
ZUP = ZCOLAR-ZREFER-(ZKNOWN(IHSEQ,ICH)-ALENGT(IHSEQ,ICH)/2.0) VCR17100
WRITE(62,260) ZDO,ZUP,DDO,DUP,WEIGHT(IHSEQ,ICH),DIAMT,IEXPLT,IPERVCR17110
X(IHSEQ,ICH)                               VCR17120
260 FORMAT(6F10.2,2I5)                     VCR17130
155 CONTINUE                               VCR17140
3000 CONTINUE                              VCR17150
3008 CONTINUE                              VCR17160
LAST = 99                                  VCR17170
WRITE(62,21) LAST,IHROW,IHCOL             VCR17180
RETURN                                      VCR17190
END                                          VCR17200
SUBROUTINE PLVIEW (PLELEV,XHOL,YHOL,ZHOL,NOHOLS) VCR17210
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC VCR17220
C                                          C VCR17230
C PURPOSE :                               C VCR17240
C TO GIVE THE X Y COORDINATES OF THE HOLES AT A PARTICULAR C VCR17250
C ELEVATION                               C VCR17260
C                                          C VCR17270
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC VCR17280
C                                          C VCR17290
C VARIABLES                               VCR17300
C PLELEV : PLAN ELEVATION                 VCR17310
C STOPID : STOPE IDENTIFICATION (UP TO 90 CHARACTERS) VCR17320
C XREFER , YREFER , ZREFER . REFERENCE POINT FOR TRANSLATION VCR17330
C                                          C VCR17340
C                                          C VCR17350
C                                          C VCR17360
CHARACTER*4 STOPID                        VCR17370
COMMON/REFER/ XREFER,YREFER,ZREFER,STANGR,STLENG,STWIDT VCR17380
X ,SIDEPT                                VCR17390
DIMENSION D(50),DIP(50),AZIM(50)         VCR17400
DIMENSION X(50),Y(50),Z(50)              VCR17410
DIMENSION STOPID(50)                     VCR17420
DIMENSION XHOL(50),YHOL(50),ZHOL(50)     VCR17430
DIMENSION HOL(50,3),XP(50),YP(50),DIAM(50) VCR17440
PP=3.1415926                             VCR17450
REWIND 51                                 VCR17460
REWIND 61                                 VCR17470
PLELEV=PLELEV-ZREFER                      VCR17480
IF (PLELEV.LT.0.0) RETURN                 VCR17490
6 FORMAT(11,' ','11)                     VCR17500
19 FORMAT(20A4)                           VCR17510
20 FORMAT(4F10.2)                         VCR17520
C----- VCR17530
C READ HOLE DATA                         VCR17540
C 99 DENOTES END OF HOLE DATA FILE      VCR17550
C----- VCR17560
C                                          VCR17570
7 READ (61,100) IHSEQ,N1,IHROW,IHCOL,DIA,DIPNM VCR17580
IF (IHSEQ.EQ.99) GO TO 8                  VCR17590
C----- VCR17600
C INCREASE HOLE DIAMETER BY A200 FOR PLOT CLARITY

```

C	READ (61,101) XCULAR,YCULAR,ZCULAR	VCR1761
C	-----	VCR1762
C	STATION INTERVAL 10 FT	VCR1763
C	FOLLOWING DATA REFERS TO HOLE AXIS	VCR1764
C	-----	VCR1765
	READ (61,101,END=8) ((X(I),Y(I),Z(I)),I=1,N1)	VCR1766
	CALL PTRANS(X,Y,Z,N1,XREFER,YREFER,ZREFER)	VCR1767
C	-----	VCR1768
C	ROTATE COORDINATES (STANGR)	VCR1769
C	-----	VCR1770
	DO 200 I = 1,N1	VCR1771
	XC = X(I) * COS(STANGR) + Y(I) * SIN (STANGR)	VCR1772
	YC = - X(I) * SIN(STANGR) + Y(I) * COS (STANGR)	VCR1773
	X(I) = XC	VCR1774
	Y(I) = YC	VCR1775
	HOL(I,1) = X(I)	VCR1776
	HOL(I,2) = Y(I)	VCR1777
	HOL(I,3) = Z(I)	VCR1778
200	CONTINUE	VCR1779
	DO 10 I=2,N1	VCR1780
	IF (HOL(I,3).LT.PLELEV) GO TO 10	VCR1781
	XP(1)=HOL(I,1)+(PLELEV-HOL(I,3))/(HOL(I-1,3)-HOL(I,3))*HOL(I-1,	VCR1782
	A1)-HOL(I,1))	VCR1783
	YP(1)=HOL(I,2)+(PLELEV-HOL(I,3))/(HOL(I-1,3)-HOL(I,3))*HOL(I-1,	VCR1784
	A2)-HOL(I,2))	VCR1785
	GO TO 11	VCR1786
10	CONTINUE	VCR1787
11	CONTINUE	VCR1788
	XP(2)=HOL(I,1)	VCR1789
	YP(2)=HOL(I,2)	VCR1790
	XHOL(IHOSQ) = XP(1)	VCR1791
	YHOL(IHOSQ) = YP(1)	VCR1792
	ZHOL(IHOSQ) = PLELEV	VCR1793
	GO TO 7	VCR1794
8	CONTINUE	VCR1795
100	FORMAT(4I5,2F10.2)	VCR1796
101	FORMAT(3F10.2)	VCR1797
	REWIND 51	VCR1798
	REWIND 61	VCR1799
	RETURN	VCR1800
	END	VCR1801
	SUBROUTINE PTRANS(X,Y,Z,NPNTS,XREF,YREF,ZREF)	VCR1802
	-----	VCR1803
	CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC	VCR1804
C		C VCR1805
C	PURPOSE :	C VCR1806
C	TO PERFORM A TRANSLATION WRT THE POINT XREF,YREF,ZREF	C VCR1807
C		C VCR1808
	CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC	VCR1809
	DIMENSION X(50),Y(50),Z(50)	VCR1810
	DO 10 I=1,NPNTS	VCR1811
	X(I)=X(I)-XREF	VCR1812
	Y(I)=Y(I)-YREF	VCR1813
	Z(I)=Z(I)-ZREF	VCR1814
10	CONTINUE	VCR1815

FILE: VCPH LORTKAN 61

VR/SP CONVERSATIONAL MONITOR SYSTEM

A36

RETURN
END

VCR18160
VCR18170

2. LARGE DIAMETER BENCH BLAST DESIGN

1.1.700540

```

INTEGRA4 CLTIME,TCPU
CHARACTER*15 EXPTYP,EXPTYB
CHARACTER*80 TITLE
CHARACTER*3 QDATE ,QTIM
CHARACTER*1 KODE,IWR,BKTHR,KKODE1,KKODEI
CHARACTER*4 FT,INCH,LBS
COMMON /RDRDT1/ DCONCH,WTCHRG,WSTRTH,SCDEPT(50),DELTA(50),
XSCRAD(50),DHOLE,X(50),Y(50),Z(50),XVCHK(10),YVCHK(10),ZVCHK(10)
X,PPVALL(10),AKFAC,AMEAC,XPIL1(10),XPIL2(10),XPIL3(10),YPIL1(10),
XPIL2(10),YPIL3(10),ZPIL1(10),ZPIL2(10),ZPIL3(10),PPVPAL,WSTR,
XXMAX,XMIN,YMAX,YMIN,ZMAX,ZMIN,DELTAR(50),RHOE,DCONCB,SCDEPB(50),
XDELTAR(50),SCRADB(50),DELTBR(50),WTCHRB,ALENGT,BMIN,SEPDIS
COMMON/RDRDT2/ NP1,NPB1,NP2,NPB2,NUMBH,NCHK,NUMPIL,INIT(50),NCONTRL
X ,NTOTAL,MSYSUN
COMMON/IBLK/ IBLOCK(100,100),ITIME(100,100)
COMMON/UXDY/ DX,DY
COMMON/DELT/DLTO,EFACTR,DELTOR,EFACTB
COMMON/XBLK/XB(100),YB(100)
COMMON/ISEQ/ IPER(50),KK,NR,NCH(50),NDECKS
COMMON/CHARGE/WEIGHT(50),WEIGB(50),DOPT(50),RCR(50),DEPTH(50),
XSCROP,DOPTB(50)
COMMON/TYPE/EXPTYP,EXPTYB
COMMON/TT/TITLE
COMMON/FREF/ XFF(10),YFF(10)
COMMON/UPDATE/XXX(50,20),YYY(50,20),ZZZ(50,20),WUPB(50,20)
COMMON/ALPHA/LWK(100,100),BKTHR
COMMON/CONTR/ XCONT1(10),XCONT2(10),YCONT1(10),YCONT2(10)
COMMON/REFER/ XREFER,YREFER,ZREFER,STANGR,STLENG,STWIDT,

```



```

X STDEPT
COMMON/UNALP/ LBS.INCH.ET
DIMENSION ISOUT(50,20)
DIMENSION TOP(50),ALUPD(50,20),000UPD(50,20)
C-----
C  **      INITIALIZE DATA      **
C-----
NDECKS = 2
ALENGT = 9.0
PI = 3.14159
DO 1901 I = 1,50
DO 1900 J = 1,50
IWR(I,J) = ' '
1900 CONTINUE
1901 CONTINUE
DO 1902 I = 1,50
WEIGHT(I) = 0.0
WEIGH(I) = 0.0
IPER(I) = 10000
1902 CONTINUE
DO 1904 I = 1,50
DO 1903 J = 1,20
ISOUT(I,J) = 0
1903 CONTINUE
1904 CONTINUE
K = 1
ICODE = 0
ICODE1 = 0
NCALL = 1
C-----
C  **      READ DATA      **
C-----
CALL READER(NPFF)
C-----
C  **      FIND LIVINGSTON'S STRAIN ENERGY FACTORS  **
C  **      FOR SPHERICAL AND CYLINDRICAL CHARGES  **
C-----
EFAC1B = DCONCH / WTCHRB ** (1.0/3.0)
EFAC1B = DCONCH / WTCHRB ** (0.5)
WRITE(6,510)
510 FORMAT(1H1,//////////,40X,'P R O G R A M   L E B B ',//
X
X 40X,'-----',//,
X 30X,'W R I T T E N   F O R   T H E   D E S I G N   O F   T H E ',//
X //,30X,'B L A S T   I N   A N   U N D E R G R O U N D   S T O P ',//
X,'E',//,30X,'U S I N G   T H E   L A R G E   D I A M E T E R ',//
X//,30X,'B L A S T H O L E   B E N C H I N G   M E T H O D ',//)
CALL QTIME(QDATE,QTIM,CLTIME,TCPU)
511 FORMAT(1H1,33X,A80,/)
WRITE(6,690) QDATE,QTIM
690 FORMAT(////////,15X,'DATE      :  ',A8,//15X,'TIME      :  '
X,A8//)
WRITE(6,512) EXPTTB
512 FORMAT(1H , '      EXPLOSIVE USED : ',A15)
WRITE(6,513) RHOE,LBS.INCH

```

```

513 FORMAT(1H0,'          DENSITY          :',F6.4,A4,'/CUBIC',A4)
      WRITE(6,590) DHOLE,INCH
590 FORMAT(1H0,'          DIAMETER          :',F6.4,A4)

```

```

C-----
C  **  FIND OPTIMUM DEPTH RATIO FOR SPHERICAL CHARGES  **
C-----

```

```

      DO 10 I = 1, NP1
      IF (SCDEPT(I+1).GE.SCDEPT(I)) GO TO 10
      DELTO = DELTA(I)
      IOPT = I
      GO TO 14
10 CONTINUE
14 CONTINUE

```

```

C-----
C  **  FIND OPTIMUM DEPTH RATIO FOR CYLINDRICAL CHARGES  **
C-----

```

```

      DO 2010 I = 1, NP1
      IF (SCDEPR(I+1).GE.SCDEPR(I)) GO TO 2010
      DELTOR = DELTAR(I)
      IOPT = I
      GO TO 2014
2010 CONTINUE
2014 CONTINUE

```

```

C-----
C  **  FIND SCALED RADIUS AT OPTIMUM DEPTH RATIO **
C-----

```

```

      DO 15 I = 2, NP2
      IF((DELTAR(I).GE.DELTO).AND.(DELTAR(I-1).LE.DELTO)) GO TO 16
15 CONTINUE
16 SCRAD = SCRAD(I-1) + (DELTO - DELTAR(I-1))/(DELTAR(I) - DELTAR(I-1))
      X A(SCRAD(I)-SCRAD(I-1))
      CALL SEPDS(DDELTA,BURDPR)
      WRITE(70,17) NUMBH,NUDECKS
17 FORMAT(15I5)
      DHOLEI = DHOLE*10.0
      WRITE(70,18) DHOLEI
18 FORMAT(F10.2)
      NTOTAL = 0
      WRITE(7,11)

```

```

11 FORMAT('  ENTER (M) FOR MANUAL OR (A) FOR AUTOMATIC'./
      X      '  GENERATION OF THE INITIATION SEQUENCE')
      READ (7,13) KKODEI

```

```

13 FORMAT(1A1)
2800 CONTINUE
      NTOTAL = NTOTAL + 1
      IF (NTOTAL.EQ.1) GO TO 2845

```

```

C-----
C  **  GET THE NEXT SERIES (HORIZONTAL) OF DECKS **
C-----

```

```

      DO 2850 I = 1, NUMBH
      Z(I) = Z(I) - ALENGT - SEPDIS
2850 CONTINUE
      ELEV = Z(I)
      CALL PLVIEW(ELEV,X,Y,NUMBH)

```

```

C-----

```

C ** GIVE INITIATION SEQUENCE **

```

C-----
2845 CALL QUADM(NPFF)
      IFIRST = 0
      IF (ICODE1.EQ.1) GO TO 2899
2855 CALL INITB(ICODE,NCALL,MAXPER,IFIRST,KKODE1)
      DO 2333 ISKA=1,NUMBH
2333 CONTINUE
      IF (ICODE.EQ.1) GO TO 2901
2899 IFIRST = 0
2900 IFIRST = IFIRST + 1
      IF(ICODE1.NE.1) GO TO 2901
4003 CALL VBRCHK( IFIRST,INDEXV,KKODE1,ICODE1 )
      IF(INDEXV.EQ.0) GO TO 2901
      DO 4001 I=1,NUMBH
      IF(IPER(I).EQ.IFIRST) IKAF=I
4001 CONTINUE
      DO 4002 I = 1, NUMBH
      IF (IPER(I).GT.IPER(IKAF)) IPER(I) = IPER(I) + 1
4002 CONTINUE
      IPER(IKAF) = IPER(IKAF) + 1
      GO TO 4003
2901 DO 3000 ICR = 1,NUMBH
      IF (IPER(ICR).NE.IFIRST) GO TO 3000
      CALL CRPLT2(ICR,BURDPP,KKODE1,ICODE1)
3000 CONTINUE
      IF (ICODE1.EQ.1) GO TO 3026
      IF (ICODE.EQ.1) GO TO 3001
      IF ( IFIRST.LT.MAXPER) GO TO 2900
      GO TO 3025

```

C-----

C ** INTERACTIVE PART WITH COLORGRAPHICS **

```

C-----
3001 CONTINUE
      DO 4601 I=1,50
      DO 4600 J=1,50
      IF(IBLOCK(I,J).EQ.0) GO TO 4699
      IF(IWR(I,J).NE.'X') IWR(I,J)='.'
      GO TO 4600
4699 IF(IWR(I,J).NE.'X') IWR(I,J) = ' '
4600 CONTINUE
4601 CONTINUE
      CALL BENGRC(X,Y,XMAX,XMIN,YMAX,YMIN,NUMBH,Z(1))
      WRITE(7,4007)
4007 FORMAT(' IS THAT SATISFACTORY (Y/N) ?')
      READ (7,4008) KODE
4008 FORMAT(A1)
      IF(KODE.EQ.'Y') GO TO 3009
      DO 4200 I = 1,50
      DO 4100 J = 1,50
      IF(itime(I,J).EQ.IFIRST) GO TO 4050
      GO TO 4100
4050 IBLOCK(I,J) = 0
      itime(I,J) = 10000
4100 CONTINUE

```

A43

4200	CONTINUE	LLM02760
	DO 4920 I = 1, NUMB1	LLM02770
	IPER(IDET) = 100000	LLM02780
4920	CONTINUE	LLM02790
	NCALL = 2	LLM02800
	IFIRST = IFIRST - 1	LLM02810
	GO TO 2855	LLM02820
3009	WRITE(7,3010)	LLM02830
3010	FORMAT(' WAS THIS THE LAST DELAY PERIOD ?')	LLM02840
	READ(7,3020) KODE	LLM02850
3020	FORMAT(1A1)	LLM02860
	IF (KODE.EQ.'N') GO TO 2855	LLM02870
	ILASTP = IFIRST	LLM02880
3025	WRITE(7,3024)	LLM02890
3024	FORMAT(' DO YOU WANT TO USE THE SAME INITIATION SEQUENCE',/	LLM02900
	X ' FOR THE SUBSEQUENT DECK LEVELS ?')	LLM02910
	READ(7,3023) KKODE1	LLM02920
3023	FORMAT(1A1)	LLM02930
	IF (KKODE1.EQ.'Y') ICODE1 = 1	LLM02940
3026	CONTINUE	LLM02950
	IF (K.EQ.1) GO TO 3028	LLM02960
	IF (IFIRST.LT.ILASTP) GO TO 2900	LLM02970
C-----		LLM02980
C	AA UPDATE VARIABLES AA	LLM02990
C-----		LLM03000
3028	DO 3030 IU = 1, NUMBH	LLM03010
	WUPD(IU,K) = WEIGHT(IU)	LLM03020
	XXX(IU,K) = X(IU)	LLM03030
	YYY(IU,K) = Y(IU)	LLM03040
	ALUPD(IU,K) = WEIGHT(IU)/(12.0*ARHOCAPIDHOLEAA2.0/4.0)	LLM03050
	IF (MSYSUN.EQ.1) ALUPD(IU,K) = WEIGHT(IU)/(0.1*ARHOCAPIDHOLEAA2.0/	LLM03060
	X4.0)	LLM03070
	ZZZ(IU,K) = Z(IU) - ALUPD(IU,K)/2.0	LLM03080
3030	CONTINUE	LLM03090
	CALL SEQOUT(K,ISOUT,ICODE1)	LLM03100
C-----		LLM03110
C	AA WRITE PRINTOUT FOR THE LEVEL AA	LLM03120
C-----		LLM03130
	DO 601 I=1,50	LLM03140
	DO 600 J=1,50	LLM03150
	IF (IBLOCK(I,J).EQ.0) GO TO 699	LLM03160
	IF (IWR(I,J).NE.'A') IWR(I,J) = ' '	LLM03170
	GO TO 600	LLM03180
699	IF (IWR(I,J).NE.'A') IWR(I,J) = ' '	LLM03190
600	CONTINUE	LLM03200
601	CONTINUE	LLM03210
	CALL BENGK (X,Y,XMAX,XMIN,YMAX,YMIN,NUMBH,Z(1))	LLM03220
	WRITE(6,496) K	LLM03230
496	FORMAT('1',/////,51X,' INITIATION SEQUENCE IN LEVEL 1',12,/	LLM03240
	X 51X, '-----',//	LLM03250
	X 40X,'HOLE NUMBER',30X,'DELAY PERIOD',/	LLM03260
	X 40X,'-----',30X,'-----',//	LLM03270
	DO 498 I=1,NUMBH	LLM03280
	WRITE(6,497) I,ISOUT(1,K)	LLM03290
497	FORMAT(45X,12,40X,12,/)	LLM03300

```

498 CONTINUE                                LLN03360  

      WRITE(6,501) K,LBS                     LLN03360  

501 FORMAT(1H1,/////.5IX,'WEIGHT OF EXPLOSIVE DECKS IN LEVEL #',(Z,/    LLN03370  

X          SIX,        -----'//           LLN03370  

X 40X,'HOLE NUMBER',30X,'WEIGHT ('A4.')',/   LLN03380  

X 40X,'-----',30X,'-----',/)            LLN03380  

      DO 503 I = 1, NUMBH                    LLN03390  

      ALOADW = WEIGHT(I)*WSTRKTH/WSTR         LLN03390  

      WRITE(6,502) I,ALOADW                  LLN03400  

502 FORMAT(43X,12,35X,F8.0,)                LLN03400  

503 CONTINUE                                 LLN03410  

      WRITE(6,7777) Z(1)                      LLN03420  

7777 FORMAT(1H1,'                           PLAN VIEW AT DEPTH', F12.4,/   LLN03430  

X'                   -----'////////')     LLN03440  

      WRITE(6,7437) XB(1),XB(11),XB(21),XB(31),XB(41),XB(51),XB(61),    LLN03450  

XXB(71)                                     LLN03460  

7437 FORMAT(8X,(F4.0,6X))                    LLN03470  

      WRITE(6,7438)                          LLN03480  

7438 FORMAT(10X,'+-----+',               LLN03490  

X'+-----+')                               LLN03500  

602 CONTINUE                                 LLN03510  

      DO 7670 JP = 1,50,10                    LLN03520  

      WRITE(6,7655) YB(JP),(IWK(I,JP),I=1,50) LLN03530  

7655 FORMAT(1H ,F4.0,' + ',50A1)             LLN03540  

      WRITE(6,7660) ((IWK(I,J),I=1,50),J=JP+1,JP+9) LLN03550  

7660 FORMAT(1H ,4X .'| ',50A1)              LLN03560  

7670 CONTINUE                              LLN03570  

      K = K + 1                             LLN03580  

      IF (K.GT.NDECKS) GO TO 3052             LLN03590  

      GO TO 2800                            LLN03600  

3052 DO 7710 J = 1,NDECKS                   LLN03610  

      WRITE(70,7709) (ZZZ(I,J),I=1,NUMBH)     LLN03620  

7709 FORMAT(8F10.2)                         LLN03630  

7710 CONTINUE                              LLN03640  

      DO 7720 J = 1,NDECKS                   LLN03650  

      WRITE(70,7709) (WUPD(I,J),I=1,NUMBH)     LLN03660  

7720 CONTINUE                              LLN03670  

      DO 7730 J = 1,NDECKS                   LLN03680  

      WRITE(70,7709) (ALUPD(I,J),I=1,NUMBH)     LLN03690  

7730 CONTINUE                              LLN03700  

      DO 7740 J = 1,NDECKS                   LLN03710  

      WRITE(70,17) (ISOUT(I,J),I=1,NUMBH)       LLN03720  

7740 CONTINUE                              LLN03730  

C-----LLN03740  

C ** GIVE SUMMARY OF THE REQUIRED SUPPLIES AA LLN03750  

C-----LLN03760  

      TW = 0.0                               LLN03770  

      DO 9100 I = 1,NUMBH                    LLN03780  

      DO 9050 J = 1,NDECKS                    LLN03790  

      TW = TW + WUPD(I,J)                     LLN03800  

9050 CONTINUE                               LLN03810  

9100 CONTINUE                               LLN03820  

      WRITE(6,9101) TW,LBS                     LLN03830  

9101 FORMAT(1H1,4SX,'SUMMARY',/4SX,'-----',///,2SX,'TOTAL WEIGHT OE' LLN03840  

X.'EXPLOSIVE :'.F10.0,A4)                 LLN03850
```

LLM03860
LLM03870
LLM03880
LLM03890
LLM03900
LLM03910
LLM03920
LLM03930
LLM03940
LLM03950
LLM03960
LLM03970
LLM03980
LLM03990
LLM04000
LLM04010
LLM04020
LLM04030
LLM04040
LLM04050
LLM04060
LLM04070
LLM04080
LLM04090
LLM04100
LLM04110
LLM04120
LLM04130
LLM04140
LLM04150
LLM04160
LLM04170
LLM04180
LLM04190
LLM04200
LLM04210
LLM04220
LLM04230
LLM04240
LLM04250
LLM04260
LLM04270
LLM04280
LLM04290
LLM04300
LLM04310
LLM04320
LLM04330
LLM04340
LLM04350
LLM04360
LLM04370
LLM04380
LLM04390
LLM04400


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C      DELTBR : DEPTH RATIO                                LLM04410
C      DEPR : DEPTH RATIO                                LLM04420
C      DHOLE : DIAMETER OF BOREHOLE                      LLM04430
C      DIST : DISTANCE                                    LLM04440
C      DX : X DIMENSION OF BLOCK                          LLM04450
C      DY : Y DIMENSION OF BLOCK                          LLM04460
C      EFACB : STRAIN ENERGY FACTOR FOR CYLINDRICAL CHARGES LLM04470
C      EFACTR : STRAIN ENERGY FACTOR FOR SPHERICAL CHARGES LLM04480
C      EXPTYB : EXPLOSIVE TYPE                             LLM04490
C      EXPTYP : EXPLOSIVE TYPE                             LLM04500
C      IBLOCK(I,J) : IF GREATER THAN ZERO BLOCK (I,J) TAKEN LLM04510
C                      OTHERWISE BLOCK IS NOT TAKEN        LLM04520
C      INDEXV : IF 1 VIBRATIONS EXCEED MAXIMUM           LLM04530
C      ISOUT : ARRAY INDICATING SEQUENCE                  LLM04540
C      ITIME(I,J) : ARRAY INDICATING PERIOD IN WHICH BLOCK (I,J) WAS LLM04550
C                      REMOVED                               LLM04560
C      NPB1 : NUMBER OF POINTS IN SCALED CRATER DEPTH - DEPTH LLM04570
C              RATIO CURVE (CYLINDRICAL)                  LLM04580
C      NPB2 : NUMBER OF POINTS IN SCALED CRATER RADIUS - DEPTH LLM04590
C              RATIO CURVE (CYLINDRICAL)                  LLM04600
C      SCDEPR : SCALED DEPTH OF BURIAL FOR CYLINDRICAL CHARGES LLM04610
C      SCDEPT : SCALED DEPTH OF BURIAL FOR SPHERICAL CHARGES LLM04620
C      SCRADB : SCALED RADIUS FOR CYLINDRICAL              LLM04630
C      SCROP : OPTIMUM SCALED RADIUS                      LLM04640
C      WEIGB : WEIGHT/UNIT LENGTH                         LLM04650
C      WEIGHT : WEIGHT OF EXPLOSIVE DECK                   LLM04660
C      WSTR : WEIGHT STRENGTH                             LLM04670
C      X(1) : X COORDINATE OF HOLE 1                     LLM04680
C      XMAX : MAX LOCAL LENGTH (USED TO DETERMINE LENGTH OF BLOCK) LLM04690
C      XMIN : MIN LOCAL LENGTH                            LLM04700
C      Y(1) : Y COORDINATE OF HOLE 1                     LLM04710
C      YMAX : MAX LOCAL WIDTH (USED TO DETERMINE LENGTH OF BLOCK) LLM04720
C      YMIN : MIN LOCAL WIDTH                             LLM04730
C      Z(1) : Z COORDINATE OF HOLE 1                     LLM04740
C                      LLM04750
C      XS,YS,ZS : ARRAYS DEFINING A CLOSED POLYGON       LLM04760
C-----
C      CHARACTER1 KKODEI                                   LLM04770
C      COMMON/IBLK/ IBLK(100,100), ITIME(100,100)        LLM04780
C      COMMON/XBLK/ XB(100),YB(100)                      LLM04790
C      COMMON/DXDY/ DX,DY                                LLM04800
C      COMMON /RDRDT1/ DCONCH,WCHRG,WSTRTH,SCDEPT(50),DELTA(50), LLM04810
C      XSCRAD(50),DHOLE,X(50),Y(50),Z(50),XVCHK(10),YVCHK(10),ZVCHK(10) LLM04820
C      X.PPVALL(10),AKEAC,AMFAC,XPIL1(10),XPIL2(10),XPIL3(10),YPIL1(10), LLM04830
C      YPIL2(10),YPIL3(10),ZPIL1(10),ZPIL2(10),ZPIL3(10),PPVPAL,WSTR. LLM04840
C      XXMAX,XMIN,YMAX,YMIN,ZMAX,ZMIN,DELTAR(50),RHUE,DCONCB,SCDEPB(50). LLM04850
C      XDELTAR(50),SCRADB(50),DELTBR(50),WCHRRB,ALENGT,BMIN,SEPDIS LLM04860
C      COMMON/RDRDT2/ NP1,NPB1,NP2,NPB2,NUMBH,NCHK,NUMPIL,INIT(50),NCONTELLM04870
C      X . NTOTAL                                         LLM04880
C      COMMON/DELT/DELTO,EFACTR,DELTOR,EFACTB            LLM04890
C      COMMON/ISEQ/ IPER(50),KK,NR,NCH(50),NDECKS        LLM04900
C      COMMON/CHARGE/ WEIGHT(50),WEIGB(50),DOPT(50),RCR(50),DEPTH(50), LLM04910
C      XSCROP,DOPTR(50)                                  LLM04920
C      COMMON/REFER/ XREFER,YREFER,ZREFER,STANGR,STLENG,STWIDT. LLM04930
C      X STDEPT                                           LLM04940
C      X STDEPT                                           LLM04950

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      DIMENSION BURMIN(50),XS(10),YS(10)
C-----
C  **  INITIALIZE VARIABLES  **
C-----
      BIG = 10000.0
      DO 10 INV = 1,10
        XS(INV) = 0.0
        YS(INV) = 0.0
10  CONTINUE
      L = IPER(ICR) - 1
      LI = IPER(ICR)
      CALL BRDCHK(L,ICR,BURDPR,KKODE1,ICODE1)
      IF (WEIGHT(ICR).LT.0.2) RETURN
C-----
C  **  IF BMIN GREATER THAN DEPTH OF CONTAINED CHARGE, POINT DOES NOT
C      AFFECT DETONATION
C-----
      DCONTR = EFACR * WEIGHT(ICR)**0.5
      IF (BMIN.GT.DCONTR) GO TO 2222
C-----
C  **  FIND CRATER RADIUS FOR MINIMUM BURDEN  **
C-----
      DEPR = BMIN / DCONTR
C-----
C  **  FIND SCALED RADIUS AT THIS DEPTH RATIO  **
C-----
      DO 40 MI = 2, NPE2
        IF ((DELTBR(MI).GE.DEPR).AND.(DELTBR(MI-1).LE.DEPR)) GO TO 35
40  CONTINUE
35  SCR = SCRADB(MI-1) + (DEPR - DELTBR(MI-1))/(DELTBR(MI) -
      XDELTBR(MI-1))*(SCRADB(MI)-SCRADB(MI-1))
      RADIUS = SCR * WEIGHT(ICR)**0.5
C-----
C  **  CALCULATE SLANT DISTANCE  **
C-----
      SLANTD = (RADIUS**2.0 + BMIN**2.0)**0.5
      DO 2020 II = 2, 49
        DO 2010 JJ = 2, 49
C-----
C  **  CHECK IF POINT (II,JJ,KKK) IN PERIOD L IS INSIDE THE MASS
C      AND THEREFORE IT DOES NOT AFFECT THE DETONATION  **
C-----
        IF(itime(II,JJ).GT.L)GO TO 2000
        I11=II+1
        J11=JJ+1
        I1M=II-1
        J1M=JJ-1
C-----
C  **  POINT MAY AFFECT DETONATION. CALCULATE DISTANCE BETWEEN POINT
C      AND THE CENTRE OF THE CHARGE.
C-----
        DIST = (ABS(Y(ICR)-YB(JJ))**2.0+ABS(X(ICR)-XB(II))**2.0)**0.5
        IF(DIST.GT.SLANTD) GO TO 2010
C-----
C  **  BLOCKS FURTHER THAN THE SLANT DISTANCE DO NOT AFFECT DETONATION **

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C-----
XS(1)=XB(I1)
YS(1)=YB(J1)
DO 1025 I1=2,49
DO 1020 J1=2,49
IF((I1.EQ.I1).AND.(J1.EQ.J1)) GO TO 1020
IF(ETIME(I1,J1).GT.L) GO TO 1020
I1=I1+1
J1=J1+1
I1=I1-1
J1=J1-1
IF((IBLOCK(I1,J1).NE.0).AND.(IBLOCK(I1,J1).NE.0).AND.
X(IBLOCK(I1,J1).NE.0).AND.(IBLOCK(I1,J1).NE.0).AND.
X(ETIME(I1,J1).LE.L).AND.(ETIME(I1,J1).LE.L).AND.
X(ETIME(I1,J1).LE.L).AND.(ETIME(I1,J1).LE.L))
X GO TO 1020
DIST1=(ABS(XB(I1)-X(ICR))**2.0+ABS(YB(J1)-Y(ICR))**2.0)**0.5
IF(DIST1.LE.(DIST-0X/2.0).OR.(DIST1.GE.(DIST+0X/2.0))) GO TO 1020
XS(2) = XB(I1)
YS(2) = YB(J1)
GO TO 1030
1020 CONTINUE
1025 CONTINUE
GO TO 2010
1030 XS(3)=X(ICR)
DO 3047 MI = 2, NPBI
IF ((DELTAB(NPBI).LT.DEPR)) GO TO 3032
IF ((DELTAB(MI).GE.DEPR).AND.(DELTAB(MI-1).LE.DEPR)) GO TO 3035
IF (DELTAB(1).GE.DEPR) GO TO 3034
3047 CONTINUE
STOP
3032 SCD = SCDEPB(NPBI) - (DEPR - DELTAB(NPBI))/(1 - DELTAB(NPBI))
XSCDEPB(NPBI)
GO TO 3036
3034 SCD = (DEPR / DELTAB(1)) * SCDEPB(1)
GO TO 3036
3035 SCD = SCDEPB(MI-1) + (DEPR - DELTAB(MI-1))/(DELTAB(MI) -
XDELTAB(MI-1)) * (SCDEPB(MI) - SCDEPB(MI-1))
3036 DEPTH = SCD * WEIGH(ICR)**0.5
YS(3)=Y(ICR)
DO 1045 I1=1,50
DO 1040 J1=1,50
IF(IBLOCK(I1,J1).NE.0) GO TO 1040
XS0=XB(I1)
YS0=YB(J1)
CALL INSIDE(3,XS,YS,XS0,YS0,KKODE)
IF(KKODE.EQ.0) GO TO 1040
IBLOCK(I1,J1) = 1
ETIME(I1,J1) = IPER(ICR)
1040 CONTINUE
1045 CONTINUE
2000 CONTINUE
2010 CONTINUE
2020 CONTINUE
2222 RETURN

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A49

END

SUBROUTINE VBRCHK (IFIRST,INDEXV,KKODEI,ICODEI)

LLM06060

LLM06070

LLM06080

LLM06090

LLM06100

LLM06110

LLM06120

LLM06130

LLM06140

LLM06150

LLM06160

LLM06170

LLM06180

LLM06190

LLM06200

LLM06210

LLM06220

LLM06230

LLM06240

LLM06250

LLM06260

LLM06270

LLM06280

LLM06290

LLM06300

LLM06310

LLM06320

LLM06330

LLM06340

LLM06350

LLM06360

LLM06370

LLM06380

LLM06390

LLM06400

LLM06410

LLM06420

LLM06430

LLM06440

LLM06450

LLM06460

LLM06470

LLM06480

LLM06490

LLM06500

LLM06510

LLM06520

LLM06530

LLM06540

LLM06550

LLM06560

LLM06570

LLM06580

LLM06590

LLM06600

C

C

C PURPOSE :

C

C TO EXAMINE THE VIBRATIONS RESULTING FROM THE DETONATIONS

C OF SINGLE AND MULTIPLE CHARGES.

C

C

C

C VARIABLES :

C AKFAC : K FACTOR FOR VIBRATIONS

C ALENGT : LENGTH OF THE EXPLOSIVE COLUMN

C ALOAD : WEIGHT OF EXPLOSIVE IN CHARGE

C AMFAC : K FACTOR FOR VIBRATIONS

C DHOLE : DIAMETER OF BOREHOLE

C DIST,DISTM,DISTP : DISTANCE

C INDEXV : IF 1 VIBRATIONS EXCEED MAXIMUM

C IPER(I) : DELAY PERIOD (LOCAL)

C ITIME(I,J) : ARRAY INDICATING PERIOD IN WHICH BLOCK (I,J) WAS

C REMOVED

C MSYSUN : 1 METRIC

C 2 IMPERIAL

C NCHK : NUMBER OF POINTS FOR VIBRATION CHECK

C NDECKS : NUMBER OF DECKS

C

C

C NUMBH : NUMBER OF HOLES IN THE BLAST

C PPVALL : MAX PPV FOR POINTS

C PPVPAL : MAX PPV FOR PILLARS

C RCR : CRATER RADIUS

C SEPDIS : SEPARATION DISTANCE BETWEEN DECKS

C WEIGB : WEIGHT/UNIT LENGTH

C WEIGHT : WEIGHT OF EXPLOSIVE DECK

C WSTR : WEIGHT STRENGTH

C WTCRKB : WEIGHT OF CHARGE IN TESTS (CYLINDRICAL)

C WTCRKB : WEIGHT OF CHARGE IN TESTS (SPHERICAL)

C X(I) : X COORDINATE OF HOLE I

C Y(I) : Y COORDINATE OF HOLE I

C

CHARACTERAI KKODEI,SEQ

COMMON /RDRDT1/ DCONCH,WTCRKB,WSTRTH,SCDEPT(50),DELTA(50),

XSCRAD(50),DHOLE,X(50),Y(50),Z(50),XVCHK(10),YVCHK(10),ZVCHK(10)

X,PPVALL(10),AKFAC,AMFAC,XPIL1(10),XPIL2(10),XPIL3(10),YPIL1(10),

XPIL2(10),YPIL3(10),ZPIL1(10),ZPIL2(10),ZPIL3(10),PPVPAL,WSTR,

XXMAX,XMIN,YMAX,YMIN,ZMAX,ZMIN,DELTAR(50),RHOE,DCONCB,SCDEPB(50),

XDELTAR(50),SCRADB(50),DELTBR(50),WTCRKB,ALENGT,BMIN,SEPDIS

COMMON/RDRDT2/ NP1,NPB1,NP2,NPB2,NUMBH,NCHK,NUMPIL,INIT(50),NCONTR

X,NOTAL,MSYSUN

COMMON/CHARGE/WEIGHT(50),WEIGB(50),DOPT(50),RCR(50),DEPTH(50),

XSCRAP,DOPTH(50)

COMMON/DELT/DELTO,EFACTR,DELTOB,EFACTR

COMMON/ISEQ/ IPER(50),KK,NR,NCH(50),NDECKS

COMMON/CONTR/XCONT1(10),XCONT2(10),YCONT1(10),YCONT2(10)

COMMON/REFER/ XREFER,YREFER,ZREFER,STANGR,STLENG,STWIDT,

X STDEPT


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      DIMENSION ALOAD(50),PPV(10),PPVPIL(10),WEIGMX(50),ID(50),TOP(50) LLM06610
C----- LLM06620
C ** INITIALIZE VARIABLES ** LLM06630
C----- LLM06640
      DO 2 I = 1,50 LLM06650
        ID(I) = 0 LLM06660
      2 CONTINUE LLM06670
      WEIGMX(1) = 100000.0 LLM06680
      INDEXV = 0 LLM06690
C----- LLM06700
C ** FIND CHARGES DETONATING IN THE SAME PERIOD ** LLM06710
C----- LLM06720
      KK = 0 LLM06730
      DO 100 IA = 1, NUMBH LLM06740
        IF (IPER(IA).NE.ICFIRST) GO TO 100 LLM06750
C----- LLM06760
C **          LOAD HOLE          ** LLM06770
C----- LLM06780
      PI = 3.14159 LLM06790
      ALOAD(IA) = (12.0*ALENGT * PI * DHOLE ** 2.0 / 4.0) * RHOE LLM06800
      IF(MSYSUN.EQ.1) ALOAD(IA) = (100.0*ALENGT*PI*DHOLE**2.0/4.0)*RHOE LLM06810
      X/1000.0 LLM06820
C----- LLM06830
C ** CALCULATE EQUIVALENT WEIGHT OF EXPLOSIVE ** LLM06840
C----- LLM06850
      WEIGHT(IA) = ALOAD(IA) * WSTR / WSTRTH LLM06860
      WEIGB(IA) = WEIGHT(IA)/ALENGT LLM06870
      IF (NTOTAL.NE.NDECKS) GO TO 20 LLM06880
      CALL TOPH(IA,TOP(IA)) LLM06890
      ALOAD(IA) = (12.0*(SEPDIS+ALENGT-TOP(IA))*PI*DHOLE**2.0/4.0)*RHOE LLM06900
      IF(MSYSUN.EQ.1) ALOAD(IA) = ALOAD(IA)/12.0 * 0.1 LLM06910
      IF (ALOAD(IA).GT.0.0) GO TO 11 LLM06920
      ALOAD(IA) = 0.0 LLM06930
      WEIGHT(IA) = 0.0 LLM06940
      GO TO 200 LLM06950
      11 WEIGHT(IA) = ALOAD(IA) * WSTR/WSTRTH LLM06960
C----- LLM06970
C ** CHECK VIBRATION LEVELS ** LLM06980
C----- LLM06990
      20 IF(NCHK.EQ.0) GO TO 32 LLM07000
C----- LLM07010
C ** CALCULATE DISTANCES FROM POINTS LLM07020
C----- LLM07030
      DO 30 I = 1, NCHK LLM07040
        CALL DISTPT(XVCHK(I),YVCHK(I),ZVCHK(I),X(IA),Y(IA),Z(IA),DIST) LLM07050
C----- LLM07060
C ** CALCULATE PPV AT THIS POINT ** LLM07070
C----- LLM07080
      PPV(I) = AKFAC*(DIST/WEIGHT(IA)**(1.0/2.0))**AMEFAC LLM07090
C----- LLM07100
C ** FIND MAXIMUM WEIGHT FOR THIS PARTICULAR POINT ** LLM07110
C----- LLM07120
      WEIGMX(I) = (AKFAC/PPVALL(I))**((2.0/AMEFAC)*DIST**2.0 LLM07130
      30 CONTINUE LLM07140
C----- LLM07150

```

C	AA	CALCULATE DISTANCE FROM PILLARS	AA	LLM07160
C		32 IF (NUMPIL.EQ.0) GO TO 52		LLM07170
		DO 50 I = 1, NUMPIL		LLM07180
		CALL DISTPL(XPIL1(I),YPIL1(I),ZPIL1(I),XPIL2(I),YPIL2(I),ZPIL2(I),		LLM07190
		XXPIL3(I),YPIL3(I),ZPIL3(I),X(IA),Y(IA),Z(IA),DISTP)		LLM07200
				LLM07210
C	AA	CALCULATE PPV AT THIS POINT	AA	LLM07220
C				LLM07230
		PPVPIL(I) = AKIAC * (DISTP/WEIGHT(IA))**(.5/2.0)**		LLM07240
		X AMEAC		LLM07250
				LLM07260
C	AA	FIND MAXIMUM WEIGHT BECAUSE OF THIS PARTICULAR PILLAR	AA	LLM07270
C				LLM07280
		WEIGMX(NCHK+1) = (AKEAC/PPVPAL)**(2.0/AMEAC)*DISTP**2.0		LLM07290
		50 CONTINUE		LLM07300
				LLM07310
C	AA	FIND MINIMUM ACCEPTABLE WEIGHTS	AA	LLM07320
C				LLM07330
		52 WMIN = WEIGMX(1)		LLM07340
		NN = NCHK + NUMPIL		LLM07350
		IF (NN.EQ.0) GO TO 99		LLM07360
		DO 80 I = 1, NN		LLM07370
		IF (WEIGMX(I).LT.WMIN) WMIN=WEIGMX(I)		LLM07380
		80 CONTINUE		LLM07390
		IF (WEIGHT(IA).LE.WMIN) GO TO 99		LLM07400
		WEIGHT(IA) = WMIN		LLM07410
		99 KK = KK + 1		LLM07420
		INIT(KK) = IA		LLM07430
		100 CONTINUE		LLM07440
		IF(NN.EQ.0) GO TO 200		LLM07450
				LLM07460
C				LLM07470
C		CHECK VIBRATIONS DUE TO THE SIMULTANEOUS DETONATION OF		LLM07480
C		MANY CHARGES		LLM07490
C				LLM07500
C				LLM07510
C	AA	FIND AN AVERAGE POSITION OF THE CONCENTRATED CHARGE	AA	LLM07520
C				LLM07530
		XM = 0.0		LLM07540
		IF(KK.EQ.1) GO TO 200		LLM07550
		YM = 0.0		LLM07560
		ZM = 0.0		LLM07570
		WM = 0.0		LLM07580
		DO 110 I = 1, KK		LLM07590
		IM = INIT(I)		LLM07600
		XM = XM + X(I)*WEIGHT(IM)		LLM07610
		YM = YM + Y(I)*WEIGHT(IM)		LLM07620
		ZM = ZM + Z(I)*WEIGHT(IM)		LLM07630
		WM = WM + WEIGHT(IM)		LLM07640
		110 CONTINUE		LLM07650
		XM = XM / WM		LLM07660
		YM = YM / WM		LLM07670
		ZM = ZM / WM		LLM07680
				LLM07690
C				LLM07700

C	AA	CALCULATE DISTANCE FROM POINTS	AA	LLM07710
C		IF (NCHK.EQ.0) GO TO 131		LLM07720
		DO 130 I = 1, NCHK		LLM07730
		CALL DISTPT(XVCHK(I),YVCHK(I),ZVCHK(I),XM,YM,ZM,DISTM)		LLM07740
C				LLM07750
C	AA	CALCULATE PPV AT THIS POINT	AA	LLM07760
C		PPV(I) = AKFAC*(DISTM/WMA(1.0/2.0))	AA AMFAC	LLM07770
C				LLM07780
C	AA	FIND MAXIMUM WEIGHT FOR THIS PARTICULAR POINT	AA	LLM07790
C		WEIGMX(I) = (AKFAC/PPVALL(I))*((2.0/AMFAC)*DISTM**2.0		LLM07800
		130 CONTINUE		LLM07810
C				LLM07820
C	AA	SAME FOR PILLARS		LLM07830
C				LLM07840
		131 IF (NUMPIL.EQ.0) GO TO 151		LLM07850
		DO 150 I = 1, NUMPIL		LLM07860
		CALL DISTPL(XPIL1(I),YPIL1(I),ZPIL1(I),XPIL2(I),YPIL2(I),ZPIL2(I),		LLM07870
		X XPIL3(I),YPIL3(I),ZPIL3(I),XM,YM,ZM,DISTM)		LLM07880
		PPVPIL(I) = AKFAC*((DISTM)/WMA**((1.0/2.0)))*AMFAC		LLM07890
		WEIGMX(NCHK+I) = (AKFAC/PPVPIL)*((2.0/AMFAC)*DISTM**2.0		LLM07900
		150 CONTINUE		LLM07910
C				LLM07920
C	AA	FIND MINIMUM OF ACCEPTABLE WEIGHTS	AA	LLM07930
C				LLM07940
		151 WHIN = 2000000.0		LLM07950
		NN = NCHK + NUMPIL		LLM07960
		IF (NN.EQ.0) GO TO 200		LLM07970
		DO 180 I = 1, NN		LLM07980
		IF(WEIGMX(I).LT.WHIN) WHIN = WEIGMX(I)		LLM07990
		180 CONTINUE		LLM08000
		IF (WH.LE.WHIN) GO TO 200		LLM08010
		IF (KKODE1.NE.'N') GO TO 192		LLM08020
		IF (ICODE1.EQ.1)GO TO 199		LLM08030
		WRITE(7,187)		LLM08040
		187 FORMAT(' THE NUMBER OF CHARGES DETONATING IN THIS PERIOD IS',/		LLM08050
		X' TOO LARGE RESULTING IN UNACCEPTABLE VIBRATIONS.',/		LLM08060
		X' DO YOU WANT TO CHANGE THE SEQUENCING OF THE CHARGES ? (Y/N)')		LLM08070
		PEAD (7,188) SEQ		LLM08080
		188 FORMAT(1A1)		LLM08090
		INDEXV = 1		LLM08100
		IF(SEQ.EQ.'Y') GO TO 191		LLM08110
		INDEXV = 0		LLM08120
		GO TO 200		LLM08130
		192 INDEXV = 1		LLM08140
		191 DO 190 I = 1,NUMBH		LLM08150
		IF(IPER(I).NE.IFIRST) GO TO 190		LLM08160
		WEIGHT(I) = 0.0		LLM08170
		WEIGR(I) = 0.0		LLM08180
		IPER(I) = 100000		LLM08190
		190 CONTINUE		LLM08200
		GO TO 200		LLM08210
		199 INDEXV = 1		LLM08220
				LLM08230
				LLM08240
				LLM08250


```

      IF (DENOM.EQ.0.0) ANGL=PP/2.  

      IF (DENOM.EQ.0.0.AND.ANOM.LT.0.0) ANGL=-PP/2.  

      X1=X2  

      Y1=Y2  

      IF (DENOM.LT.0.0.AND.ANGL.EQ.0.0) KODE=KPN  

      IF (KODE.EQ.KPN) RETURN  

-----  

C   IF ANGL=180. THE POINT FALLS ON THE AREA BOUNDARY  

-----  

      IF (ANGL.LT.0.0.AND.ANOM.GT.0.0) ANGL=ANGL+PP  

      IF (ANGL.GT.0.0.AND.ANOM.LT.0.0) ANGL=ANGL-PP  

      SUM=SUM+ANGL  

401 CONTINUE  

      P22 = 2.0A PP  

      P44 = 4.0A PP  

      P66 = 6.0A PP  

-----  

C   IF SUM =0. THE POINT FALLS OUTSIDE THE AREA BOUNDARY  

-----  

      IF (ABS(SUM).LT.0.3) KODE=0  

      IF (ABS(SUM).LT.0.3) RETURN  

-----  

C   IF SUM =2APP THE POINT FALLS INSIDE THE AREA BOUNDARY  

-----  

      IF (ABS(SUM).GT.(2.0APP-0.3)) KODE=-1  

      IF (KODE.EQ.(-1)) RETURN  

-----  

C   SHOULD NOT GET HERE. ENTER AN ERROR CODE  

-----  

      KODE = -2  

      RETURN  

      END  

      SUBROUTINE BRDCHK(L,ICR,BURDPF,KKODEI,ICODEI)  

CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC LLM09690  

C  

C   PURPOSE :  

C           TO CHECK BURDENS OF NEW CHARGE TO THE PREVIOUS  

C               CRATERS AND DETERMINE IF THE CHARGE IS IN  

C               THE FLYROCK REGION.  

C  

CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC LLM09760  

C  

C   VARIABLES :  

C       ALENGT : LENGTH OF THE EXPLOSIVE COLUMN  

C       BCHKI  : BURDEN  

C       BCHECK : BURDEN  

C       BKTHK  : KODE INDICATING IF THE HOLES ARE BREAKTHROUGH  

C       BMIN   : MINIMUM BURDEN  

C       BURDPF : BURDEN OF INITIAL PATTERN  

C       DELTO  : OPTIMUM DEPTH RATIO ( SPHERICAL )  

C       DELTOR : OPTIMUM DEPTH RATIO ( CYLINDRICAL )  

C       DHOLE  : DIAMETER OF BOREHOLE  

C       EFACIB : STRAIN ENERGY FACTOR FOR CYLINDRICAL CHARGES  

C       EFACK  : STRAIN ENERGY FACTOR FOR SPHERICAL CHARGES  

C       ELEV   : ELEVATION  


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A56

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C      EXPTY9 : EXPLOSIVE TYPE                      LLM09910
C      EXPTYP : EXPLOSIVE TYPE                      LLM09920
C      INDEXV : IF 1 VIBRATIONS EXCEED MAXIMUM      LLM09930
C      ITIME(1,J) : ARRAY INDICATING PERIOD IN WHICH BLOCK (I,J) WAS LLM09940
C      REMOVED                                       LLM09950
C      MSYSUN : 1 METRIC                             LLM09960
C      2 IMPERIAL                                   LLM09970
C      RATIO : RATIO BURDEN TO ADJACENT FREE FACE/OPTIMUM BURDEN LLM09980
C      SEPDIS : SEPARATION DISTANCE BETWEEN DECKS   LLM09990
C      WEIGH : WEIGHT/UNIT LENGTH                   LLM10000
C      WEIGHT : WEIGHT OF EXPLOSIVE DECK             LLM10010
C      X(1) : X COORDINATE OF HOLE 1                 LLM10020
C      XB(I) : X COORDINATE OF POINT I (BLOCK I,J)  LLM10030
C      Y(1) : Y COORDINATE OF HOLE 1                 LLM10040
C      YB(J) : Y COORDINATE OF POINT J (BLOCK I,J)  LLM10050
C----- LLM10060
C      CHARACTER*1 KKODE1                           LLM10070
C      COMMON /RDRDT1/ DCNCH,WTCHRG,WSTRTH,SCDEPT(50),DELTA(50), LLM10080
C      XSCRAD(50),DHOLE,X(50),Y(50),Z(50),XVCHK(10),YVCHK(10),ZVCHK(10) LLM10090
C      X.PPVALL(10),AKEAC,AMEAC,XPIL1(10),XPIL2(10),XPIL3(10),YPIL1(10), LLM10100
C      YPIL2(10),YPIL3(10),ZPIL1(10),ZPIL2(10),ZPIL3(10),PPVPAL,WSTR, LLM10110
C      XXMAX,XMIN,YMAX,YMIN,ZMAX,ZMIN,DELTAR(50),RHDE,DCDNCH,SCDEPB(50), LLM10120
C      XDeltar(50),SCRADB(50),DELTBR(50),WTCHRB,ALNGT,BMIN,SEPDIS LLM10130
C      COMMON/IBLK/ IBLOCK(100,100),ITIME(100,100) LLM10140
C      COMMON/DELT/DELTO,EFACTR,DELTOB,EFACTB LLM10150
C      COMMON/XBLK/XB(100),YB(100) LLM10160
C      COMMON/ISER/ IPER(50),KK,NR,NCH(50),NDECKS LLM10170
C      COMMON/CHARGE/WEIGHT(50),WEIGH(50),DOPT(50),RCR(50),DEPTH(50), LLM10180
C      XSCROP,DOPTB(50) LLM10190
C      COMMON/RDRDT2/ NP1,NP11,NP2,NP22,NUMBH,NCHK,NUMPIL,INIT(50),NCONTE LLM10200
C      X ,NTOTAL,MSYSUN LLM10210
C      COMMON/REFER/ XREFER,YREFER,ZREFER,STANGR,STLENG,STWIDT, LLM10220
C      X STDEPT LLM10230
C      DIMENSION IPREV(50) , DIST(50,50) LLM10240
C----- LLM10250
C      *** INITIALIZE *** LLM10260
C----- LLM10270
C      BMIN = 100000.0 LLM10280
C      DO 100 I= 1,50 LLM10290
C      DO 90 J=1,50 LLM10300
C      IF (ITIME(I,J).GT.IPER(100)) GO TO 90 LLM10310
C      DISTAN=(ABS(X(ICR)-XB(I))**2.0+ABS(Y(ICR)-YB(J))**2.0)**0.5 LLM10320
C      IF (DISTAN.GE.BMIN) GO TO 90 LLM10330
C      BMIN = DISTAN LLM10340
C      90 CONTINUE LLM10350
C      100 CONTINUE LLM10360
C      BCHECK = 1.1*BURDPE LLM10370
C      IF (BMIN.LT.BCHECK) GO TO 220 LLM10380
C----- LLM10390
C      ** CHECK SEPARATION DISTANCE ** LLM10400
C----- LLM10410
C      SEPMIN = DHOLE LLM10420
C      SEPDI = SEPDIS - SEPMIN LLM10430
C      IF (SEPDI.LE.0.05) GO TO 150 LLM10440
C      RATIO = SEPDI/SEPDIS LLM10450

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A58

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      X      Y1*(Z2-Z1)*(X3-X1) - Z1*(X2-X1)*(Y3-Y1)
      A2 = ABS(A1)
      B2 = ABS(B1)
      C2 = ABS(C1)
      DENOM = A2**2.0 + B2**2.0 + C2**2.0
      IF(DENOM.LE.1E-15) GO TO 10
      DD= (A1*X + B1*Y + C1*Z + D1) / (A2**2.0 + B2**2.0 + C2**2.0)**0.5
      D = ABS (DD)
      RETURN
10  IBUG = 1
      RETURN
      END
      SUBROUTINE DISTPT(X1,Y1,Z1,X,Y,Z,D)
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC C
C  PURPOSE :
C      TO CALCULATE THE DISTANCE BETWEEN TWO POINTS.
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC C
C  VARIABLES :
C
C      *** INPUT ***
C      X,Y,Z,X1,Y1,Z1 : THE X, Y, Z COORDINATES OF THE TWO POINTS.
C
C      *** OUTPUT ***
C      D : THE DISTANCE
C
      A = ABS(X-X1)
      B = ABS(Y-Y1)
      C = ABS(Z-Z1)
      D = (A**2.0 + B**2.0 + C**2.0)**0.5
      RETURN
      END
      SUBROUTINE DISPLN(X1,Y1,X2,Y2,X,Y,DISTA,IBUG)
      IBUG = 0
      A1= Y1 - Y2
      B1= X2 - X1
      C1= X1*Y2-X2*Y1
      A = ABS(A1)
      B = ABS(B1)
      DENOM = A**2.0 + B**2.0
      IF(DENOM.LE.1.E-25) GO TO 10
      DISTA=ABS(A1*X + B1*Y + C1)/DENOM**0.5
      RETURN
10  IBUG = 1
      RETURN
      END
      SUBROUTINE READER(NPFF)
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC C
C
C  PURPOSE : TO READ GENERAL DATA FOR THE DESIGN OF THE VCR BLAST
C  THE DATA ARE READ FROM THE FOLLOWING UNITS :
C  UNIT 7 - TERMINAL ( INTERACTIVELY )
C  UNIT 8 - DISK FILE WITH THE DATA FOR THE CRATERING CURVES
C  UNIT 9 - DISK FILE WITH DATA FOR THE STOPE
C  UNIT 10 - INITIATION SEQUENCE

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CHARACTER*1 IWR,BRTHR
CHARACTER*4 FT,INCH,LBS
C-----
C  **          INCLUDE COMMONS          **
C-----
COMMON /RDRDT1/ DCONCH,WCHRG,WSTRTH,SCDEPT(50),DELTA(50),
XSCRAD(50),DHOLE,X(50),Y(50),Z(50),XVCHK(10),YVCHK(10),ZVCHK(10),
X,PPVALL(10),AKFAC,AMFAC,XPIL1(10),XPIL2(10),XPIL3(10),YPIL1(10),
XPIL2(10),YPIL3(10),ZPIL1(10),ZPIL2(10),ZPIL3(10),PPVPAL,WSTR,
XXMAX,XMIN,YMAX,YMIN,ZMAX,ZMIN,DELTAR(50),RHOE,DCONCB,SCDEPB(50),
XDELTAB(50),SCRADB(50),DELTBR(50),WCHRB,ALNGT,BMIN,SEPDIS
COMMON/RDRDT2/ NP1,NPB1,NP2,NPB2,NUMBH,NCHK,NUMPIL,INIT(50),NCONTR
X ,NTOTAL,MSYSUN
COMMON/ISEQ/ IPER(50),KK,NR,NCH(50),NDECKS
COMMON/CHARGE/WEIGHT(50),WEIGB(50),DOPT(50),RCR(50),DEPTH(50),
XSCROP,DOPTB(50)
COMMON/TYPE/EXPTYP,EXPTYB
COMMON/TT/TITLE
COMMON/FREEF/ XFF(10),YFF(10)
COMMON/ALPHA/ IWR(100,100),BRTHR
COMMON/CONTR/ XCONT1(10),XCONT2(10),YCONT1(10),YCONT2(10)
COMMON/REFER/ XREFER,YREFER,ZREFER,STANGR,STLENG,STWIDT,
X SIDEPT
COMMON/UNALP/LBS,INCH,FT
C-----
C  **  READ CRATERING CHARACTERISTICS  **
C-----
WRITE(7,8)
8 FORMAT(' WRITE TITLE TO IDENTIFY PROBLEM')
READ(7,1007) TITLE
1007 FORMAT(A80)
WRITE(7,9)
9 FORMAT(' ENTER TYPE OF EXPLOSIVE USED FOR TESTS')
READ(7,1009) EXPTYP
1009 FORMAT(A15)
WRITE(7,1010)
1010 FORMAT(' ENTER SYSTEM OF UNITS YOU ARE USING :',/
X' (1) M E T R I C',/
X' (2) I M P E R I A L ')
READ(7,* ) MSYSUN
IF (MSYSUN.EQ.1) GO TO 1020
LBS=' LBS'
FT = ' FT '
INCH = ' INCH '
GO TO 1030
1020 LBS = ' KG '
FT = ' M '
INCH = ' CM '
1030 WRITE(7,10) FT,LBS
10 FORMAT(' ENTER DEPTH OF CONTAINED CHARGE ('.A4,')',/,
X' WEIGHT OF EXPLOSIVE ('.A4,')',/,
X' FOR SPHERICAL CHARGES.',/
X' ----- ')
READ(7,*) DCONCH, WCHRG
WRITE(7,2010) FT,LBS

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2010 FORMAT (' ENTER DEPTH OF CONTAINED CHARGE ('.A4.').',/,
X          ' WEIGHT OF EXPLOSIVE ('.A4.').',/,
X          ' FOR CYLINDRICAL CHARGES.',/,
X          ' -----')
READ (7,A) DCUNCB, WICHRB
WRITE (7,11)
11 FORMAT (' WHAT IS THE WEIGHT STRENGTH OF THE EXPLOSIVE',/
X          ' RELATIVE TO AN/FO ?')
READ (7,A) WSTREN
C-----
C  **          READ CRATERING CURVES          **
C-----
WRITE (7,12)
12 FORMAT (' DO YOU WANT TO INPUT NEW CRATERING CURVES ? ')
READ (7,13) KODE
13 FORMAT (1A1)
IF (KODE.EQ.'N') GO TO 30
WRITE (7,14)
14 FORMAT (' ENTER NUMBER OF POINTS TO DESIGN THE ',/
X          ' SCALED CRATER DEPTH - DEPTH RATIO',/
X          ' CURVE FOR SPHERICAL CHARGES: ',/
X          ' -----')
READ (7,A) NP1
WRITE (8,15) NP1
15 FORMAT (15)
WRITE (7,16)
16 FORMAT(' ENTER SCALED DEPTH, DEPTH RATIO ',/
X          ' FOR EACH POINT OF THE CURVE.')
DO 19 I = 1, NP1
READ (7,A) SCDEPT(I), DELTA(I)
WRITE(8,18) SCDEPT(I), DELTA(I)
18 FORMAT(2F10.4)
19 CONTINUE
WRITE(7,20)
20 FORMAT(' ENTER NUMBER OF POINTS TO DESIGN ',/
X          ' THE SCALED CRATER RADIUS - DEPTH RATIO',/
X          ' CURVE FOR SPHERICAL CHARGES: ',/
X          ' -----')
READ (7,A) NP2
WRITE(8,15) NP2
WRITE(7,26)
26 FORMAT(' ENTER SCALED CRATER RADIUS, DEPTH RATIO',/
X          ' FOR EACH POINT OF THE CURVE.')
DO 29 I = 1, NP2
READ (7,A) SCRAD(I), DELTAR(I)
WRITE(8,18) SCRAD(I), DELTAR(I)
29 CONTINUE
WRITE (7,2014)
2014 FORMAT (' ENTER NUMBER OF POINTS TO DESIGN THE ',/
X          ' SCALED CRATER DEPTH - DEPTH RATIO',/
X          ' CURVE FOR CYLINDRICAL CHARGES: ',/
X          ' -----')
READ (7,A) NPB1
WRITE (8,2015) NPB1
2015 FORMAT (15)

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LLM12660
 LLM12670
 LLM12680
 LLM12690
 LLM12700
 LLM12710
 LLM12720
 LLM12730
 LLM12740
 LLM12750
 LLM12760
 LLM12770
 LLM12780
 LLM12790
 LLM12800
 LLM12810
 LLM12820
 LLM12830
 LLM12840
 LLM12850
 LLM12860
 LLM12870
 LLM12880
 LLM12890
 LLM12900
 LLM12910
 LLM12920
 LLM12930
 LLM12940
 LLM12950
 LLM12960
 LLM12970
 LLM12980
 LLM12990
 LLM13000
 LLM13010
 LLM13020
 LLM13030
 LLM13040
 LLM13050
 LLM13060
 LLM13070
 LLM13080
 LLM13090
 LLM13100
 LLM13110
 LLM13120
 LLM13130
 LLM13140
 LLM13150
 LLM13160
 LLM13170
 LLM13180
 LLM13190
 LLM13200

WRITE (7,2016)	LLM13210
2016 FORMAT(' ENTER SCALED DEPTH, DEPTH RATIO ',/	LLM13220
X ' FOR EACH POINT OF THE CURVE.')	LLM13230
DO 2019 I = 1, NPB1	LLM13240
READ (7,A) SCDEPR(I), DELTAB(I)	LLM13250
WRITE(8,2018) SCDEPR(I), DELTAB(I)	LLM13260
2018 FORMAT(2F10.4)	LLM13270
2019 CONTINUE	LLM13280
WRITE(7,2020)	LLM13290
2020 FORMAT(' ENTER NUMBER OF POINTS TO DESIGN ',/	LLM13300
X ' THE SCALED CRATER RADIUS - DEPTH RATIO',/	LLM13310
X ' CURVE FOR CYLINDRICAL CHARGES :',/	LLM13320
X ' -----')	LLM13330
READ (7,A) NPB2	LLM13340
WRITE(8,2015) NPB2	LLM13350
WRITE(7,2026)	LLM13360
2026 FORMAT(' ENTER SCALED CRATER RADIUS, DEPTH RATIO',/	LLM13370
X ' FOR EACH POINT OF THE CURVE.')	LLM13380
DO 2029 I = 1, NPB2	LLM13390
READ (7,A) SCRADB(I), DELTBR(I)	LLM13400
WRITE(8,2018) SCRADB(I), DELTBR(I)	LLM13410
2029 CONTINUE	LLM13420
GO TO 40	LLM13430
C-----	LLM13440
C ** READ CURVES FROM FILE **	LLM13450
C-----	LLM13460
30 READ (8,15) NP1	LLM13470
READ (8,18) ((SCDEPT(I), DELTA(I)), I=1,NP1)	LLM13480
READ (8,15) NP2	LLM13490
READ (8,18) ((SCRADB(I), DELTAR(I)), I=1,NP2)	LLM13500
READ (8,2015) NPB1	LLM13510
READ (8,2018) ((SCDEPR(I), DELTAB(I)), I=1,NPB1)	LLM13520
READ (8,2015) NPB2	LLM13530
READ (8,2018) ((SCRADB(I), DELTBR(I)), I=1,NPB2)	LLM13540
40 CONTINUE	LLM13550
C-----	LLM13560
C ** READ DATA OF THE STOPE **	LLM13570
C-----	LLM13580
WRITE(7,201)	LLM13590
201 FORMAT(' ENTER THE DIAMETER OF THE BLASTHOLES (INCHES) :')	LLM13600
READ (7,A) DHOLE	LLM13610
WRITE(7,202)	LLM13620
202 FORMAT(' ENTER NUMBER OF HOLES IN THE BLAST :')	LLM13630
READ (7,A) NUMBH	LLM13640
WRITE(7,204)	LLM13650
204 FORMAT(' ENTER NUMBER OF ROWS IN THE BLAST :')	LLM13660
READ (7,A) NR	LLM13670
DO 208 I = 1, NR	LLM13680
WRITE(7,206) I	LLM13690
206 FORMAT(' ENTER NUMBER OF HOLES IN ROW ',I2,' :')	LLM13700
READ (7,A) NCH(I)	LLM13710
208 CONTINUE	LLM13720
WRITE(7,2001)	LLM13730
2001 FORMAT(' ARE THE HOLES BREAKTHROUGH HOLES ?')	LLM13740
READ (7,2002) BRYNR	LLM13750

2002 FORMAT(1A1)

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C-----
C  **  READ DATA FOR VIBRATION CHECKS  **
C  SPECIFY POINTS OF PARTICULAR INTEREST AND ACCEPTABLE
C  VIBRATIONS IN THESE POINTS.
C-----
      WRITE (7,250)
250 FORMAT('  THE FOLLOWING DATA ARE FOR CHECKING VIBRATION',/
X      '  LEVELS AT PILLARS AND OTHER PARTICULAR POINTS',/
X      '  OF INTEREST ....',/
X      '  ARE THESE NEW OR PREVIOUS DATA ?')
      READ (7,13) KODE
      IF (KODE.EQ.'P') GO TO 490
      WRITE(7,270)
270 FORMAT('  ENTER THE NUMBER OF POINTS IN WHICH VIBRATIONS ARE',/
X      '  TO BE CHECKED:')
      READ (7,*) NCHK
      IF(NCHK.EQ.0) GO TO 331
      WRITE(11,280)
280 FORMAT(15)
      WRITE(7,300)
300 FORMAT('  ENTER SPECIFIC POINTS IN WHICH VIBRATIONS WILL BE',
X      '  CHECKED.',/
X      '  ( EACH POINT MUST BE SPECIFIED BY ITS COORDINATES SEPARATED',/
X      '  BY COMMAS, AND THE MAXIMUM ACCEPTABLE LEVEL OF PEAK PARTICLE'
X      '  VELOCITY. E.G. 12.4,12.6,14.2,10.0)')
      DO 315 I = 1, NCHK
      READ (7,*) XVCHK(I), YVCHK(I), ZVCHK(I), PPVALL(I)
C-----
C  **  CONVERT TO LOCAL COORDINATES  **
C-----
      REWIND 51
      READ(51,519) TITLE
      READ(51,520) XREFER,YREFER,ZREFER
      READ(51,520) STLENG,STWIDT,STDEPT
      READ(51,520) STANGR
      STANGR=3.14159*STANGR/180.0
519 FORMAT(A80)
520 FORMAT(4F10.2)
      XVCHK(I) = XVCHK(I) - XREFER
      YVCHK(I) = YVCHK(I) - YREFER
      ZVCHK(I) = ZVCHK(I) - ZREFER
      XC = XVCHK(I)*COS(STANGR) + YVCHK(I)*SIN(STANGR)
      YC = -XVCHK(I)*SIN(STANGR) + YVCHK(I)*COS(STANGR)
      XVCHK(I) = XC
      YVCHK(I) = YC
      WRITE(11,310) XVCHK(I), YVCHK(I), ZVCHK(I), PPVALL(I)
310 FORMAT(4F15.5)
315 CONTINUE
      WRITE(7,320)
320 FORMAT('  ENTER THE SITE FACTORS K, M FOR THE CALCULATION OF THE',
X      '  PEAK PARTICLE',/
X      '  VELOCITY :')
      READ (7,*) AKFAC, AMFAC
      WRITE(11,330) AKFAC, AMFAC
330 FORMAT (2F15.5)

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A64

331	CONTINUE	LLM14310
C	-----	LLM14320
C	** ENTER DATA FOR PILLARS **	LLM14330
C	-----	LLM14340
	WRITE (7,430)	LLM14350
430	FORMAT(' ARE THERE ANY PILLARS IN WHICH YOU WOULD LIKE TO CHECK '	LLM14360
	X, 'VIBRATIONS ?')	LLM14370
	READ (7,431) KODE1	LLM14380
431	FORMAT (1A1)	LLM14390
	IF (KODE1.EQ.'N') GO TO 490	LLM14400
	WRITE(7,440)	LLM14410
440	FORMAT(' ENTER NUBER OF PILLARS :')	LLM14420
	READ (7,*) NUMPIL	LLM14430
	WRITE(11,450) NUMPIL	LLM14440
450	FORMAT(I5)	LLM14450
	DO 480 I = 1, NUMPIL	LLM14460
	WRITE(7,460) I	LLM14470
460	FORMAT(' ENTER X, Y, Z, COORDINATES OF THE 1ST POINT OF PILLAR',	LLM14480
	X' NO.', I3)	LLM14490
	READ (7,*) XPIL1(I), YPIL1(I), ZPIL1(I)	LLM14500
	WRITE(11,470) XPIL1(I), YPIL1(I), ZPIL1(I)	LLM14510
470	FORMAT (3F15.5)	LLM14520
	WRITE(7,471) I	LLM14530
471	FORMAT(' ENTER X, Y, Z, COORDINATES OF THE 2ND POINT OF PILLAR',	LLM14540
	X' NO.', I3)	LLM14550
	READ (7,*) XPIL2(I), YPIL2(I), ZPIL2(I)	LLM14560
	WRITE(11,470) XPIL2(I), YPIL2(I), ZPIL2(I)	LLM14570
	WRITE(7,473) I	LLM14580
473	FORMAT(' ENTER X, Y, Z, COORDINATES OF THE 3RD POINT OF PILLAR',	LLM14590
	X' NO.', I3)	LLM14600
	READ (7,*) XPIL3(I), YPIL3(I), ZPIL3(I)	LLM14610
	WRITE(11,470) XPIL3(I), YPIL3(I), ZPIL3(I)	LLM14620
480	CONTINUE	LLM14630
	WRITE(7,482)	LLM14640
482	FORMAT (' ENTER MAXIMUM ACCEPTABLE LEVEL FOR PEAK PARTICLE ',	LLM14650
	X 'VELOCITY ', '/' IN THE PILLAR')	LLM14660
	READ (7,*) PPVPAL	LLM14670
	WRITE(11,484) PPVPAL	LLM14680
484	FORMAT(I5)	LLM14690
	GO TO 500	LLM14700
C	-----	LLM14710
C	** READ FROM FILE **	LLM14720
C	-----	LLM14730
490	IF (KODE.NE.'P') GO TO 500	LLM14740
	READ (11,280) NCHK	LLM14750
	DO 420 I = 1, NCHK	LLM14760
	READ (11,310) XVCHK(I), YVCHK(I), ZVCHK(I), PPVALL(I)	LLM14770
420	CONTINUE	LLM14780
	READ(11,450) NUMPIL	LLM14790
	DO 498 I = 1, NUMPIL	LLM14800
	READ(11,470) XPIL1(I), YPIL1(I), ZPIL1(I)	LLM14810
	READ(11,470) XPIL2(I), YPIL2(I), ZPIL2(I)	LLM14820
	READ(11,470) XPIL3(I), YPIL3(I), ZPIL3(I)	LLM14830
498	CONTINUE	LLM14840
	READ(11,484) PPVAL	LLM14850

```
500 CONTINUE
C-----
C  **  READ COORDINATES OF THE FREE FACE  **
C-----
      READ (9,*) NPFF
      READ (9,213)((XFF(I),YFF(I)),I=1,NPFF)
213 FORMAT(2F15.5)
C-----
C  **  CONVERT TO LOCAL COORDINATES  **
C-----
      DO 511 I = 1,NPFF
      XFF(I) = XFF(I) - XREFER
      YFF(I) = YFF(I) - YREFER
      XC = XFF(I)*ACOS(STANGR) + Y(I)*ASIN(STANGR)
      YC = -XFF(I)*ASIN(STANGR) + YFF(I)*ACOS(STANGR)
      XFF(I) = XC
      YFF(I) = YC
511 CONTINUE
C-----
C  **  READ LINE OF FINAL WALL IN THE TOP LEVEL **
C-----
      READ(12,*) NCONTR
      IF (NCONTR.EQ.0) GO TO 4100
      DO 4050 I = 1,NCONTR
      READ(12,4051) XCONT1(I),YCONT1(I),XCONT2(I),YCONT2(I)
4051 FORMAT(4F10.2)
      XCONT1(I) = XCONT1(I) - XREFER
      YCONT1(I) = YCONT1(I) - YREFER
      XC = XCONT1(I)*ACOS(STANGR) + YCONT1(I)*ASIN(STANGR)
      YC = -XCONT1(I)*ASIN(STANGR) + YCONT1(I)*ACOS(STANGR)
      XCONT1(I) = XC
      YCONT1(I) = YC
      XCONT2(I) = XCONT2(I) - XREFER
      YCONT2(I) = YCONT2(I) - YREFER
      XC = XCONT2(I)*ACOS(STANGR) + YCONT2(I)*ASIN(STANGR)
      YC = -XCONT2(I)*ASIN(STANGR) + YCONT2(I)*ACOS(STANGR)
      XCONT2(I) = XC
      YCONT2(I) = YC
4050 CONTINUE
4100 CONTINUE
C-----
C  **  ENTER DATA FOR THE EXPLOSIVE WHICH IS USED  **
C-----
      WRITE(7,509)
509 FORMAT(' ENTER TYPE OF EXPLOSIVE TO BE USED :')
      READ(7,1509) EXPTYB
1509 FORMAT(A15)
      WRITE(7,507)
507 FORMAT(' WHAT IS THE WEIGHT STRENGTH OF THE EXPLOSIVE YOU ARE',
X' USING ?')
      READ (7,*) WSTR
C-----
      WRITE(7,508) LBS,INCH
508 FORMAT(' WHAT IS THE DENSITY OF THE EXPLOSIVE YOU ARE USING ?',/
X' ',A4,'/ CUBIC ',A4,'')

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IVREF = 0
IBEF = 0
INDEXV = 0
IF(KKODE1.EQ.'M') GO TO 500
WRITE (7,17)
17 FORMAT('      AUTOMATIC GENERATION OF THE INITIATION SEQUENCE',/
X      '-----')
C-----
C TAKE FIRST ROW AND FIND CHARGE IN THE CENTER OF THE ROW. THIS
C CHARGE WILL DETONATE FIRST.
C-----
      III = NCH(1)/2
      KP = NCH(1)
      DO 20 I=1,KP
      IPER(I) = 1 + ABS(III-I)
20 CONTINUE
C-----
C **      SUBSEQUENT ROWS      **
C-----
      DO 50 LR = 2, NR
      II = NCH(LR) / 2
      KPP = NCH(LR)
      DO 40 I = 1, KPP
      IPER( KP+ I) = IPER(III) + ABS(II-I) + 2
40 CONTINUE
      III = II + KP
      KP = KP + KPP
50 CONTINUE
C-----
C **      FIND MAXIMUM PERIOD      **
C-----
      IA = 0
      DO 60 I = 1, NUMBH
      IF(IPER(I).GE.100) GO TO 60
      IF(IA.GT.IPER(I)) GO TO 60
      IA = IPER(I)
60 CONTINUE
C-----
C **      CHECK VIBRATIONS FOR EACH DELAY PERIOD      **
C-----
65 DO 70 IV = 1,IA
      CALL VBRCHK(IV,INDEXV,KKODE1,ICODE1 )
      IF (INDEXV.EQ.1) GO TO 80
70 CONTINUE
      DO 71 IKOP=1,NUMBH
71 CONTINUE
      RETURN
C-----
C VIBRATIONS EXCEED MAXIMUM ACCEPTABLE. FIND LAST CHARGE WITH PERIOD
C EQUAL TO IV.
C-----
80 DO 90 I = 1, NUMBH
      IF ( IPER(I).LT.IV) GO TO 90
      ICOUNT = I
90 CONTINUE

```

A68

IF (IV.NE.IVBEF) IBEF = 100000	LLM16510
C	LLM16520
C ** PERIODS FROM CHARGE ICOUNT ON ARE INCREASED BY ONE **	LLM16530
C	LLM16540
DO 100 I = 1, NUMBH	LLM16550
IF ((IPER(I).GE.IV).AND.(1.GE.ICOUNT)) GO TO 120	LLM16560
GO TO 100	LLM16570
120 IF (1.GE.IBEF) GO TO 130	LLM16580
IPER(I) = IPER(I) + 1	LLM16590
100 CONTINUE	LLM16600
130 IVBEF = IV	LLM16610
IBEF = ICOUNT	LLM16620
GO TO 65	LLM16630
500 ICODE = 1	LLM16640
IFIRST = IFIRST + 1	LLM16650
505 WRITE(7,501) IFIRST	LLM16660
501 FORMAT(' HOW MANY CHARGES ARE DETONATED IN PERIOD # ',I2,' ?')	LLM16670
READ (7,*) NCDI	LLM16680
WRITE(7,510) IFIRST	LLM16690
510 FORMAT(' ENTER NUMBERS INDICATING CHARGES DETONATING IN PERIOD '	LLM16700
X' # ',I2,' :')	LLM16710
DO 520 I = 1,NCDI	LLM16720
READ(7,*) IDET	LLM16730
IPER(IDET) = IFIRST	LLM16740
520 CONTINUE	LLM16750
CALL VBRCHK(IFIRST,INDEXV,KKODE1,ICODE1)	LLM16760
IF(INDEXV.EQ.1) GO TO 505	LLM16770
RETURN	LLM16780
END	LLM16790
SUBROUTINE SEQOUT(K,ISQUT,ICODE)	LLM16800
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC	LLM16810
C	LLM16820
C PURPOSE :	LLM16830
C TO DETERMINE THE FINAL SEQUENCE OF AN UNDERGROUND	LLM16840
C BENCH BLAST.	LLM16850
C	LLM16860
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC	LLM16870
C	LLM16880
C VARIABLES : REFER TO MAIN PROGRAM	LLM16890
C	LLM16900
C	LLM16910
C	LLM16920
INTEGERS4 CLTIME,ICPU	LLM16930
CHARACTER*15 EXPTYP,EXPTYB	LLM16940
CHARACTER*80 TITLE	LLM16950
CHARACTER*8 QDATE ,QTIM	LLM16960
CHARACTER*1 KODE,IMR,BRTHR,KKODE1,KKODEI	LLM16970
COMMON /RDRDT1/ UCONCH,WTCRG,WSTRTH,SCDEPT(50),DELTA(50),	LLM16980
XSCRAD(50),DHOLE,X(50),Y(50),Z(50),XVCHK(10),YVCHK(10),ZVCHK(10)	LLM16990
X,PPVALL(10),AKFAC,AMFAC,XPIL1(10),XPIL2(10),XPIL3(10),YPIL1(10),	LLM17000
XPIL2(10),YPIL3(10),ZPIL1(10),ZPIL2(10),ZPIL3(10),PPVPAL,WSTR.	LLM17010
XXMAX,XMIN,YMAX,YMIN,ZMAX,ZMIN,DELTAR(50),RHOE,UCONCB,SCDEPB(50).	LLM17020
XDELTAB(50),SCRADB(50),DELTBR(50),WTCRBR,ALENGT,BMIN,SEPDIS	LLM17030
COMMON/RDRDT2/ NP1,NPB1,NP2,NPB2,NUMBH,NCHK,NUMPIL,INIT(50),NCONTRL	LLM17040
X .NITOTAL,MSYSUN	LLM17050


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COMMON/IBLK/ IBLCK(100,100),ITIME(100,100)
COMMON/BDY/ DX,DY
COMMON/DELT/DELTO,EFACR,DELTOB,EFACR
COMMON/XBLK/XB(100),YB(100)
COMMON/ISEQ/ IPER(50),KK,NR,NCH(50),NDECKS
COMMON/CHARGE/WEIGHT(50),WEIGR(50),DOPT(50),RCR(50),DEPTH(50),
XSCROP,DOPTB(50)
COMMON/TYPE/EXPTYP,EXPTYB
COMMON/TT/TITLE
COMMON/EREEF/ XEF(10),YEF(10)
COMMON/UPDATE/XXX(50,20),YYY(50,20),ZZZ(50,20),WUPD(50,20)
COMMON/ALPHA/IWR(100,100),BRTHR
COMMON/CONTR/ XCONT1(10),XCONT2(10),YCONT1(10),YCONT2(10)
COMMON/REFER/ XREFER,YREFER,ZREFER,STANGR,STLENG,STWIDT,
X STDEPT
DIMENSION ISOUT(50,20)
C-----
C  **      INITIALIZE VARIABLES      **
C-----
      INDEXV = 0
      IVREF = 100000
C-----
C  **      GET THE FIRST LEVEL OF CHARGES ( DECKS )      **
C-----
      DO 20 I = 1,NUMBH
      ISOUT(I,1) = IPER(I)
20 CONTINUE
      IF ( K.EQ.1 ) RETURN
C-----
C  **      GO TO SUBSEQUENT LEVELS      **
C-----
      DO 50 I = 1, NUMBH
      ISOUT(I,K) = ISOUT(I,K-1) + 2
50 CONTINUE
      DO 150 I = 1, NUMBH
      IF (ISOUT(I,K-1).GE.1000.0) GO TO 150
      IF (ISOUT(I,K-1).LT.ISOUT(I,K)) GO TO 150
      IDIFF = ISOUT(I,K-1)-ISOUT(I,K) + 1
      DO 100 IS = 1,NUMBH
      IF ( (ISOUT(IS,K).GE.ISOUT(I,K)).AND.(IS.GT.I) ) ISOUT(IS,K)=
      XISOUT(IS,K)+IDIFF
100 CONTINUE
150 CONTINUE
C-----
C  **      FIND MAXIMUM PERIOD (SO FAR)      **
C-----
165 IA = 0
      INDEXV = 0
      DO 160 I = 1, NUMBH
      IF (ISOUT(I,K).LE.IA) GO TO 160
      IF (ISOUT(I,K).GE.1000) GO TO 160
      IA = ISOUT(I,K)
160 CONTINUE
C-----
C  **      EXAMINE VIBRATIONS FOR EACH PERIOD      **

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C		LLM17610
	DO 170 IV = 1, IA	LLM17620
	CALL VIBRM(IV,INDEXV,K,ISOUT)	LLM17630
	IF (INDEXV.EQ.1) GO TO 180	LLM17640
	170 CONTINUE	LLM17650
	RETURN	LLM17660
C-----C	** VIBRATIONS EXCEED MAXIMUM ACCEPTABLE LEVEL **	LLM17670
C	FIND LAST CHARGE WITH PERIOD EQUAL TO IV	LLM17680
C-----C		LLM17690
	180 DO 190 I = 1, NUMBH	LLM17710
	IF (ISOUT(I,K).NE.IV) GO TO 190	LLM17720
	ICOUNT = I	LLM17730
	190 CONTINUE	LLM17740
	IF(IV.NE.IVBREF) IBEF = 100000	LLM17750
C-----C		LLM17760
C	** PERIODS FROM CHARGE ICOUNT ON ARE INCREASED BY ONE **	LLM17770
C-----C		LLM17780
	DO 200 I = 1, NUMBH	LLM17790
	IF ((ISOUT(I,K).GE.IV).AND.(I.GE.ICOUNT)) GO TO 220	LLM17800
	GO TO 200	LLM17810
	220 IF(I.GE.IBEF) GO TO 230	LLM17820
	ISOUT(I,K) = ISOUT(I,K) + 1	LLM17830
	200 CONTINUE	LLM17840
	230 IVBREF = IV	LLM17850
	IBEF = ICOUNT	LLM17860
	GO TO 165	LLM17870
	END	LLM17880
	SUBROUTINE SEPDST(IDELTA,BURDPF)	LLM17890
	CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC	LLM17900
C	PURPOSE :	LLM17910
C	TO CALCULATE THE SEPARATON DISTANCE BETWEEN CHARGES IN THE	LLM17920
C	BOREHOLE	LLM17930
C		LLM17940
C	CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC	LLM17950
C	VARIABLES :	LLM17960
C	REFER TO MAIN PROGRAM	LLM17970
C		LLM17980
	CHARACTERABO TITLE	LLM17990
	CHARACTERAL BRYTR,IWR	LLM18000
	COMMON /RDRDT1/ DCONCH,WTCNRG,WSTRTH,SCEPT(50),DELTA(50).	LLM18010
	XSCRAB(50),DHOLE,X(50),Y(50),Z(50),XVCHK(10),YVCHK(10),ZVCHK(10)	LLM18020
	X,PPVALL(10),AKFAC,AMEAC,XPIL1(10),XPIL2(10),XPIL3(10),YPIL1(10),	LLM18030
	XPIL2(10),YPIL3(10),ZPIL1(10),ZPIL2(10),ZPIL3(10),PPVPAL,WSTR,	LLM18040
	XXMAX,XMIN,YMAX,YMIN,ZMAX,ZMIN,DELTAR(50),RHOE,DCONCB,SCEPR(50),	LLM18050
	XDELTAR(50),SCRADB(50),DELTBR(50),WTCNRR,ALENGT,BMAIN,SEPDIS	LLM18060
	COMMON/RDRDT2/ NP1,NPB1,NP2,NPB2,NUMBH,NCHK,NUMPIL,INIT(50),NCONTPLLA	LLM18070
	X ,NTOTAL,MYSUN	LLM18080
	COMMON/IHLK/ ILOCK(100,100),ITIME(100,100)	LLM18090
	COMMON/OXDY/ DX,DY	LLM18100
	COMMON/DILT/ DELTO,EFACTR,DELTOB,EFACTB	LLM18110
	COMMON/XBLK/XB(100),YB(100)	LLM18120
	COMMON/ISEQ/ IPER(50),KK,NR,NCH(50),NDECKS	LLM18130
		LLM18140
		LLM18150

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COMMON/CHARGE/WEIGHT(50),WEIGH(50),DOPT(50),RCR(50),DEPTH(50),
XSCROP,DOPTB(50)
COMMON/TYPE/EXPTYP,EXPTYB
COMMON/ALPHA/1WR(100,100),BRTHR
COMMON/TT/TITLE
COMMON/FREEF/ XFF(10),YFF(10)
COMMON/CONTR/XCONT1(10),XCONT2(10),YCONT1(10),YCONT2(10)
COMMON/REFER/ XREFER,YREFER,ZREFER,STANGR,STLENG,STWIDT,
X STDEPT
DIMENSION WMINN(50),ZLEFT(50),CHARGB(50,15)
PI = 3.14159
ICWKPT = 0
TOP = 0
BOT = 0
ZMAX = 10000000.0
DO 5 I = 1,NUMBH
IF(ZMAX.LT.Z(1)) GO TO 5
ZMAX = Z(1)
5 CONTINUE
DO 6 I = 1, NUMBH
ZLEFT(I) = Z(I) - ZMAX
6 CONTINUE
WMINA = 10000000.0
WRITE(7,10)
10 FORMAT(' ENTER POWDER FACTOR FOR THE BLAST :')
READ(7,A) POWDFC
WRITE(7,20)
20 FORMAT(' ENTER BURDEN AND SPACING OF THE PATTERN :')
READ (7,A) BURDPE,SPACPE
VOLUME = BURDPE*SPACPE*(ZMAX-ZMIN)
C-----
C ** ENTER FACTOR FOR THE DETERMINATION OF MAXIMUM SEPARATION
C DISTANCE FOR ACCEPTABLE FRAGMENTATION **
C-----
WRITE(7,25)
25 FORMAT(' ENTER MAXIMUM DEPTH RATIO FOR ACCEPTABLE ',
X'FRAGMENTATION :',/' TYPICAL VALUES :',/' HARD ROCK : 0.75',
X/' SOFT ROCK : 0.85')
READ(7,A) AMXDRT
C-----
C ** WEIGHT OF EXPLOSIVE PER HOLE **
C-----
WEXPH = VOLUME * POWDFC
C-----
C ** TOTAL LENGTH OF EXPLOSIVE PER HOLE **
C-----
ALEXP = WEXPH/((RHOEADHOLE**2.0*PI/4.0)*12.0)
IF(MSYSUN.EQ.1)ALEXP=WEXPH/((RHOE/1000.0*ADHOLE**2.0*PI/4.0)*100.0)
C-----
C ** TOTAL LENGTH OF STENNING COLUMN PER HOLE **
C-----
ALSTEM = ZMAX - ZMIN - ALEXP
IDELTA = 1
IF(BRTHR.EQ.'N') IDELTA = 0
C-----

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C ** EXAMINE VIBRATIONS **

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C-----
NN = 0
ZH = (ZMAX+ZMIN)/2.0
NN = NCHK + NUNHIL
IF ( NN.EQ.0 ) GO TO 100
ELEV = ZH
CALL PLVIEW(ELEV,X,Y,NUMBH)
XM = 0.0
YM = 0.0
DO 50 IA=1,NUMBH
XM = XM + X(IA)
YM = YM + Y(IA)
50 CONTINUE
XM = XM/NUMBH
YM = YM/NUMBH
WHIN = 1000000.0
DO 30 I = 1,NCHK
CALL DISTPT(XVCHK(I),YVCHK(I),ZVCHK(I),XM,YM,ZH,DIST)
WEIGMX = (AKEAC/PPVALL(1))*2.0/AKEAC*ADISTAA2.0
IF(WEIGMX.LT.WHIN) WHIN = WEIGMX
30 CONTINUE
IF (WHINA.GT.WHIN) WHINA=WHIN
C-----
C ** FIND NUMBER OF DECKS **
C-----
100 NDECKS = IFIX(WEXPH/WHINA + 0.5)
IF(NDECKS.GT.0) GO TO 120
NDECKS = 1
ALENGT = ALEXP
ALST = ALSTEM
GO TO 200
120 ALENGT = ALEXP/NDECKS
C-----
C ** IDelta = 0 FOR NON BREAKTHROUGH HOLES **
C ** IDelta = 1 FOR BREAKTHROUGH HOLES **
C-----
ALST = ALSTEM/ILUAT(NDECKS + IDelta)
C-----
C ** OPTIMUM SEPARATION DISTANCE **
C-----
IF(MSYSUN.EQ.1) GO TO 291
200 SEPM1 = ((8.0ADHOLEAPIADHOLEAA2.0/4.0)ARHUE)AA(1.0/3.0)*
X EFACTRADELTO - 4.0ADHOLE/12.0
GO TO 292
291 SEPM1 = ((8.0ADHOLEAPIADHOLEAA2.0/4.0)ARHUEAO.001)AA(1.0/3.0)*
X EFACTRADELTO - 4.0ADHOLE/100.0
292 SEPM2 = 1000000.0
WXXX = 8.0ADHOLEAPIADHOLEAA2.0/4.0ARHUE
IF(MSYSUN.EQ.1) WXXX = WXXX/1000.0
IF(WHINA.GE.WXXX) GO TO 201
IF(MSYSUN.EQ.1) GO TO 295
SEPM2 = WHINAAA(1.0/3.0)AEFACTRADELTO-((WHINA/(KHUEAPIADHOLEAA2.0
X/4.0))/12.0)/2.0
GO TO 201

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295 SEPM2 = WMINAAA(1.0/3.0)ALFACTRADELTO-((WMINA/(RHOEAPIADHOLEAA2.0
X/(4.0A1000.0))))/100.0)/2.0 LLM19260
201 SEPMAX = MIN(SEPM1,SEPM2) LLM19270
IF(NN.EQ.0) SEPMAX = SEPM1 LLM19280
C----- LLM19290
C AA MINIMUM SEPARATION DISTANCE (GENERALLY ACCEPTED) AA LLM19300
C----- LLM19310
SEPMIN = 1.25ADHOLE LLM19320
IF(MSYSUN.EQ.1) SEPMIN = 1.25ADHOLE/(2.54A3.33) LLM19330
IF (ALST.LE.SEPMAX) GO TO 300 LLM19340
202 NDECKS = ALSTEM /SEPMAX - IDelta + 0.5 LLM19350
205 WXXX = WEXPH / NDECKS LLM19360
IF ( WXXX.GT.WMINA ) GO TO 203 LLM19370
IF(NDECKS.GT.0) GO TO 220 LLM19380
ALENGT = ALEXP LLM19390
ALST = ALSTEM LLM19400
NDECKS = 1 LLM19410
GO TO 300 LLM19420
220 ALENGT = ALEXP/FLUAT(NDECKS) LLM19430
ALST = ALSTEM/FLUAT(NDECKS + IDelta) LLM19440
300 SEPDIS = ALST LLM19450
IF(SEPDIS.GE.SEPMIN) GO TO 350 LLM19460
IF(SEPMAX.GT.SEPMIN) GO TO 301 LLM19470
NDECKS = NDECKS -1 LLM19480
GO TO 205 LLM19490
301 SEPMAX = SEPMIN LLM19500
ICHPKT = 1 LLM19510
GO TO 202 LLM19520
203 WRITE(7,308) LLM19530
308 FORMAT(' THE SEPARATION DISTANCE BETWEEN DECKS IS UNACCEPTABLY', LLM19540
X ' SMALL.',/, ' EXECUTION STOPS HERE.') LLM19550
STOP LLM19560
C----- LLM19570
C CHECK BOTTOM PARTS OF THE HOLES TO CONSIDER THE IRREGULARITIES LLM19580
C OF THE INITIAL FACE. LLM19590
C----- LLM19600
350 IF (ICHPKT.EQ.0) GO TO 351 LLM19610
CH1=(8.0ADHOLEAPIADHOLEAA2.0/4.0)ARHOE LLM19620
IF(MSYSUN.EQ.1) CH1 = CH1/1000.0 LLM19630
CH2=WMINA LLM19640
CH3=MIN(CH1,CH2) LLM19650
DC1=EFACTRACH3AA(1/3.0) LLM19660
PCR=SEPDIS/DC1 LLM19670
IF(PCR.LT.AMXDRT) GO TO 351 LLM19680
WRITE(7,307) LLM19690
WRITE(6,307) LLM19700
307 FORMAT(' THE SEPARATION DISTANCE BETWEEN DECKS IS LARGE.',/ LLM19710
X ' FRAGMENTATION WILL BE UNACCEPTABLE IN MANY CASES.') LLM19720
351 DO 600 I = 1,NUNRH LLM19730
IF(SEPMAX.GT.(ZLEFT(I)+ALST)) GO TO 600 LLM19740
IF((ALST+ALENGT).GT.ZLEFT(I)) GO TO 500 LLM19750
CHARGB(I,1)=WMINA LLM19760
ZLEFT(I) = ZLEFT(I)-ALENGT LLM19770
GO TO 600 LLM19780
500 CHARGB(I,1) = WMINAALENGT/(ALST+ALENGT) LLM19790
LLM19800

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600 CONTINUE                                     LLM19810
      RETURN                                       LLM19820
      END                                          LLM19830
      SUBROUTINE DISTLN(X1,Y1,X2,Y2,X3,Y3,DIST)   LLM19840
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC LLM19850
C                                                     C LLM19860
C    PURPOSE :                                    C LLM19870
C          TO CALCULATE DISTANCE OF ONE POINT TO A CERTAIN LINE C LLM19880
C                                                     C LLM19890
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC LLM19900
C                                                     LLM19910
C    VARIABLES :                                  LLM19920
C                                                     LLM19930
C        X1,X2,Y1,Y2 : X, Y COORDINATES OF THE LINE       LLM19940
C        X3,Y3         : Y, Y COORDINATES OF THE POINT     LLM19950
C                                                     LLM19960
C                                                     LLM19970
DO 20 I=1,10                                     LLM19980
XM = (X1+X2)/2.0                                LLM19990
YM = (Y1+Y2)/2.0                                LLM20000
DM = ((ABS(X3-XM))**2.0+(ABS(Y3-YM))**2.0)**0.5 LLM20010
D1 = ((ABS(X3-X1))**2.0+(ABS(Y3-Y1))**2.0)**0.5 LLM20020
D2 = ((ABS(X3-X2))**2.0+(ABS(Y3-Y2))**2.0)**0.5 LLM20030
IF(D1.GT.DM) GO TO 5                             LLM20040
X2 = XM                                           LLM20050
Y2 = YM                                           LLM20060
GO TO 20                                         LLM20070
5 X1 = XM                                        LLM20080
Y1 = YM                                        LLM20090
20 CONTINUE                                     LLM20100
DIST = ((ABS(X3-XM))**2.0+(ABS(Y3-YM))**2.0)**0.5 LLM20110
RETURN                                           LLM20120
END                                              LLM20130
SUBROUTINE TOPH (N,TOP)                          LLM20140
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC LLM20150
C                                                     C LLM20160
C    PURPOSE :                                    C LLM20170
C          TO ADJUST CHARGE WEIGHT SO THAT BACKBREAK AT THE TOP IS C LLM20180
C          AVOIDED.                               C LLM20190
C                                                     C LLM20200
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC LLM20210
C                                                     LLM20220
C    VARIABLES : REFER TO MAIN PROGRAM           LLM20230
C                                                     LLM20240
INTEGER*4 CLTIME,TCPU                           LLM20250
CHARACTER*1 KODE,IWR,BRTHR,KKODE1,KKODE1        LLM20260
COMMON /RDRT1/ DCONCH,WTRHRG,WSTRTH,SCDEPT(50),DELTA(50), LLM20270
XSCRAB(50),DHOLE,X(50),Y(50),Z(50),XVCHK(10),YVCHK(10),ZVCHK(10) LLM20280
X,PPVAL(10),AKEAC,AHFAC,XPIL1(10),XPIL2(10),XPIL3(10),YPIL1(10). LLM20290
XYPIL2(10),YPIL3(10),ZPIL1(10),ZPIL2(10),ZPIL3(10),PPVPAL,WSTR, LLM20300
XXMAX,XMIN,YMAX,YMIN,ZMAX,ZMIN,DELTAR(50),RHOE,DCONCR,SCDEPR(50). LLM20310
XDELTAR(50),SCRADB(50),DELTER(50),WTRHR,ALENGT,BMIN,SEPDIS LLM20320
COMMON/RDRT2/ NP1,NPB1,NP2,NPB2,NUMBH,NCHK,NUMPIL,INIT(50),NCONTRL LLM20330
X ,NTOTAL,MSYSUN                                 LLM20340
COMMON/DELT/ DELTO,EFACTR,DELTOB,EFACTRB        LLM20350

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COMMON/ISEQ/ IPER(50),KK,NR,NCH(50),NDECKS
COMMON/CHARGE/WEIGHT(50),WEIGB(50),DOPT(50),RCR(50),DEPTH(50),
XSCROP,DOPTH(50)
COMMON/CONTR/ XCONT1(10),XCONT2(10),YCONT1(10),YCONT2(10)
COMMON/REFER/ XREFER,YREFER,ZREFER,STANGR,STLENG,STWIOT,
X STDEPT
PI = 3.14159
WXX1 = (8.0ADHOLEAPIADHOLEAA2.0/4.0)AKHUE
IF(MSYSUN.EQ.1) WXX1 = WXX1/1000.0
TOP = SEPDIS
WXX2 = WEIGHT(N)
WXXX = MIN(WXX1,WXX2)
CHAR2 = (((WXXX/RHUE)/(DHOLEAA2.0API/4.0))/2.0)/12.0
IF(MSYNUN.EQ.1)
XCHAR2 = (((WXXX/(KHUE/1000.0))/(DHOLEAA2.0API/4.0))/2.0)/100.0
DELTOT=(SEPDIS+CHAR2)/(EFACTRA*WXXXAA(1.0/3.0))
DO 20 I = 2,NP2
IF(DELTA(I).GE.DELTOT) GO TO 21
20 CONTINUE
21 SCRTOP=SCRAD(I-1)+(DELTOT-DELTA(I-1))/(DELTA(I)-DELTA(I-1))X
X (SCRAD(I)-SCRAD(I-1))
DCONTH = 100000.0
IF(NCONTR.EQ.0) GO TO 200
DO 100 IP=1,NCONTR
X1 = XCONT1(IP)
X2 = XCONT2(IP)
Y1 = YCONT1(IP)
Y2 = YCONT2(IP)
DO 50 IJ = 1,10
X3 = (X1 + X2)/2.0
Y3 = (Y1 + Y2)/2.0
D1 = (ABS(X1-X(N))AA2.0+ABS(Y1-Y(N))AA2.0)AA0.5
UCONT = (ABS(X3-X(N))AA2.0+ABS(Y3-Y(N))AA2.0)AA0.5
D2 = (ABS(X2-X(N))AA2.0+ABS(Y2-Y(N))AA2.0)AA0.5
IF (D1.GT.D2) GO TO 49
X2 = X3
Y2 = Y3
GO TO 50
49 X1 = X3
Y1 = Y3
50 CONTINUE
IF(DCONTH.GT.UCONT) DCONTH = UCONT
100 CONTINUE
SCDCON = DCONTH/WXXXAA(1.0/3.0)
IF(SCDCON.GT.SCRTOP) GO TO 200
DO 80 IB = NP2,1
IF(SCRAD(IB).LE.SCDCON) GO TO 80
IF(IB.EQ.NP2) GO TO 75
DEL = (DELTA(IB+1)+DELTA(IB))/2.0
GO TO 81
75 DEL = (DELTA(IB)+1.0)/2.0
GO TO 81
80 CONTINUE
81 TOP = DELAEFACTRA*WXXXAA(1.0/3.0) -
X (((WXXX/RHUE)/(DHOLEAA2.0API/4.0))/2.0)/12.0

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LLM2036
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 LLM2089
 LLM2090

C	AA	CALCULATE DISTANCE FROM POINTS	AA	LLM21460
C		IF (NCHK.EQ.0) GO TO 131		LLM21470
		DO 130 I = 1, NCHK		LLM21480
		CALL DISTPT(XVCHK(I),YVCHK(I),ZVCHK(I),XM,YM,ZM,DISTM)		LLM21490
C				LLM21500
C	AA	CALCULATE PPV AT THIS POINT	AA	LLM21510
C		PPV(I) = AKEACA(DISTM/WMA*(1.0/2.0)) AA AMEAC		LLM21520
C				LLM21530
C	AA	FIND MAXIMUM WEIGHT FOR THIS PARTICULAR POINT	AA	LLM21540
C				LLM21550
		WEIGMX(I) = (AKEAC/PPVALL(I))AA(2.0/AMEAC)*DISTMAA2.0		LLM21560
		130 CONTINUE		LLM21570
C				LLM21580
C	AA	SAME FOR PILLARS	AA	LLM21590
C				LLM21600
		131 IF (NUMPIL.EQ.0) GO TO 151		LLM21610
		DO 150 I = 1, NUMPIL		LLM21620
		CALL DISTPL(XPIL1(I),YPIL1(I),ZPIL1(I),XPIL2(I),YPIL2(I),ZPIL2(I),		LLM21630
		X XPIL3(I),YPIL3(I),ZPIL3(I),XM,YM,ZM,DISTM)		LLM21640
		PPVPIL(I) = AKEACA((DISTM)/WMA*(1.0/2.0))AAAMEAC		LLM21650
		WEIGMX(NCHK+I) = (AKEAC/PPVPIL(I))AA(2.0/AMEAC)*DISTMAA2.0		LLM21660
		150 CONTINUE		LLM21670
C				LLM21680
C	AA	FIND MINIMUM OF ACCEPTABLE WEIGHTS	AA	LLM21690
C				LLM21700
		151 WMIN = WEIGMX(I)		LLM21710
		NN = NCHK + NUMPIL		LLM21720
		IF (NN.EQ.0) GO TO 200		LLM21730
		DO 180 I = 1, NN		LLM21740
		IF(WEIGMX(I).LT.WMIN) WMIN = WEIGMX(I)		LLM21750
		180 CONTINUE		LLM21760
		IF (WM.LE.(WMIN+1.0)) GO TO 200		LLM21770
		INDEXV = 1		LLM21780
		200 RETURN		LLM21790
		END		LLM21800
		SUBROUTINE BENGRC(X,Y,XMAX,XMIN,YMAX,YMIN,NUMBH,PLELEV)		LLM21810
				LLM21820
				LLM21830
				LLM21840
C				LLM21850
C		PURPOSE :		LLM21860
C		TO PROVIDE GRAPHICS OUTPUT		LLM21870
C		LANGUAGE : D13000		LLM21880
C				LLM21890
				LLM21900
C				LLM21910
C				LLM21920
		CHARACTER*4 XALPHA		LLM21930
		CHARACTER*2 XALP		LLM21940
		CHARACTER*32 STOPID		LLM21950
		COMMON/IRLK/ IBLOCK(100,100),ITIME(100,100)		LLM21960
		COMMON/XBLK/ XB(100),YB(100)		LLM21970
		COMMON/DXDY/ DX,DY		LLM21980
		COMMON/REFER/ XREFER,YREFER,ZREFER,STANCR,STLENG,STWIDT,		LLM21990
		X SIDEPT		LLM22000

DIMENSION X(50),Y(50),X0(20),Y0(20),XX(4),YY(4)	LLM22010
REWIND 51	LLM22020
CALL JBEGIN	LLM22030
CALL JDINIT(1)	LLM22040
CALL JDEVON(1)	LLM22050
CALL JDCOLR(7)	LLM22060
XM = XMIN - 10.0	LLM22070
XMM = XMAX + 10.0	LLM22080
YM = YMIN - 10.0	LLM22090
YMM = YMAX + 10.0	LLM22100
XSIZE = (XMAX-XMIN)/70.0	LLM22110
YSIZE = (YMAX-YMIN)/70.0	LLM22120
CALL JWINDOW(XM,XMM,YM,YMM)	LLM22130
CALL JOPEN	LLM22140
CALL JCOLOR(6)	LLM22150
CALL JPINTR(1)	LLM22160
CALL JPIDEX(6,10)	LLM22170
CALL JRECT(XM,YM,XMM,YMM)	LLM22180
CALL JCOLOR(3)	LLM22190
CALL JPINTR(1)	LLM22200
CALL JPIDEX(3,10)	LLM22210
CALL JRECT(XMIN,YMIN,XMAX,YMAX)	LLM22220
CALL JMOVE(XMIN,YMIN)	LLM22230
DO 110 J = 1,49	LLM22240
KGR = 1	LLM22250
DO 100 I = 1,49	LLM22260
IF(IBLOCK(I,J).EQ.0) GO TO 10	LLM22270
IF(IBLOCK(I,J).NE.0) GO TO 20	LLM22280
GO TO 100	LLM22290
10 CALL JCOLOR(3)	LLM22300
CALL JPINTR(1)	LLM22310
CALL JPIDEX(3,1)	LLM22320
GO TO 99	LLM22330
20 CALL JCOLOR(4)	LLM22340
CALL JPINTR(1)	LLM22350
CALL JPIDEX(4,12)	LLM22360
99 IF(IBLOCK(I,J).NE.IBLOCK(I+1,J)) GO TO 200	LLM22370
GO TO 150	LLM22380
200 IF(KGR.EQ.1) GO TO 340	LLM22390
IF(I.EQ.KGR) GO TO 433	LLM22400
XX(1) = XB(KGR)-DX/2.	LLM22410
YY(1) = YB(J)	LLM22420
IF(J.EQ.1) YY(1)=YMIN	LLM22430
XX(2) = XB(I)+DX/2.	LLM22440
YY(2) = YY(1)	LLM22450
IF(KGR.LE.2) GO TO 221	LLM22460
IF(IBLOCK(KGR-2,J+1).EQ.IBLOCK(KGR,J)) GO TO 220	LLM22470
221 IF(IBLOCK(KGR-1,J+1).EQ.IBLOCK(KGR,J)) GO TO 240	LLM22480
IF(IBLOCK(KGR,J+1).EQ.IBLOCK(KGR,J)) GO TO 250	LLM22490
IF(IBLOCK(KGR+1,J+1).EQ.IBLOCK(KGR,J)) GO TO 260	LLM22500
IF(KGR.GE.48) GO TO 222	LLM22510
IF(IBLOCK(KGR+2,J+1).EQ.IBLOCK(KGR,J)) GO TO 270	LLM22520
222 XX(4) = XB(KGR+1)-DX/2.0	LLM22530
YY(4) = YB(J+1)	LLM22540
GO TO 300	LLM22550

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220 XX(4) = XB(KGR-2)-DX/2.0
    YY(4) = YB(J+1)
    GO TO 300
240 XX(4) = XB(KGR-1)-DX/2.0
    YY(4) = YB(J+1)
    GO TO 300
250 XX(4) = XB(KGR)-DX/2.0
    YY(4) = YB(J+1)
    GO TO 300
260 XX(4) = XB(KGR+1) -DX/2.
    YY(4) = YB(J+1)
    GO TO 300
270 XX(4) = XB(KGR+2) -DX/2.
    YY(4) = YB(J+1)
    GO TO 300
340 XX(1)=XMIN
    YY(1) = YB(J)
    IF(J.EQ.1) YY(1) = YMIN
    XX(2) = XB(1)+DX/2.0
    YY(2) = YY(1)
    XX(4) = XMIN
    YY(4) = YB(J+1)
300 IF(I.EQ.49) GO TO 350
    IF(I.GE.49) GO TO 3001
    IF(1BLOCK(I+2,J+1).EQ.1BLOCK(I,J)) GO TO 385
3001 IF(1BLOCK(I+1,J+1).EQ.1BLOCK(I,J)) GO TO 380
    IF(1BLOCK(I,J+1).EQ.1BLOCK(I,J)) GO TO 350
    IF(1BLOCK(I-1,J+1).EQ.1BLOCK(I,J)) GO TO 360
    IF(I.LE.2) GO TO 3002
    IF(1BLOCK(I-2,J+1).EQ.1BLOCK(I,J)) GO TO 365
3002 XX(3) = XB(I-1)+ DX/2.
    YY(3) = YB(J+1)
    GO TO 400
385 XX(3) = XB(I+2)+DX/2.0
    YY(3) = YB(J+1)
    GO TO 400
380 XX(3) = XB(I+1)+DX/2.0
    YY(3) = YB(J+1)
    GO TO 400
350 XX(3) = XB(I) + DX/2.0
    YY(3) = YB(J+1)
    GO TO 400
360 XX(3) = XB(I-1)+DX/2.0
    YY(3) = YB(J+1)
    GO TO 400
365 XX(3) = XB(I-2)+DX/2.0
    YY(3) = YB(J+1)
400 IF(1BLOCK(I,J).EQ.0) GO TO 411
    CALL JPOLGN(XX,YY,4)
411 KGR = I + 1
433 IF(I.EQ.49) GO TO 100
150 IF(I.LT.49) GO TO 100
    GO TO 200
100 CONTINUE
110 CONTINUE
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LLM22560
LLM22570
LLM22580
LLM22590
LLM22600
LLM22610
LLM22620
LLM22630
LLM22640
LLM22650
LLM22660
LLM22670
LLM22680
LLM22690
LLM22700
LLM22710
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LLM23000
LLM23010
LLM23020
LLM23030
LLM23040
LLM23050
LLM23060
LLM23070
LLM23080
LLM23090
LLM23100

CALL JCOLOR(8)	LLM23110
IPREV = 0	LLM23120
CALL JLWIDE(32000)	LLM23130
REWIND 72	LLM23140
READ (72,800) NPERP	LLM23150
800 FORMAT(I5)	LLM23160
READ (72,810) ((X0(I),Y0(I)),I = 1,NPERP)	LLM23170
810 FORMAT(2F10.2)	LLM23180
DO 700 I = 1,NPERP	LLM23190
KK1 = 0	LLM23200
IF((X0(I).GT.XMAX).OR.(X0(I).LT.XMIN).OR.(Y0(I).GT.YMAX).OR.	LLM23210
X(Y0(I).LT.YMIN)) GO TO 701	LLM23220
IF(I.NE.1) GO TO 699	LLM23230
CALL JMOVE(X0(I),Y0(I))	LLM23240
GO TO 700	LLM23250
699 IF(IPREV.EQ.(I-1)) GO TO 710	LLM23260
CALL JDRAW(X0(I),Y0(I))	LLM23270
GO TO 700	LLM23280
701 IF(IPREV.NE.(I-1)) GO TO 710	LLM23290
IPREV = I	LLM23300
GO TO 700	LLM23310
710 X3 = (X0(I-1)+X0(I))/2.0	LLM23320
Y3 = (Y0(I-1)+Y0(I))/2.0	LLM23330
712 KK1 = KK1 + 1	LLM23340
IF(IPREV.EQ.(I-1)) GO TO 950	LLM23350
IF((X3.GT.XMAX).OR.(X3.LT.XMIN).OR.(Y3.GT.YMAX).OR.(Y3.LT.YMIN))	LLM23360
X GO TO 720	LLM23370
X3 = (X3+X0(I))/2.0	LLM23380
Y3 = (Y3+Y0(I))/2.0	LLM23390
IF(KK1.LT.4) GO TO 712	LLM23400
GO TO 740	LLM23410
720 X3 = (X0(I-1)+X3)/2.0	LLM23420
Y3 = (Y0(I-1)+Y3)/2.0	LLM23430
IF(KK1.LT.4) GO TO 712	LLM23440
740 IF(IPREV.NE.(I-1)) GO TO 760	LLM23450
912 KK1 = KK1 + 1	LLM23460
950 IF((X3.GT.XMAX).OR.(X3.LT.XMIN).OR.(Y3.GT.YMAX).OR.(Y3.LT.YMIN))	LLM23470
X GO TO 920	LLM23480
X3 = (X3+X0(I-1))/2.0	LLM23490
Y3 = (Y3+Y0(I-1))/2.0	LLM23500
IF(KK1.LT.4) GO TO 912	LLM23510
GO TO 940	LLM23520
920 X3 = (X0(I)+X3)/2.0	LLM23530
Y3 = (Y0(I)+Y3)/2.0	LLM23540
IF(KK1.LT.4) GO TO 912	LLM23550
940 CALL JMOVE(X3,Y3)	LLM23560
CALL JDRAW(X0(I),Y0(I))	LLM23570
GO TO 700	LLM23580
760 IPREV = I	LLM23590
CALL JDRAW(X3,Y3)	LLM23600
700 CONTINUE	LLM23610
CALL JCOLOR(1)	LLM23620
CALL JMOVE(XMIN,YMIN)	LLM23630
CALL JDRAW(XMAX,YMIN)	LLM23640
CALL JMOVE(XMIN,YMIN)	LLM23650

CALL JDRAW(XMIN,YMAX)	LLM23660
DO 4000 I = 1,10	LLM23670
XL = XMIN + DX * FLOAT(I-1) * 10.0	LLM23680
IF(XL.GT.XMAX) GO TO 401	LLM23690
CALL JMOVE(XL,YMIN)	LLM23700
CALL JDRAW(XL,YMIN-0.5)	LLM23710
CALL JMOVE(XL,YMIN-1.0)	LLM23720
IF(XL.GE.0) GO TO 112	LLM23730
NL = IFIX(XL - 0.5)	LLM23740
GO TO 113	LLM23750
112 NL = IFIX(XL + 0.5)	LLM23760
113 WRITE(61,307) NL	LLM23770
BACKSPACE 61	LLM23780
READ(61,301) XALPHA	LLM23790
301 FORMAT(A4)	LLM23800
CALL JJUST(2.3)	LLM23810
CALL JSIZE(XSIZE,YSIZE)	LLM23820
CALL J3STRG(XALPHA)	LLM23830
4000 CONTINUE	LLM23840
401 CONTINUE	LLM23850
DO 500 I = 1,10	LLM23860
YL = YMIN + DY*FLOAT(I-1)*10.0	LLM23870
IF (YL.GT.YMAX) GO TO 501	LLM23880
CALL JMOVE(XMIN,YL)	LLM23890
CALL JDRAW(XMIN-0.5,YL)	LLM23900
CALL JMOVE(XMIN-1.0,YL)	LLM23910
IF(YL.GE.0.0) GO TO 412	LLM23920
NL = IFIX(YL - 0.5)	LLM23930
GO TO 413	LLM23940
412 NL = IFIX(YL + 0.5)	LLM23950
413 WRITE(61,307) NL	LLM23960
307 FORMAT(14)	LLM23970
BACKSPACE 61	LLM23980
READ(61,301) XALPHA	LLM23990
CALL JJUST(3.2)	LLM24000
CALL JSIZE(XSIZE,YSIZE)	LLM24010
CALL J3STRG(XALPHA)	LLM24020
500 CONTINUE	LLM24030
501 CALL JCMARK(3)	LLM24040
DO 600 I = 1,NUMER	LLM24050
WRITE(61,510) I	LLM24060
510 FORMAT(12)	LLM24070
BACKSPACE 61	LLM24080
READ(61,520) XALP	LLM24090
520 FORMAT(1A2)	LLM24100
CALL JMARK(X(I),Y(I))	LLM24110
CALL JMOVE(X(I)+0.6,Y(I))	LLM24120
CALL JJUST(1,2)	LLM24130
CALL JSIZE(XSIZE,YSIZE)	LLM24140
CALL J3STRG(XALP)	LLM24150
600 CONTINUE	LLM24160
XSIZE = 2.0*XSIZE	LLM24170
YSIZE = 2.0*YSIZE	LLM24180
REWIND 51	LLM24190
READ(51,610) STOPID	LLM24200

[illegible]

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X ,NTOTAL,MSYSUN
COMMON/CHARGE/WEIGHT(50),WEIGH(50),DOPT(50),RCR(50),DEPTH(50),
XSCROP,DOPTH(50)
COMMON/DELT/DELTO,EFACR,DELTOB,EFACB
COMMON/ISEQ/ IPER(50),KK,NR,NCH(50),NDECKS
COMMON/REFER/ XREFER,YREFER,ZREFER,STANGR,STLENG,STWIDT,
X STDEPT
DIMENSION ALOAD(50),PPV(10),PPVPIL(10),WEIGMX(50),ID(50),TOP(50)
C-----
C ** INITIALIZE VARIABLES **
C-----
DO 2 I = 1,50
ID(I) = 0
2 CONTINUE
WEIGMX(1) = 100000.0
INDEXV = 0
C-----
C ** FIND CHARGES DETONATING IN THE SAME PERIOD **
C-----
KK = 0
DO 100 IA = 1, NUMBH
IF (IPER(IA).NE.IFIRST) GO TO 100
C-----
C ** LOAD HOLE **
C-----
PI = 3.14159
IF (NTOTAL.NE.NDECKS) GO TO 20
CALL TOPH(IA,TOP(IA))
ALOAD(IA) = (12.0*(SEPDIS+ALLNGT-TOP(IA))*APIADHOLE**2.0/4.0)*ARHDE
IF (MSYSUN.EQ.1) ALOAD(IA) = ALOAD(IA)/12.0*0.1
C-----
C ** CHECK VIBRATION LEVELS **
C-----
20 IF (NCHK.EQ.0) GO TO 32
C-----
C ** CALCULATE DISTANCES FROM POINTS
C-----
DO 30 I = 1, NCHK
CALL DISTPT(XVCHK(I),YVCHK(I),ZVCHK(I),X(IA),Y(IA),Z(IA),DIST)
C-----
C ** CALCULATE PPV AT THIS POINT **
C-----
PPV(I) = AKFAC*(DIST/WEIGHT(IA)**(1.0/2.0))*AMFAC
C-----
C ** FIND MAXIMUM WEIGHT FOR THIS PARTICULAR POINT **
C-----
WEIGMX(I) = (AKFAC/PPVALL(I))*((2.0/AMFAC)*DIST**2.0
30 CONTINUE
C-----
C ** CALCULATE DISTANCE FROM PILLARS **
C-----
32 IF (NUMPIL.EQ.0) GO TO 52
DO 50 I = 1, NUMPIL
CALL DISTPL(XPIL1(I),YPIL1(I),ZPIL1(I),XPIL2(I),YPIL2(I),ZPIL2(I),LLM25360

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      XXPIL3(I),YPIL3(I),ZPIL3(I),X(IA),Y(IA),Z(IA),DISTP)      LLM25310
C-----LLM25320
C  ** CALCULATE PPV AT THIS POINT **                             LLM25330
C-----LLM25340
      PPVPIL(I) = ARCAC * (DISTP/WEIGHT(IA))**((1.0/2.0)**AA)    LLM25350
      X AMFAC                                                    LLM25360
C-----LLM25370
C  ** FIND MAXIMUM WEIGHT BECAUSE OF THIS PARTICULAR PILLAR **  LLM25380
C-----LLM25390
      WEIGHX(NCHK+1) = (ARFAC/PPVPAL)**((2.0/AMFAC)*DISTP**2.0)  LLM25400
      50 CONTINUE                                              LLM25410
C-----LLM25420
C  ** FIND MINIMUM ACCEPTABLE WEIGHTS **                         LLM25430
C-----LLM25440
      52 WMIN = WEIGHX(1)                                       LLM25450
      NN = NCHK + NUPIL                                         LLM25460
      IF (NN.EQ.0) GO TO 99                                     LLM25470
      DO 80 I = 1, NN                                           LLM25480
      IF (WEIGHX(I).LT.WMIN) WMIN=WEIGHX(I)                     LLM25490
      80 CONTINUE                                              LLM25500
      IF (WEIGHT(IA).LE.WMIN) GO TO 99                          LLM25510
      WEIGHT(IA) = WMIN                                         LLM25520
      99 KK = KK + 1                                           LLM25530
      INIT(KK) = IA                                             LLM25540
      100 CONTINUE                                              LLM25550
      IF (NN.EQ.0) GO TO 200                                    LLM25560
C-----LLM25570
C      CHECK VIBRATIONS DUE TO THE SIMULTANEOUS DETONATION OF   LLM25580
C      MANY CHARGES                                           LLM25590
C-----LLM25600
C-----LLM25610
C-----LLM25620
C  ** FIND AN AVERAGE POSITION OF THE CONCENTRATED CHARGE **    LLM25630
C-----LLM25640
      XM = 0.0                                                  LLM25650
      IF (KK.EQ.1) GO TO 200                                    LLM25660
      YM = 0.0                                                  LLM25670
      ZM = 0.0                                                  LLM25680
      WM = 0.0                                                  LLM25690
      DO 110 I = 1, KK                                          LLM25700
      IM = INIT(I)                                              LLM25710
      XM = XM + X(I)*WEIGHT(IM)                                LLM25720
      YM = YM + Y(I)*WEIGHT(IM)                                LLM25730
      ZM = ZM + Z(I)*WEIGHT(IM)                                LLM25740
      WM = WM + WEIGHT(IM)                                       LLM25750
      110 CONTINUE                                              LLM25760
      XM = XM / WM                                              LLM25770
      YM = YM / WM                                              LLM25780
      ZM = ZM / WM                                              LLM25790
C-----LLM25800
C  ** CALCULATE DISTANCE FROM POINTS **                         LLM25810
C-----LLM25820
      IF (NCHK.EQ.0) GO TO 131                                  LLM25830
      DO 130 I = 1, NCHK                                         LLM25840
      CALL DISTPT(XVCHK(I),YVCHK(I),ZVCHK(I),XM,YM,ZM,DISTH)    LLM25850

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C----- LLM25860
C  AA  CALCULATE PPV AT THIS POINT  AA  LLM25870
C----- LLM25880
      PPV(I) = AKEACA(DISTN/WMA(1.0/2.0)) AA AKEAC LLM25890
C----- LLM25900
C  AA  FIND MAXIMUM WEIGHT FOR THIS PARTICULAR POINT  AA  LLM25910
C----- LLM25920
      WEIGMX(I) = (AKEAC/PPVALL(I))AA(2.0/AKEAC)*DISTNAA2.0 LLM25930
130 CONTINUE LLM25940
C----- LLM25950
C  AA  SAME FOR PILLARS LLM25960
C----- LLM25970
131 IF (NUMPIL.EQ.0) GO TO 151 LLM25980
      DO 150 I = 1, NUMPIL LLM25990
          CALL DISTPL(XPIL1(I),YPIL1(I),ZPIL1(I),XPIL2(I),YPIL2(I),ZPIL2(I),
          X XPIL3(I),YPIL3(I),ZPIL3(I),XM,YM,ZH,DISTN) LLM26000
          PPVIL(I) = AKEACA((DISTN/WMAA(1.0/2.0))AAAKEAC LLM26010
          WEIGMX(NCHK+I) = (AKEAC/PPVIL(I))AA(2.0/AKEAC)*DISTNAA2.0 LLM26020
150 CONTINUE LLM26030
C----- LLM26040
C  AA  FIND MINIMUM OF ACCEPTABLE WEIGHTS  AA  LLM26050
C----- LLM26060
151 WHIN = 2000000.0 LLM26070
      NN = NCHK + NUMPIL LLM26080
      IF (NN.EQ.0) GO TO 200 LLM26090
      DO 180 I = 1, NN LLM26100
          IF (WEIGMX(I).LT.WHIN) WHIN = WEIGMX(I) LLM26110
180 CONTINUE LLM26120
          IF (WH.LE.WHIN) GO TO 200 LLM26130
          IF (KRODEI.NE.'N') GO TO 192 LLM26140
          IF (IC0001.EQ.1) GO TO 199 LLM26150
          WRITE(7,187) LLM26160
187 FORMAT(' THE NUMBER OF CHARGES DETONATING IN THIS PERIOD IS',/ LLM26170
          X' TOO LARGE RESULTING IN UNACCEPTABLE VIBRATIONS.',/ LLM26180
          X' DO YOU WANT TO CHANGE THE SEQUENCING OF THE CHARGES ? (Y/N)') LLM26190
          READ (7,188) SEQ LLM26200
188 FORMAT(1A1) LLM26210
          INDEXV = 1 LLM26220
          IF(SEQ.EQ.'Y') GO TO 191 LLM26230
          INDEXV = 0 LLM26240
          GO TO 200 LLM26250
192 INDEXV = 1 LLM26260
191 DO 190 I = 1, NUMBH LLM26270
          IF(IPER(I).NE.IFIRST) GO TO 190 LLM26280
          WEIGHT(I) = 0.0 LLM26290
          WEIGB(I) = 0.0 LLM26300
          IPER(I) = 100000 LLM26310
190 CONTINUE LLM26320
          GO TO 200 LLM26330
199 INDEXV = 1 LLM26340
          DO 2190 I = 1, NUMBH LLM26350
          IF(IPER(I).NE.IFIRST) GO TO 2190 LLM26360
          WEIGHT(I) = 0.0 LLM26370
          WEIGB(I) = 0.0 LLM26380
2190 CONTINUE LLM26390
      LLM26400

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200 RETURN	LLM26410
END	LLM26420
SUBROUTINE CHARGE(DOUPD)	LLM26430
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC	LLM26440
C	LLM26450
C PURPOSE :	LLM26460
C TO PREPARE THE DATA FILE FOR THE GRAPHICS PROGRAM	LLM26470
C	LLM26480
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC	LLM26490
C	LLM26500
C VARIABLES : REFER TO MAIN PROGRAM	LLM26510
C	LLM26520
C	LLM26530
CHARACTER*80 TITLE	LLM26540
COMMON/REFER/ XREFER,YREFER,ZREFER,STANGR,STLENG,STWIDT.	LLM26550
X STDEPT	LLM26560
DIMENSION ZKNOWN(50,20),ALENGT(50,20),WEIGHT(50,20),IPER(50,20),	LLM26570
X XDI(50),YDI(50),ZDI(50),STOPID(40),DOUPD(50,20)	LLM26580
PP = 3.1415926	LLM26590
REWIND 70	LLM26600
READ(70,910) NUMBH,NCHRGs	LLM26610
910 FORMAT(15I5)	LLM26620
READ(70,900) DIANT	LLM26630
DO 1000 I = 1,NCHRGs	LLM26640
READ(70,900) (ZKNOWN(J,I),J=1,NUMBH)	LLM26650
900 FORMAT(8F10.2)	LLM26660
1000 CONTINUE	LLM26670
DO 1050 I = 1,NCHRGs	LLM26680
READ(70,900) (WEIGHT(J,I),J=1,NUMBH)	LLM26690
1050 CONTINUE	LLM26700
DO 1100 I = 1,NCHRGs	LLM26710
READ(70,900) (ALENGT(J,I),J=1,NUMBH)	LLM26720
1100 CONTINUE	LLM26730
IEXP = 1	LLM26740
DO 1200 I = 1,NCHRGs	LLM26750
READ(70,910) (IPER(J,I),J=1,NUMBH)	LLM26760
1200 CONTINUE	LLM26770
REWIND 66	LLM26780
DO 3000 IHUSEN = 1,NUMBH	LLM26790
READ(66,100) IJUNK,N1,IHOKOW,IHOCOL,DDDDD,DIPNOM	LLM26800
100 FORMAT(4I5,2F10.2)	LLM26810
IF(IJUNK.EQ.99) GO TO 3000	LLM26820
WRITE(62,21) NCHRGs,IHOKOW,IHOCOL	LLM26830
21 FORMAT(15I5)	LLM26840
READ(66,101) XCOLAK,YCOLAK,ZCOLAK	LLM26850
101 FORMAT(3F10.2)	LLM26860
READ(66,101,END=3000) ((XDI(I),YDI(I),ZDI(I)),I=1,N1)	LLM26870
DO 155 ICH = 1,NCHRGs	LLM26880
X1 = XCOLAK	LLM26890
Y1 = YCOLAK	LLM26900
Z1 = ZCOLAK-ZREFER	LLM26910
D1 = 0	LLM26920
DO 150 I = 1,N1	LLM26930
Z2 = ZDI(I)-ZREFER	LLM26940
X2 = XDI(I)	LLM26950

Y2 = YDI(1)	LLM26960
IF(Z2.LT.ZKNOWN(IHSEQ,ICH)) GO TO 109	LLM26970
ZLOCAL = ZKNOWN(IHSEQ,ICH)	LLM26980
RATIO = (ZKNOWN(IHSEQ,ICH)-Z1)/(Z2-Z1)	LLM26990
DX1X2 = RATIOA(X1-X2)	LLM27000
DY1Y2 = RATIOA(Y1-Y2)	LLM27010
D1=D1+(ABS(DX1X2)AA2.0+ABS(DY1Y2)AA2.0+ABS(Z1-ZKNOWN(IHSEQ,ICH))	LLM27020
AA2.0)AA0.5	LLM27030
GO TO 200	LLM27040
109 ZLOCAL = Z2	LLM27050
D1=D1 + (ABS(X1-Z2)AA2.0+ABS(Y1-Y2)AA2.0+ABS(Z1-Z2)AA2.0)AA0.5	LLM27060
X1 = X2	LLM27070
Y1 = Y2	LLM27080
Z1 = Z2	LLM27090
150 CONTINUE	LLM27100
200 DUP = D1 - ALNGT(IHSEQ,ICH)/2.0	LLM27110
DDO = D1 + ALNGT(IHSEQ,ICH)/2.0	LLM27120
DDOUPD(IHSEQ,ICH) = DDO	LLM27130
ZDO = ZCOLAR-ZREFER-(ZKNOWN(IHSEQ,ICH)-ALNGT(IHSEQ,ICH)/2.0)	LLM27140
ZUP = ZCOLAR-ZREFER-(ZKNOWN(IHSEQ,ICH)-ALNGT(IHSEQ,ICH)/2.0)	LLM27150
WRITE(62,260) ZDO,ZUP,DDO,DUP,WEIGHT(IHSEQ,ICH),DIANT,TEXPLT,IPER	LLM27160
X(IHSEQ,ICH)	LLM27170
260 FORMAT(6F10.2,2I5)	LLM27180
155 CONTINUE	LLM27190
3000 CONTINUE	LLM27200
3008 CONTINUE	LLM27210
LAST = 99	LLM27220
WRITE(62,21) LAST,INOROW,INUCOL	LLM27230
RETURN	LLM27240
END	LLM27250
SUBROUTINE PVIEW(PLELEV,XHOL,YHOL,NOHOLS)	LLM27260
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC	LLM27270
C	LLM27280
C PURPOSE :	LLM27290
C TO GIVE THE LOCAL COORDINATES OF THE HOLES AT	LLM27300
C A SPECIFIED ELEVATION	LLM27310
C	LLM27320
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC	LLM27330
C	LLM27340
C VARIABLES :	LLM27350
C PLELEV : PLAN ELEVATION	LLM27360
C XREFER , YREFER , ZREFER . REFERENCE POINT FOR TRANSLATION	LLM27370
C	LLM27380
C	LLM27390
C	LLM27400
C	LLM27410
C	LLM27420
C	LLM27430
C COMMON/REFER/ XREFER,YREFER,ZREFER,STANGR,STLENG,STWIDT,	LLM27440
X STDEPT	LLM27450
DIMENSION D(50),DIP(50),AZIM(50)	LLM27460
DIMENSION X(50),Y(50),Z(50)	LLM27470
DIMENSION STOPID(50)	LLM27480
DIMENSION XHOL(50),YHOL(50)	LLM27490
DIMENSION HOL(50,3),XP(50),YP(50),DIAM(50)	LLM27500

PP=3.1415926	LLM27510
REWIND 66	LLM27520
PLELEV=PLELEV-ZREFER	LLM27530
IF (PLELEV.LT.0.0) RETURN	LLM27540
6 FORMAT(11,/,',.11)	LLM27550
19 FORMAT(20A4)	LLM27560
20 FORMAT(4F10.2)	LLM27570
C-----	LLM27580
C READ HOLE DATA	LLM27590
C 99 DENOTES END OF HOLE DATA FILE	LLM27600
C-----	LLM27610
C	LLM27620
7 READ (66,100) IHOSQ,N1,IHOROW,IHOCOL,DIA,DIPNOH	LLM27630
IF (IHOSQ.EQ.99) GO TO 8	LLM27640
C-----	LLM27650
C INCREASE HOLE DIAMETER BY .200 FOR PLOT CLARITY	LLM27660
C	LLM27670
READ (66,101) XCOLAR,YCOLAR,ZCOLAR	LLM27680
C-----	LLM27690
C STATION INTERVAL 10 FT	LLM27700
C FOLLOWING DATA REFERS TO HOLE AXIS	LLM27710
C-----	LLM27720
READ (66,101,END=8) ((X(I),Y(I),Z(I)),I=1,N1)	LLM27730
CALL PTRANS(X,Y,Z,N1,XREFER,YREFER,ZREFER)	LLM27740
C-----	LLM27750
C ROTATE COORDINATES (STANGR)	LLM27760
C-----	LLM27770
DO 200 I = 1,N1	LLM27780
XC = X(I) * COS(STANGR) + Y(I) * SIN (STANGR)	LLM27790
YC = - X(I) * SIN(STANGR) + Y(I) * COS (STANGR)	LLM27800
X(I) = XC	LLM27810
Y(I) = YC	LLM27820
HOL(I,1) = X(I)	LLM27830
HOL(I,2) = Y(I)	LLM27840
HOL(I,3) = Z(I)	LLM27850
200 CONTINUE	LLM27860
C-----	LLM27870
C ** ROTATE COORDINATES **	LLM27880
C-----	LLM27890
DO 10 I=2,N1	LLM27900
IF (HOL(I,3).LT.PLELEV) GO TO 10	LLM27910
XP(1)=HOL(I,1)+(PLELEV-HOL(I,3))/(HOL(I-1,3)-HOL(I,3))*HOL(I-1,	LLM27920
A1)-HOL(I,1))	LLM27930
YP(1)=HOL(I,2)+(PLELEV-HOL(I,3))/(HOL(I-1,3)-HOL(I,3))*HOL(I-1,	LLM27940
A2)-HOL(I,2))	LLM27950
GO TO 11	LLM27960
10 CONTINUE	LLM27970
11 CONTINUE	LLM27980
XP(2)=HOL(I,1)	LLM27990
YP(2)=HOL(I,2)	LLM28000
XHOL(IHOSQ) = XP(1)	LLM28010
YHOL(IHOSQ) = YP(1)	LLM28020
GO TO 7	LLM28030
B CONTINUE	LLM28040
100 FORMAT(4I5,2F10.2)	LLM28050

A89

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101  FORMAT(3F10.2)                                LLM28060
      REWIND 51                                       LLM28070
      REWIND 66                                       LLM28080
      RETURN                                          LLM28090
      END                                             LLM28100
      SUBROUTINE PTRANS(X,Y,Z,NPNTS,XREF,YREF,ZREF)  LLM28110
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC LLM28120
C                                                     C LLM28130
C   PURPOSE :                                         C LLM28140
C       TO PERFORM A TRANSLATION WRT THE POINT XREF,YREF,ZREF C LLM28150
C                                                     C LLM28160
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC LLM28170
      DIMENSION X(50),Y(50),Z(50)                   LLM28180
      DO 10 I=1,NPNTS                                LLM28190
      X(I)=X(I)-XREF                                  LLM28200
      Y(I)=Y(I)-YREF                                  LLM28210
      Z(I)=Z(I)-ZREF                                  LLM28220
10  CONTINUE                                         LLM28230
      RETURN                                          LLM28240
      END                                             LLM28250

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3. GRAPHICS OUTPUT GENERATOR PROGRAM FOR BOTH
DESIGN PROGRAMS

PROGRAM PGRAPH

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C-----PGR00010
C  MENU DRIVER  FOR PLOTTING..PGR00020
C  AXONOMETRIC PROJECTION OF A STOPE, PLANS AND CROSS SECTIONS WITHPGR00030
C  THE HOLE LOCATIONS AND SINGLE HOLE PROJECTIONSPGR00040
C-----PGR00050
C  WRITE (6,100)PGR00060
100 FORMAT (2X,'LARGE DIAMETER BLASTHOLE MINING'//PGR00070
      A10X,'G R A P H I C S'//)PGR00080
      WRITE(6,1133)PGR00090
1133 FORMAT(2X,'ENTER 1 FOR GRAPHICS OUTPUT FOR A VCR STOPE',/PGR00100
      X2X,' OR 2 FOR GRAPHICS OUTPUT FOR AN UNDERGROUND BENCH.')

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A92

READ(5,A,END=40) IROW,ICOLUN	PGR00560
CALL PHOPRO(IROW,ICOLUN)	PGR00570
GO TO 111	PGR00580
50 CONTINUE	PGR00590
STOP	PGR00600
END	PGR00610
C	PGR00620
C CALCULATES THE ADJUSTED HOLE BOUNDARIES. FOR- RA	PGR00630
C IT ALSO CALCULATES THE AZIMUTH OF THE PERPENDICULAR TO A SEGMENT	PGR00640
C	PGR00650
C SLOP : VECTOR DIRECTION (LOCAL)	PGR00660
C SLOP : VECTOR DIRECTION +PP/2. (RETURN)	PGR00670
C X,Y : HOLE AXIS	PGR00680
C RA, : HOLE RADIUS	PGR00690
C XA,YA,XB,YB : HOLE WALLS PLUS OR MINUS RADIUS	PGR00700
C	PGR00710
SUBROUTINE PANG(X,Y,N,RA)	PGR00720
DIMENSION ANGL(50),X(50),Y(50)	PGR00730
COMMON/BL1/XA(50),YA(50),XB(50),YB(50),SLOP(50)	PGR00740
PP=3.1415927	PGR00750
N1=N-1	PGR00760
N2=N-2	PGR00770
DO 10 I=1,N1	PGR00780
F1=0.0	PGR00790
IF ((X(I+1)-X(I)).EQ.0.0) F1=PP/2.	PGR00800
IF ((X(I+1)-X(I)).NE.0.0) F1=ATAN((Y(I)-Y(I+1))/(X(I)-X(I+1)))	PGR00810
IF (F1.EQ.0.0.AND.X(I).LT.X(I+1)) F1=F1+PP	PGR00820
IF (F1.LT.0.0) F1=F1+PP	PGR00830
IF ((Y(I)-Y(I+1)).LT.0.0) F1=F1+PP	PGR00840
SLOP(I)=F1	PGR00850
10 CONTINUE	PGR00860
DO 20 I=2,N1	PGR00870
AS=SLOP(I-1)+PP	PGR00880
IF (AS.GT.2.0*PP) AS=AS-2.*PP	PGR00890
ANGL(I)=SLOP(I)-AS	PGR00900
IF (ANGL(I).GT.2.0*PP) ANGL(I)=ANGL(I)-2.*PP	PGR00910
IF (ANGL(I).LT.0.0) ANGL(I)=ANGL(I)+2.*PP	PGR00920
20 CONTINUE	PGR00930
C	PGR00940
C CALCULATE WALLS	PGR00950
C	PGR00960
DO 30 I=2,N1	PGR00970
AL=RA	PGR00980
F12=ANGL(I)/2.	PGR00990
IF (SIN(F12).NE.0.0) AL=RA/SIN(F12)	PGR01000
F13=SLOP(I-1)+F12	PGR01010
XA(I)=X(I)+AL*COS(F13)	PGR01020
YA(I)=Y(I)+AL*SIN(F13)	PGR01030
XB(I)=X(I)-AL*COS(F13)	PGR01040
YB(I)=Y(I)-AL*SIN(F13)	PGR01050
30 CONTINUE	PGR01060
C	PGR01070
C ADD POINTS N AND 1	PGR01080
C	PGR01090
AL=RA	PGR01100

A94

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      END
      SUBROUTINE PHOPRO (IRD,ICO)
      C
      C PROJECTS SINGLE HOLES AT THE THREE MAIN PLANES
      C
      C
      CHARACTER*4 AXI
      CHARACTER*32 STOPID
      DIMENSION HOL(50,3),X(50),Y(50),Z(50),NN1(4),XP(50),YP(50)
      COMMON/BL1/XA(50),YA(50),XB(50),YB(50),DIRE(50)
      PP=3.1415927
      C
      REWIND 51
      REWIND 61
      READ (51,19) STOPID
      READ (51,20) XREFER,YREFER,ZREFER
      READ (51,20) STLENG,STWINT,STDEPT
      READ (51,20) STANGR
      STANGR = STANGRPP/180.
      READ (51,100) NOHOLS
      6 FORMAT(11,'.',11)
      19 FORMAT(A32)
      20 FORMAT(4F10.2)
      C
      7 READ (61,100) IH0SEQ,N1,IH0RU,IH0CU,DIA,DIPNUM
      IF (IH0SEQ.EQ.99) WRITE (6,133)
      133 FORMAT (' HOLE NOT FOUND')
      IF (IH0SEQ.EQ.99) GO TO 999
      C-----
      C INCREASE HOLE DIAMETER BY A200 FOR PLOT CLARITY
      C
      DIA=DIA/400.0
      KA=DIA/2.0
      READ (61,101) XCULAR,YCULAR,ZCULAR
      C-----
      C STATION INTERVAL 10 FT
      C FOLLOWING DATA REFERS TO HOLE AXIS
      C-----
      READ (61,101,END=999) ((X(I),Y(I),Z(I)),I=1,N1)
      IF (IH0RU.NE.1KH0UR,IH0CU.NE.1CO) GO TO 7
      C
      CALL PTRANS(X,Y,Z,N1,XCULAR,YCULAR,ZCULAR)
      C-----
      C ROTATE COORDINATES (STANGR)
      C-----
      DO 200 I = 1,N1
      XC = X(I) * COS(STANGR) + Y(I) * SIN (STANGR)
      YC = - X(I) * SIN(STANGR) + Y(I) * COS (STANGR)
      X(I) = XC
      Y(I) = YC
      HOL(I,1) = X(I)
      HOL(I,2) = Y(I)
      HOL(I,3) = - Z(I)
      200 CONTINUE

```

```

C
100 FORMAT(415,2E10.2)
101 FORMAT(3E10.2)
C
108 WRITE (6,109)
109 FORMAT (2X,'GIVE # OF PROJECTIONS AND RESPECTIVE AXES'/
+2X,'(3) HORIZONTAL'/
+2X,'(2) PLANE XZ '/
+2X,'(1) PLANE YZ ')
      READ (5,A,END=108) NPRO,(NN1(1),1=1,NPRO)
C
      DO 130 IH1=1,NPRO
      NAXIS=NN1(IH1)
C
      GET X,Y ARRAYS FOR PLOT AND THE XTENT OF 'DEVIATION'
C
      IF (NAXIS.EQ.3) CALL PROJE2(HOL,N1,NAXIS,X,Y,Z,XMAX,YMAX,ZMAX)
      IF (NAXIS.EQ.2) CALL PROJE2(HOL,N1,NAXIS,X,Z,Y,XMAX,ZMAX,YMAX)
      IF (NAXIS.EQ.1) CALL PROJE2(HOL,N1,NAXIS,Z,X,Y,ZMAX,XMAX,YMAX)
      XWP=XMAX
      YWP=YMAX
      IF (XMAX.LT.4.0) XWP=4.0
      IF (YMAX.LT.4.0) YWP=4.0
      XW=XWPA2.0
      XW2=XWPA2.0
      YW=YWPA2.0
      YW2=YWPA1.30
      IF (NAXIS.NE.3) YW2=.25*YWP
C-----
C      CALL CMSCHD('EXEC LINEMODE ON.',IRC)
C
      CALL JBEGIN
      CALL JUNIT ( 1)
      CALL JOEVDN ( 1)
      CALL JUPINT (1)
      CALL JDJUST (2.2)
      CALL JDINTE (32767)
      CALL JUPIOX(2.0)
      CALL JDLSTY(0)
      CALL JDCOLR(7)
      CALL JSETER(7)
      CALL JVSFAC(-1.,1.,-1.,1.)
      CALL JVPORT (-1.,1.,-1.,1.)
      CALL JWINDO(-XW,XW,-YW,YW2)
      CALL JWCLIP (.FALSE.)
C-----
C      LETTER SIZE CALCULATIONS
C-----
      XLETR=4.0*XWPA0.04A0.7
      YLETR=(YW*YW2)*A0.04
      XLETR2=XLETR/2.
      YLETR2=YLETR/2.
C
      CALL JOYEN
      CALL JPIDEX (7.0)

```

PGR02210
 PGR02220
 PGR02230
 PGR02240
 PGR02250
 PGR02260
 PGR02270
 PGR02280
 PGR02290
 PGR02300
 PGR02310
 PGR02320
 PGR02330
 PGR02340
 PGR02350
 PGR02360
 PGR02370
 PGR02380
 PGR02390
 PGR02400
 PGR02410
 PGR02420
 PGR02430
 PGR02440
 PGR02450
 PGR02460
 PGR02470
 PGR02480
 PGR02490
 PGR02500
 PGR02510
 PGR02520
 PGR02530
 PGR02540
 PGR02550
 PGR02560
 PGR02570
 PGR02580
 PGR02590
 PGR02600
 PGR02610
 PGR02620
 PGR02630
 PGR02640
 PGR02650
 PGR02660
 PGR02670
 PGR02680
 PGR02690
 PGR02700
 PGR02710
 PGR02720
 PGR02730
 PGR02740
 PGR02750

```

CALL JMOVE (-XW,-YW)
CALL JRECT (2.0AXW,YW+YW2)
C
C DRAW SCALE MARKS ALONG THE TWO AXES
C
CALL JMARK(3)
C AXES.DRAW X OR HORIZONTAL
X1=-1.25AXWP
Y1=0.
CALL JMOVE(X1,Y1)
X1=-X1
CALL JCOLOR(2)
CALL JDRAW(X1,Y1)
N13=13
DO 15 L=1,N13
XP(L)=X1-(L-1)AX1/6.0
15 YP(L)=0.0
CALL JCOLOR(1)
CALL JPMARK(XP,YP,N13)
X1=-X1
Y1=-YLETR2
CALL JMOVE(X1,Y1)
CALL JSIZE(XLLTR2,YLETR2)
CALL JJUST(1,3)
IF(NAXIS.EQ.2.OR.NAXIS.EQ.3) CALL J3STRG('X')
IF(NAXIS.EQ.1) CALL J3STRG('Y')
901 FORMAT(F4.1)
904 FORMAT(F4.0)
902 FORMAT(A4)
903 FORMAT(I4)
N11=N13-2
CALL JJUST(2,3)
DO 16 L=3,N11,2
IF (L.EQ.7) GO TO 16
X1=XP(L)
Y1=-YLETR2
X2=ABS(X1)
WRITE(92,901) X2
BACKSPACE 92
READ(92,902) AX1
CALL JMOVE(X1,Y1)
CALL J3STRG(AX1)
16 CONTINUE
X1=1.25AXWP
CALL JMOVE(X1,Y1)
CALL JJUST(3,3)
IF(NAXIS.EQ.2.OR.NAXIS.EQ.3) CALL J3STRG('X')
IF(NAXIS.EQ.1) CALL J3STRG('Y')
IF(NAXIS.EQ.3) GO TO 136
VERTICAL AXIS (Z FOR OPTIONS 1 + 2)
X1=0.
Y1=0.

```

PGR02760
 PGR02770
 PGR02780
 PGR02790
 PGR02800
 PGR02810
 PGR02820
 PGR02830
 PGR02840
 PGR02850
 PGR02860
 PGR02870
 PGR02880
 PGR02890
 PGR02900
 PGR02910
 PGR02920
 PGR02930
 PGR02940
 PGR02950
 PGR02960
 PGR02970
 PGR02980
 PGR02990
 PGR03000
 PGR03010
 PGR03020
 PGR03030
 PGR03040
 PGR03050
 PGR03060
 PGR03070
 PGR03080
 PGR03090
 PGR03100
 PGR03110
 PGR03120
 PGR03130
 PGR03140
 PGR03150
 PGR03160
 PGR03170
 PGR03180
 PGR03190
 PGR03200
 PGR03210
 PGR03220
 PGR03230
 PGR03240
 PGR03250
 PGR03260
 PGR03270
 PGR03280
 PGR03290
 PGR03300

CALL JMOVE(Y1,X1)	PGR03310
X1=-1.15AYWP	PGR03320
CALL JCOLOR(2)	PGR03330
CALL JORAW(Y1,X1)	PGR03340
N4=4	PGR03350
DO 225 L=1,N4	PGR03360
XP(L)=-YMAX*(L-1)AYMAX/4.0	PGR03370
225 YP(L)=0.0	PGR03380
CALL JCOLOR(1)	PGR03390
CALL JPMARK(YP,XP,N4)	PGR03400
X1=X1	PGR03410
Y1=-XLETR2	PGR03420
CALL JMOVE(Y1,X1)	PGR03430
CALL JJUST(3,2)	PGR03440
IF(NAXIS.EQ.2.OR.NAXIS.EQ.1) CALL J3STRG('-Z')	PGR03450
IF(NAXIS.EQ.3) CALL J3STRG('-Y')	PGR03460
CALL JJUST(3,2)	PGR03470
DO 226 L=1,N4	PGR03480
X1=XP(L)	PGR03490
X2=ABS(X1)	PGR03500
WRITE(92,904) X2	PGR03510
BACKSPACE 92	PGR03520
READ(92,902) AX1	PGR03530
CALL JMOVE(-XLETR2,X1)	PGR03540
CALL J3STRG(AX1)	PGR03550
226 CONTINUE	PGR03560
GO TO 137	PGR03570
	PGR03580
	PGR03590
C 1 AXIS FOR OPTION 3	PGR03600
	PGR03610
136 X1=-1.25AYWP	PGR03620
Y1=0.	PGR03630
CALL JMOVE(Y1,X1)	PGR03640
X1=-X1	PGR03650
CALL JCOLOR(2)	PGR03660
CALL JORAW(Y1,X1)	PGR03670
N13=13	PGR03680
N11=N13-2	PGR03690
DO 25 L=1,N13	PGR03700
XP(L)=X1-(L-1)AX1/6.0	PGR03710
25 YP(L)=0.0	PGR03720
CALL JCOLOR(1)	PGR03730
CALL JPMARK(YP,XP,N13)	PGR03740
X1=-X1	PGR03750
Y1=-XLETR2	PGR03760
CALL JMOVE(Y1,X1)	PGR03770
CALL JJUST(3,2)	PGR03780
IF(NAXIS.EQ.2.OR.NAXIS.EQ.1) CALL J3STRG('-Z')	PGR03790
IF(NAXIS.EQ.3) CALL J3STRG('-Y')	PGR03800
	PGR03810
CALL JJUST(3,2)	PGR03820
DO 26 L=3,N11,2	PGR03830
IF (L.EQ.7) GO TO 26	PGR03840
X1=XP(L)	PGR03850

A98

```

Y1=-XLETR2
X2=ABS(X1)
WRITE(92,901) X2
BACKSPACE 92
READ(92,902) AX1
CALL JMOVE(Y1,X1)
CALL J3STRG(AX1)

```

26 CONTINUE

```

X1=1.25AYWP
CALL JMOVE(Y1,X1)
CALL JJUST(3,2)
IF(NAXIS.EQ.2.OR.NAXIS.EQ.1) CALL J3STRG('Z')
IF(NAXIS.EQ.3) CALL J3STRG('Y')

```

137 CONTINUE

CALL PANG TO FIND THE DIRECTIONS OF THE DEPTH INDICATORS

CALL PANG (X,Y,N1,KA)

DRAW HOLE AXIS ONLY (IF TWO LINES ARE TO BE PLOTTED IT GETS TOO MESSY)

```

CALL JMOVE(X(1),Y(1))
CALL JCOLOR(1)
CALL JPOLY(X,Y,N1)

```

```

IF (NAXIS.NE.3) GO TO 132
DZ=HOL(N1,3)-HOL(1,3)
DZ1=50.
IF (ABS(DZ).LT.120.0) DZ1=20.
IF (ABS(DZ).LT.60.) DZ1=10.
DZ1=SIGN(DZ1,DZ)
NZ=DZ/DZ1

```

INDICATE DEPTH ON HORIZONTAL PROJECTION ONLY

```

DO 110 J=1,NZ
DZ=DZ1*J
PO 111 I=1,N1
IF (HOL(I,3).GT.DZ) GO TO 111
XA(J)=X(1)+(DZ-HOL(1,3))/(HOL(I-1,3)-HOL(1,3))*X(I-1)-X(1)
XB(J)=XA(J)+XLETR2ACOS(DIRE(1))
YA(J)=Y(1)+(DZ-HOL(1,3))/(HOL(I-1,3)-HOL(1,3))*Y(I-1)-Y(1)
YB(J)=YA(J)+YLETR2ASIN(DIRE(1))
CALL JMOVE(XA(J),YA(J))
CALL JORAW(XB(J),YB(J))

```

```

AN=DIRE(1)
IF (AN.LT. 45..OR. AN.GE.315.) CALL JJUST (1,2)
IF (AN.GT. 45..AND. AN.LT.135.) CALL JJUST (2,1)
IF (AN.GE.135..AND. AN.LT.225.) CALL JJUST (3,2)
IF (AN.GE.225..AND. AN.LT.315.) CALL JJUST (2,3)
ID2=INT(DZ)

```

PGR03860
 PGR03870
 PGR03880
 PGR03890
 PGR03900
 PGR03910
 PGR03920
 PGR03930
 PGR03940
 PGR03950
 PGR03960
 PGR03970
 PGR03980
 PGR03990
 PGR04000
 PGR04010
 PGR04020
 PGR04030
 PGR04040
 PGR04050
 PGR04060
 PGR04070
 PGR04080
 PGR04090
 PGR04100
 PGR04110
 PGR04120
 PGR04130
 PGR04140
 PGR04150
 PGR04160
 PGR04170
 PGR04180
 PGR04190
 PGR04200
 PGR04210
 PGR04220
 PGR04230
 PGR04240
 PGR04250
 PGR04260
 PGR04270
 PGR04280
 PGR04290
 PGR04300
 PGR04310
 PGR04320
 PGR04330
 PGR04340
 PGR04350
 PGR04360
 PGR04370
 PGR04380
 PGR04390
 PGR04400

A99

[illegible]

PGR04410
 PGR04420
 PGR04430
 PGR04440
 PGR04450
 PGR04460
 PGR04470
 PGR04480
 PGR04490
 PGR04500
 PGR04510
 PGR04520
 PGR04530
 PGR04540
 PGR04550
 PGR04560
 PGR04570
 PGR04580
 PGR04590
 PGR04600
 PGR04610
 PGR04620
 PGR04630
 PGR04640
 PGR04650
 PGR04660
 PGR04670
 PGR04680
 PGR04690
 PGR04700
 PGR04710
 PGR04720
 PGR04730
 PGR04740
 PGR04750
 PGR04760
 PGR04770
 PGR04780
 PGR04790
 PGR04800
 PGR04810
 PGR04820
 PGR04830
 PGR04840
 PGR04850
 PGR04860
 PGR04870
 PGR04880
 PGR04890
 PGR04900
 PGR04910
 PGR04920
 PGR04930
 PGR04940
 PGR04950

DIMENSION X(50),Y(50),Z(50)	PGR04960
DIMENSION HUL(50,3),XP(50),YP(50),DIAM(50)	PGR04970
PP=3.1415926	PGR04980
REWIND 51	PGR04990
REWIND 61	PGR05000
READ (51,19) STOPID	PGR05010
READ (51,20) XREFER,YREFER,ZREFER	PGR05020
READ (51,20) STLENG,STWIDT,STDEPT	PGR05030
READ (51,20) STANGR	PGR05040
STANGR = STANGRAPP/180.	PGR05050
READ (51,100) NOHOLS	PGR05060
PLELEV=PLELEV-ZREFER	PGR05070
IF (PLELEV.LT.0.0) RETURN	PGR05080
6 FORMAT(11,' ',11)	PGR05090
19 FORMAT(A32)	PGR05100
20 FORMAT(4F10.2)	PGR05110
C-----	PGR05120
C WINDOW DIMENSION CALCULATIONS	PGR05130
C-----	PGR05140
XWIND = STLENG	PGR05150
IF (STWIDT.GT.STLENG) XWIND = STWIDT	PGR05160
YWIND = XWIND	PGR05170
C-----	PGR05180
C CALL CASCAD('EXEC LINEMODE ON.',IRC)	PGR05190
C	PGR05200
CALL JBEGIN	PGR05210
CALL JINITI (1)	PGR05220
CALL JOEVEN (1)	PGR05230
CALL JDPINT (1)	PGR05240
CALL JDJUST (2,2)	PGR05250
CALL JDATE (32767)	PGR05260
CALL JPIDIX(7,0)	PGR05270
CALL JDLSTY(0)	PGR05280
CALL JDCOLR(7)	PGR05290
CALL JSETER(7)	PGR05300
CALL JVSPAC(-1.,1.,-1.,1.)	PGR05310
CALL JVPORF (-0.8,0.8,-0.8,0.8)	PGR05320
CALL JWINDO(0.0,XWIND,0.0,YWIND)	PGR05330
CALL JWCLIP (.FALSE.)	PGR05340
C-----	PGR05350
C LETTER SIZE CALCULATIONS	PGR05360
C-----	PGR05370
XLETR=.04AXWIND	PGR05380
YLETR=.04AXWIND*.7	PGR05390
XLETR2=XLETR/2.	PGR05400
YLETR2=YLETR/2.	PGR05410
C	PGR05420
CALL JOPEN	PGR05430
CALL JPIDEX (7,0)	PGR05440
CALL JMOVE (-0.1AXWIND,-0.1AYWIND)	PGR05450
CALL JRECT (1.2AXWIND,1.2AYWIND)	PGR05460
CALL JPIDEX (2,0)	PGR05470
CALL JMOVE (0.0,0.0)	PGR05480
CALL JRECT (STLENG,STWIDT)	PGR05490
C	PGR05500

A101

C DRAW SCALE MARKS ALONG THE TWO AXES

C

IM=INT(STWIDT/10.)+1

DO 400 I=1,IM

X(I)=0.

Y(I)=(I-1)A10.

400 CONTINUE

CALL JJUST(3,2)

CALL JCOLOR(1)

CALL JSIZE(XLETR2,YLETR2)

DO 401 I=1,IM

XSS=X(I)-XLETR2

YSS=Y(I)

CALL JMOVE(XSS,YSS)

AW=(I-1)A10.

WRITE (92,102) AW

BACKSPACE 92

READ (92,103) AA1

CALL J3STRG(AA1)

XSS=X(I)-XLETR2/2.

YSS=Y(I)

CALL JMOVE(XSS,YSS)

CALL JDRAW(X(I),Y(I))

401 CONTINUE

IM=INT(STLENG/10.)+1

DO 405 I=1,IM

Y(I)=0.

X(I)=(I-1)A10.

405 CONTINUE

CALL JJUST(2,3)

DO 406 I=1,IM

XSS=X(I)

YSS=Y(I)-YLETR2

CALL JMOVE(XSS,YSS)

AW=(I-1)A10.

WRITE (92,102) AW

BACKSPACE 92

READ (92,103) AA1

CALL J3STRG(AA1)

XSS=X(I)

YSS=Y(I)-YLETR2/2.

CALL JMOVE(XSS,YSS)

CALL JDRAW(X(I),Y(I))

406 CONTINUE

C

C MARKS DRAWN

C

C READ HOLE DATA

C

99 DENOTES END OF HOLE DATA FILE

C

C

7 READ (61,100) IHUSEQ,N1,IHROW,IHCOL,DIA,DIPNOM

IF (IHUSEQ.EQ.99) GO TO 8

C

C

INCREASE HOLE DIAMETER BY A200 FOR PLOT CLARITY

PGK05510

PGK05520

PGK05530

PGK05540

PGK05550

PGK05560

PGK05570

PGK05580

PGK05590

PGK05600

PGK05610

PGK05620

PGK05630

PGK05640

PGK05650

PGK05660

PGK05670

PGK05680

PGK05690

PGK05700

PGK05710

PGK05720

PGK05730

PGK05740

PGK05750

PGK05760

PGK05770

PGK05780

PGK05790

PGK05800

PGK05810

PGK05820

PGK05830

PGK05840

PGK05850

PGK05860

PGK05870

PGK05880

PGK05890

PGK05900

PGK05910

PGK05920

PGK05930

PGK05940

PGK05950

PGK05960

PGK05970

PGK05980

PGK05990

PGK06000

PGK06010

PGK06020

PGK06030

PGK06040

PGK06050

A102

C	DIA=DIA/200.0	PG06060
	READ (61,101) XCULAR,YCULAR,ZCULAR	PG06070
C	-----	PG06080
C	STATION INTERVAL 10 FT	PG06090
C	FOLLOWING DATA REFERS TO HOLE AXIS	PG06100
C	-----	PG06110
	READ (61,101,END=9) ((X(I),Y(I),Z(I)),I=1,N1)	PG06120
	CALL PTRANS(X,Y,Z,N1,XREFER,YREFER,ZREFER)	PG06130
C	-----	PG06140
C	ROTATE COORDINATES (STANGR)	PG06150
C	-----	PG06160
	DO 200 I = 1,N1	PG06170
	XC = X(I) * COS(STANGR) + Y(I) * SIN (STANGR)	PG06180
	YC = - X(I) * SIN(STANGR) + Y(I) * COS (STANGR)	PG06190
	X(I) = XC	PG06200
	Y(I) = YC	PG06210
	HOL(I,1) = X(I)	PG06220
	HOL(I,2) = Y(I)	PG06230
	HOL(I,3) = Z(I)	PG06240
	200 CONTINUE	PG06250
C	-----	PG06260
C	ROTATE COORDINATES	PG06270
C	-----	PG06280
	DO 10 I=2,N1	PG06290
	IF (HOL(I,3).LT.PLELEV) GO TO 10	PG06300
	XP(1)=HOL(I,1)+(PLELEV-HOL(I,3))/(HOL(I-1,3)-HOL(I,3))*HOL(I-1,	PG06310
	A1)-HOL(I,1))	PG06320
	YP(1)=HOL(I,2)+(PLELEV-HOL(I,3))/(HOL(I-1,3)-HOL(I,3))*HOL(I-1,	PG06330
	A2)-HOL(I,2))	PG06340
	GO TO 11	PG06350
10	CONTINUE	PG06360
11	CONTINUE	PG06370
	XP(2)=HOL(I,1)	PG06380
	YP(2)=HOL(I,2)	PG06390
	Z1=1.	PG06400
	N12=6	PG06410
	X1=XP(1)	PG06420
	X2=XP(2)	PG06430
	Y1=YP(1)	PG06440
	Y2=YP(2)	PG06450
	RA=DIA	PG06460
C	-----	PG06470
C	TAG HOLES ON PLOT	PG06480
C	-----	PG06490
	CALL JCOLOR(8)	PG06500
	X12=X1	PG06510
	Y12=Y1	PG06520
	EI=0.0	PG06530
	IF ((X1-X2).EQ.0.0) E1=PP/2.	PG06540
	IF ((X1-X2).NL.0.0) E1=ATAN((Y1-Y2)/(X1-X2))	PG06550
	IF (E1.EQ.0.0.AND.Y2.LT.Y1) E1=E1+PP	PG06560
	IF (E1.LT.0.0) E1=E1+PP	PG06570
	IF ((X2-X1).LT.0.0) E1=E1+PP	PG06580
	WRITE (92,6) IHOROW,IHUCOL	PG06590
		PG06600

A103

```

BACKSPACE 92
READ (92,137) AA2
CALL JSIZE(XLETR2,YLETR2)
CALL JGAP(0.)
CALL JJUST(1,2)
IF (X2.GT.X1) CALL JJUST(3,2)
IF (X2.GT.X1) CALL JMOVE(X12-XLETR2/2.0,Y12)
IF (X2.LE.X1) CALL JMOVE(X12+XLETR2/2.0,Y12)
CALL JSTRG(AA2)
C-----
C HOLE ID TAG END
C-----
CALL JLSTYL(0)
CALL JPIDEX(1,32767)
CALL JMOVE(X1,Y1)
CALL JCIRCL(X1,Y1,Z1,RA,N12)
C PERPENDICULAR
C
X3=X1+RAACOS(F1+PP/2.)
Y3=Y1+RAASIN(F1+PP/2.)
CALL JMOVE(X3,Y3)
X4=X2+RAACOS(F1+PP/2.)
Y4=Y2+RAASIN(F1+PP/2.)
CALL JLSTYL(1)
CALL JDRAW(X4,Y4)
CALL JMOVE(X2,Y2)
CALL JCOLOR(8)
CALL JPINTR(1)
CALL JPIDEX(8,0)
CALL JCIRCL(X2,Y2,Z1,RA,N12)
C-----
C DRAW AXES ON THE PROJECTION OF TOP TO DISTINGUISH FROM BOTTOM
C-----
X3=X2-RAA1.5
CALL JMOVE(X3,Y2)
X3=X2+RAA1.5
CALL JLSTYL(1)
CALL JDRAW(X3,Y2)
Y3=Y2-RAA1.5
CALL JMOVE(X2,Y3)
Y3=Y2+RAA1.5
CALL JDRAW(X2,Y3)
X3=X2+RAACOS(F1+3.0APP/2.)
Y3=Y2+RAASIN(F1+3.0APP/2.)
CALL JMOVE(X3,Y3)
X3=X1+RAACOS(F1+3.0APP/2.)
Y3=Y1+RAASIN(F1+3.0APP/2.)
CALL JLSTYL(2)
CALL JDRAW(X3,Y3)
C 26 CONTINUE
GO TO 7
8 CONTINUE
C-----
C DRAW TITLE
C-----

```

PGR0661
 PGR0662
 PGR0663
 PGR0664
 PGR0665
 PGR0666
 PGR0667
 PGR0668
 PGR0669
 PGR0670
 PGR0671
 PGR0672
 PGR0673
 PGR0674
 PGR0675
 PGR0676
 PGR0677
 PGR0678
 PGR0679
 PGR0680
 PGR0681
 PGR0682
 PGR0683
 PGR0684
 PGR0685
 PGR0686
 PGR0687
 PGR0688
 PGR0689
 PGR0690
 PGR0691
 PGR0692
 PGR0693
 PGR0694
 PGR0695
 PGR0696
 PGR0697
 PGR0698
 PGR0699
 PGR0700
 PGR0701
 PGR0702
 PGR0703
 PGR0704
 PGR0705
 PGR0706
 PGR0707
 PGR0708
 PGR0709
 PGR0710
 PGR0711
 PGR0712
 PGR0713
 PGR0714
 PGR0715

A105

```

        DIMENSION HUL(50,3)
        DIMENSION XX(40),YY(40)
        DIMENSION MAT(21)
        COMMON/BL1/XA(50),YA(50),XB(50),YB(50),DIRE(50)
        PP=3.1415926
61 WRITE (6,65)
65 FORMAT(2X,'DO YOU WISH TO DRAW THE CHARGES? 1=Y')
        READ (5,*,END=61) ICH

```

```

C
        REWIND 51
        REWIND 61
        READ (51,19) STOPID
        READ (51,20) XREFER,YREFER,ZREFER
        READ (51,20) STLENG,STWIDT,STDEPT
        READ (51,20) STANGR
        STANGR = STANGRAPP/180.
        6 FORMAT(11,',',',',11)
        19 FORMAT(A32)
        20 FORMAT(4F10.2)

```

```

C
C-----
C WINDOW DIMENSION CALCULATIONS
C-----

```

```

        YWIND = STDEPT
        XWIND = STWIDT
        IF (IRC.EQ.1) XWIND=STLENG

```

```

C-----
C CALL CMSMD('EXEC LINEMODE ON.',IRCODE)
C

```

```

        CALL JBEGIN
        CALL JDINIT ( 1)
        CALL JDEVON ( 1)
        CALL JDPINT (1)
        CALL JDJUST (2,2)
        CALL JDINTE (32767)
            CALL JPIIDX(2,0)
            CALL JDLSTY(0)
            CALL JDCULR(7)
            CALL JSETER(7)
            CALL JVSPEC(-1.,1.,-1.,1.)
            CALL JVPOR (-0.8,0.8,-.8,0.8)
            CALL JWINDW(0.0,XWIND,-YWIND,0.0)
            CALL JWCLIP (.FALSE.)

```

```

C-----
C LETTER SIZE CALCULATIONS
C-----

```

```

        XLETR=.04*XWIND
        YLETR=.04*YWIND*.7
        XLETR2=XLETR/2.
        YLETR2=YLETR/2.
        XLETR3 = XLETR2/1.3
        YLETR3 = YLETR2/1.3

```

```

C
        CALL JOPEN
        CALL JPIDEX (7,0)

```

PGR07710
 PGR07720
 PGR07730
 PGR07740
 PGR07750
 PGR07760
 PGR07770
 PGR07780
 PGR07790
 PGR07800
 PGR07810
 PGR07820
 PGR07830
 PGR07840
 PGR07850
 PGR07860
 PGR07870
 PGR07880
 PGR07890
 PGR07900
 PGR07910
 PGR07920
 PGR07930
 PGR07940
 PGR07950
 PGR07960
 PGR07970
 PGR07980
 PGR07990
 PGR08000
 PGR08010
 PGR08020
 PGR08030
 PGR08040
 PGR08050
 PGR08060
 PGR08070
 PGR08080
 PGR08090
 PGR08100
 PGR08110
 PGR08120
 PGR08130
 PGR08140
 PGR08150
 PGR08160
 PGR08170
 PGR08180
 PGR08190
 PGR08200
 PGR08210
 PGR08220
 PGR08230
 PGR08240
 PGR08250


```

CALL JMOVE (-0.1AXWIND,-1.1AYWIND)
CALL JRECT (1.2AXWIND,1.2AYWIND)
CALL JPIDEX (2.0)
CALL JMOVE (0.0,-YWIND)
CALL JRECT (XWIND,YWIND)

```

PGR08260
PGR08270
PGR08280
PGR08290
PGR08300
PGR08310

```

C
C DRAW SCALE MARKS ALONG THE TWO AXES
C

```

PGR08320
PGR08330
PGR08340
PGR08350
PGR08360
PGR08370

```

      IM=INT(YWIND/10.0)+1
      DO 400 I=1,IM
      X(I)=0.
      Y(I)=(1-I)*10.
400 CONTINUE
      CALL JCOLOR(1)
      CALL JJUST(3,2)
      CALL JSIZE(XLETR2,YLETR2)
      DO 401 I=1,IM
      CALL JMOVE(X(I)-XLETR2,Y(I))
      AW=(I-1)*10.
      WRITE (92,110) AW
      BACKSPACE 92
      READ (92,103) AA1
      CALL J3STRG(AA1)
      CALL JMOVE(X(I)-XLETR2/2.,Y(I))
      CALL JDRAW(X(I),Y(I))

```

PGR08380
PGR08390
PGR08400
PGR08410
PGR08420
PGR08430

```

401 CONTINUE

```

PGR08440
PGR08450
PGR08460
PGR08470
PGR08480
PGR08490

```

C
      IM=INT(XWIND/10.0)+1
      DO 405 I=1,IM
      Y(I)=-YWIND
      X(I)=(1-I)*10.
405 CONTINUE

```

PGR08500
PGR08510
PGR08520
PGR08530
PGR08540
PGR08550

```

C
      CALL JJUST(2,3)
      CALL JSIZE(XLETR2,YLETR2)
      DO 406 I=1,IM
      CALL JMOVE(X(I),Y(I)-YLETR2)
      AW=(I-1)*10.
      WRITE (92,110) AW
      BACKSPACE 92
      READ (92,103) AA1
      CALL J3STRG(AA1)
      CALL JMOVE(X(I),Y(I)-YLETR2/2.)
      CALL JDRAW(X(I),Y(I))

```

PGR08560
PGR08570
PGR08580
PGR08590
PGR08600
PGR08610

```

406 CONTINUE

```

PGR08620
PGR08630
PGR08640
PGR08650
PGR08660
PGR08670

```

C MARKS DRAWN

```

PGR08680
PGR08690
PGR08700
PGR08710
PGR08720
PGR08730

```

C
C -----
40 READ (61,100) IHUSEQ,N1,IHORO,IHOCO,DIA,DIPNDW
   IF (IHUSEQ.EQ.99) GO TO 41
   DIA=DIA/200.0
   PA =DIA/2.0
   READ (61,101) XCULAR,YCULAR,ZCULAR

```

PGR08740
PGR08750
PGR08760
PGR08770
PGR08780
PGR08790

```

C
C STATION INTERVAL 10 FT

```

PGR08800

C	FOLLOWING DATA REFERS TO HOLE AXIS	PG00881
C	-----	PG00882
	READ (61,101,END=41) ((X(I),Y(I),Z(I)),I=1,N1)	PG00883
	IF (IRC.EQ.2.AND.IHORO.NE.IHRC) GO TO 40	PG00884
	IF (IRC.EQ.1.AND.IHOCO.NE.IHRC) GO TO 40	PG00885
C	-----	PG00886
C	PERFORM A TRANSLATION WRT THE POINT XREF,YREF,ZREF	PG00887
C	-----	PG00888
	CALL PTRANS(X,Y,Z,N1,XREFER,YREFER,ZREFER)	PG00889
C	-----	PG00890
C	ROTATE COORDINATES (STANGR)	PG00891
C	-----	PG00892
	DO 200 I = 1,N1	PG00893
	XC = X(I) * COS(STANGR) + Y(I) * SIN (STANGR)	PG00894
	YC = - X(I) * SIN(STANGR) + Y(I) * COS (STANGR)	PG00895
	X(I) = XC	PG00896
	Y(I) = YC	PG00897
200	CONTINUE	PG00898
	DO 51 I=1,N1	PG00899
	IF (IRC.EQ.2) X(I)=Y(I)	PG00900
51	Y(I)= - Z(I)	PG00901
C	-----	PG00902
C	CALL PANG(X,Y,N1,KA)	PG00903
C	DRAW HOLE	PG00904
	CALL JMOVE(XB(1),YB(1))	PG00905
	CALL JPOLY(XB,YB,N1)	PG00906
	CALL JMOVE(XA(1),YA(1))	PG00907
	CALL JPOLY(XA,YA,N1)	PG00908
C	-----	PG00909
C	DRAW AXIS ONLY	PG00910
C	-----	PG00911
	CALL JMOVE(XA(N1),YA(N1))	PG00912
	CALL JDRAW(XB(N1),YB(N1))	PG00913
C	ANGLES INCORPORATED	PG00914
C	TAG	PG00915
	CALL JSIZE(XLETR,YLETR)	PG00916
	CALL JJUST(2,1)	PG00917
	WRITE (92,6) IHORO,IHOCO	PG00918
	BACKSPACE 92	PG00919
	READ (92,103) AA1	PG00920
	CALL JMOVE(X(1),Y(1)+YLETR/4.)	PG00921
	CALL J3STKG(AA1)	PG00922
C	-----	PG00923
C	TAG END	PG00924
C	-----	PG00925
C	DRAW CHARGES	PG00926
C	-----	PG00927
	IF (ICH.N1.1) GO TO 40	PG00928
C	-----	PG00929
C	READ CHARGE INFO NCHRG= CHARGES+NO OF STEMMINGS	PG00930
	REWIND 62	PG00931
105	READ (62,21) NCHRG,IR0,IC0	PG00932
	IF (NCHRG.EQ.99) GO TO 40	PG00933
	DO 300 L=1,NCHRG	PG00934
		PG00935

READ (62,17) DEST,DEF1,AST,AFI,QUANT,CHDIA,1EXPLT	PGR09360
A,1DELT	PGR09370
21 FORMAT(15I5)	PGR09380
17 FORMAT(6F10.2,2I5)	PGR09390
IF (IRO.NE.1HOKO.OK.ICG.NE.1HOCO) GO TO 300	PGR09400
IF (QUANT.LI.0.01) GO TO 300	PGR09410
C LOCATE	PGR09420
CHRA=CHDIA/400.	PGR09430
C	PGR09440
DO 70 I=1,N1	PGR09450
IF (YB(I).GT.DEST) GO TO 70	PGR09460
YST=XB(I)+(DEST-YB(I))/(YB(I-1)-YB(I))*A(XB(I-1)-XB(I))	PGR09470
NYS=I-1	PGR09480
GO TO 71	PGR09490
70 CONTINUE	PGR09500
71 CONTINUE	PGR09510
DO 80 I=1,N1	PGR09520
IF (YB(I).GE.DEF1) GO TO 80	PGR09530
YFI=XB(I)+(DEF1-Y(I))/(Y(I-1)-Y(I))*A(XB(I-1)-XB(I))	PGR09540
NYF=I	PGR09550
GO TO 81	PGR09560
80 CONTINUE	PGR09570
81 I1=1	PGR09580
XX(I1)=YFI	PGR09590
YY(I1)=DEF1	PGR09600
IF (NYF.GT.NYS) GO TO 90	PGR09610
OO 35 I=NYF,NYS	PGR09620
I1=I1+1	PGR09630
XX(I1)=XB(I)	PGR09640
YY(I1)=YB(I)	PGR09650
85 CONTINUE	PGR09660
90 CONTINUE	PGR09670
I1=I1+1	PGR09680
XX(I1)=YST	PGR09690
YY(I1)=DEST	PGR09700
C	PGR09710
DO 170 I=1,N1	PGR09720
IF (YA(I).GT.DEST) GO TO 170	PGR09730
YST=XA(I)+(DEST-YA(I))/(YA(I-1)-YA(I))*A(XA(I-1)-XA(I))	PGR09740
NYS=I-1	PGR09750
GO TO 171	PGR09760
170 CONTINUE	PGR09770
171 CONTINUE	PGR09780
DO 180 I=1,N1	PGR09790
IF (YA(I).GE.DEF1) GO TO 180	PGR09800
YFI=XA(I)+(DEF1-YA(I))/(YA(I-1)-YA(I))*A(XA(I-1)-XA(I))	PGR09810
NYF=I	PGR09820
GO TO 181	PGR09830
180 CONTINUE	PGR09840
181 I1=I1+1	PGR09850
IL1=I1	PGR09860
XX(I1)=YST	PGR09870
YY(I1)=DEST	PGR09880
IF (NYF.GT.NYS) GO TO 190	PGR09890
DO 1135 I=NYF,NYS	PGR09900

A109

```

      JJ1=NYS+NYE-I
      IL=IL+1
      XX(IL)=XA(JJ1)
      YY(IL)=YA(JJ1)
1185 CONTINUE
190 CONTINUE
      IL=IL+1
      XX(IL)=YFI
      YY(IL)=DEFI
      IL2=IL
      IF (XX(1).LT.XX(IL)) GO TO 197
      IL1=IL-1
      IL2=1
C
197 X1=XX(1)
      Y1=YY(1)
      CALL JMOVE(X1,Y1)
      MATER=2
      IF (MATER.EQ.2) MCOL = 1
      IF (MATER.EQ.1) MCOL = 6
      CALL JPINDEX(MCOL,3AMATER)
      CALL JPOLGN(XX,YY,IL)
      CALL JSIZE(XLETR3,YLETR3)
      X1=XX(IL1)
      Y1=YY(IL1)
      X2=XX(IL2)
      Y2=YY(IL2)
      CALL JMOVE(X1+XLETR3/5.,Y1)
      WRITE (92,108) AST
      BACKSPACE 92
      READ (92,103) AA1
      CALL JJUST(1,3)
      CALL J3STRG(AA1)
      WRITE (92,108) AF1
      BACKSPACE 92
      READ (92,103) AA1
      CALL JJUST(1,1)
      CALL JMOVE(X2+XLETR3/5.,Y2)
      CALL J3STRG(AA1)
      Y3=(Y2+Y1)/2.
      X3=AMAX1(X1,X2)
      CALL JMOVE(X3+XLETR3/5.,Y3+YLETR3/5.)
      WRITE (92,108) QUANT
      BACKSPACE 92
      READ (92,103) AA1
      CALL JJUST(1,1)
      CALL J3STRG(AA1)
      CALL JMOVE(X3+XLETR3/5.,Y3-YLETR3/5.0)
      WRITE (92,109) IDELT
      BACKSPACE 92
      READ (92,103) AA1
      CALL JJUST(1,3)
      CALL J3STRG(AA1)
300 CONTINUE
C

```

```

PGR09910
PGR09920
PGR09930
PGR09940
PGR09950
PGR09960
PGR09970
PGR09980
PGR09990
PGR10000
PGR10010
PGR10020
PGR10030
PGR10040
PGR10050
PGR10060
PGR10070
PGR10080
PGR10090
PGR10100
PGR10110
PGR10120
PGR10130
PGR10140
PGR10150
PGR10160
PGR10170
PGR10180
PGR10190
PGR10200
PGR10210
PGR10220
PGR10230
PGR10240
PGR10250
PGR10260
PGR10270
PGR10280
PGR10290
PGR10300
PGR10310
PGR10320
PGR10330
PGR10340
PGR10350
PGR10360
PGR10370
PGR10380
PGR10390
PGR10400
PGR10410
PGR10420
PGR10430
PGR10440
PGR10450

```

A110

GO TO 185	PGR10460
41 CONTINUE	PGR10470
C-----	PGR10480
C TITLE	PGR10490
CALL JSIZE(XLETR,YLETR)	PGR10500
CALL JCAP(0.)	PGR10510
CALL JJUST(1,1)	PGR10520
CALL JMOVE(0.,0.05*YWIND)	PGR10530
IF(IRC.EQ.2) CALL J3STRG('CROSS SECTION ON ROW')	PGR10540
IF(IRC.EQ.1) CALL J3STRG('CROSS SECTION ON COLUMN')	PGR10550
WRITE (92,107) IIRC	PGR10560
BACKSPACE 92	PGR10570
READ (92,113) AA2	PGR10580
X1=(22.0+(2-IRC)*2)*XLETR	PGR10590
CALL JMOVE(X1,0.05*YWIND)	PGR10600
CALL JJUST(1,1)	PGR10610
CALL J3STRG(AA2)	PGR10620
C	PGR10630
100 FORMAT(4I5,2F10.2)	PGR10640
101 FORMAT(3F10.2)	PGR10650
102 FORMAT(F10.2)	PGR10660
108 FORMAT(F5.1)	PGR10670
103 FORMAT(A4)	PGR10680
107 FORMAT(I2)	PGR10690
109 FORMAT('#',I2)	PGR10700
110 FORMAT(F6.1)	PGR10710
113 FORMAT(A2)	PGR10720
CALL JCLOSE	PGR10730
CALL JPAUSE (1)	PGR10740
CALL JDEVPF (1)	PGR10750
CALL JDEND (1)	PGR10760
CALL JEND	PGR10770
RETURN	PGR10780
END	PGR10790

4. GRAPHICS OUTPUT GENERATOR FOR THE VERTICAL
CRATER RETREAT AFTER BLAST PROFILE

A112

```

PROGRAM PLBLVC                                PLB00010
CCCCCCCCCC( CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC) PLB00020
C                                           C PLB00030
C PURPOSE :                               C PLB00040
C     TO CREATE GRAPHICS OUTPUT FOR VERM.   C PLB00050
C     GRAPHICS LANGUAGE : B13000          C PLB00060
C                                           C PLB00070
CCCCCCCCCC( CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC) PLB00080
CHARACTER A4 XALPHA                        PLB00090
CHARACTER A2 XALP                          PLB00100
CHARACTER A32 STUPID                      PLB00110
INTEGER HUES,SATS,LIGHTS,INDEXS,IWR      PLB00120
DIMENSION HUES(24),SATS(24),LIGHTS(24),INDEXS(24),IWR(100) PLB00130
WRITE(7,3)                                PLB00140
3 FORMAT(' ENTER NUMBER OF HOLES IN THE BLAST :') PLB00150
READ(7,A) NURBH                           PLB00160
WRITE(7,4)                                 PLB00170
4 FORMAT(' ENTER MAX AND MIN FOR X AND Y COORDINATES OF THE STOPE' PLB00180
X./ ' IN THE ORDER XMAX,XMIN,YMAX,YMIN :') PLB00190
READ (7,A) XMAX,XMIN,YMAX,YMIN           PLB00200
WRITE(7,B)                                PLB00210
8 FORMAT(' ENTER ELEVATION OF THE FREE FACE :') PLB00220
READ(7,A) PLELEV                         PLB00230
----- PLB00240
C AA    CREATE SHADES OF THE SAME COLOR    AA PLB00250
----- PLB00260
INDEXS(1) = 10                            PLB00270
INDEXS(2) = 11                            PLB00280
INDEXS(3) = 12                            PLB00290
INDEXS(4) = 13                            PLB00300
INDEXS(5) = 14                            PLB00310
INDEXS(6) = 15                            PLB00320
INDEXS(7) = 16                            PLB00330
HUES(1) = 0                              PLB00340
HUES(2) = 0                              PLB00350
HUES(3) = 0                              PLB00360
HUES(4) = 0                              PLB00370
HUES(5) = 0                              PLB00380
HUES(6) = 0                              PLB00390
HUES(7) = 120                             PLB00400
SATS(1) = 19000                           PLB00410
SATS(2) = 19000                           PLB00420
SATS(3) = 19000                           PLB00430
SATS(4) = 19000                           PLB00440
SATS(5) = 19000                           PLB00450
SATS(6) = 19000                           PLB00460
SATS(7) = 30000                           PLB00470
LIGHTS(1)=32000                           PLB00480
LIGHTS(2)=28000                           PLB00490
LIGHTS(3)=27000                           PLB00500
LIGHTS(4)=26000                           PLB00510
LIGHTS(5)=25000                           PLB00520
LIGHTS(6)=23000                           PLB00530
LIGHTS(7)=20000                           PLB00540
BX = 0.7                                  PLB00550

```


99 IF(1WR(J),NE,1WR(J+1)) GO TO 200	PLB01110
GO TO 150	PLB01120
200 XX1 = XMIN + (FLOAT(KK-1))ADX	PLB01130
YY1 = YMIN + (FLOAT(I-1))ADY	PLB01140
XX2 = XMIN + OXAELOAT(J)	PLB01150
YY2 = YMIN + OYAELOAT(I)	PLB01160
CALL JRECT(XX1,YY1,XX2,YY2)	PLB01170
KK = J+1	PLB01180
GO TO 100	PLB01190
150 XX1 = XMIN + (FLOAT(KK-1))ADX	PLB01200
YY1 = YMIN + (FLOAT(I-1))ADY	PLB01210
XX2 = XMIN + OXAELOAT(J)	PLB01220
YY2 = YMIN + OYAELOAT(I)	PLB01230
IF(J.LT.99) GO TO 100	PLB01240
CALL JRECT(XX1,YY1,XX2,YY2)	PLB01250
100 CONTINUE	PLB01260
110 CONTINUE	PLB01270
CALL JCOLOR(16)	PLB01280

C DRAW AXES AND BOREHOLES	PLB01290
C	PLB01300
C	PLB01310
CALL JMOVE(XMIN,YMIN)	PLB01320
CALL JDRAW(XMAX,YMIN)	PLB01330
CALL JMOVE(XMIN,YMIN)	PLB01340
CALL JDRAW(XMIN,YMAX)	PLB01350
DO 400 I = 1,10	PLB01360
XL = XMIN + OX * FLOAT(I-1) * 10.0	PLB01370
CALL JMOVE(XL,YMIN)	PLB01380
CALL JDRAW(XL,YMIN-0.5)	PLB01390
CALL JMOVE(XL,YMIN-1.0)	PLB01400
IF(XL.GE.0) GO TO 112	PLB01410
NL = IFIX(XL - 0.5)	PLB01420
GO TO 113	PLB01430
112 NL = IFIX(XL + 0.5)	PLB01440
113 WRITE(61,300) NL	PLB01450
BACKSPACE 61	PLB01460
READ(61,301) XALPHA	PLB01470
301 FORMAT(A4)	PLB01480
CALL JJUST(2,3)	PLB01490
CALL JSIZE(1.0,1.0)	PLB01500
CALL JSSRG(XALPHA)	PLB01510
400 CONTINUE	PLB01520
DO 500 I = 1,10	PLB01530
YL = YMIN + OYAEFLOAT(I-1)*10.0	PLB01540
CALL JMOVE(XMIN,YL)	PLB01550
CALL JDRAW(XMIN-0.5,YL)	PLB01560
CALL JMOVE(XMIN-1.0,YL)	PLB01570
IF(YL.GE.0.0) GO TO 412	PLB01580
NL = IFIX(YL - 0.5)	PLB01590
GO TO 413	PLB01600
412 NL = IFIX(YL + 0.5)	PLB01610
413 WRITE(61,300) NL	PLB01620
300 FORMAT(I4)	PLB01630
BACKSPACE 61	PLB01640
READ(61,301) XALPHA	PLB01650

CALL JJUST(3,2)	PLR01660
CALL JSIZE(1.0,1.0)	PLR01670
CALL J3STRG(XALPHA)	PLR01680
500 CONTINUE	PLR01690
CALL JHARK(3)	PLR01700
DO 600 I = 1,NUMBH	PLR01710
WRITE(61,510) I	PLR01720
510 FORMAT(I2)	PLR01730
BACKSPACE 61	PLR01740
READ(61,520) XALF	PLR01750
520 FORMAT(1A2)	PLR01760
READ(62,670) XX,YY,ZZ	PLR01770
670 FORMAT(3F15.1)	PLR01780
CALL JHARK(XX,YY)	PLR01790
CALL JMOVE(XX+0.5,YY)	PLR01800
CALL JJUST(1,2)	PLR01810
CALL JSIZE(1.0,1.0)	PLR01820
CALL J3STRG(XALF)	PLR01830
600 CONTINUE	PLR01840
READ(51,610) STOPID	PLR01850
610 FORMAT(A32)	PLR01860
CALL JMOVE((XM+XMM)/2.0,YMM-3.0)	PLR01870
CALL JJUST(2,2)	PLR01880
CALL JSIZE(2.0,2.0)	PLR01890
CALL J3STRG(STOPID)	PLR01900
IELEV = IFIX(PLELEV)	PLR01910
WRITE(61,630) IELEV	PLR01920
630 FORMAT(I4)	PLR01930
BACKSPACE 61	PLR01940
READ(61,640) XALPHA	PLR01950
640 FORMAT(A4)	PLR01960
CALL JMOVE((XM+XMM-12.)/2.0,YMM-6.0)	PLR01970
CALL JJUST(2,2)	PLR01980
CALL JSIZE(2.0,2.0)	PLR01990
CALL J3STRG('PLAN ON ELEVATION ')	PLR02000
CALL JMOVE((XM+XMM+36.0)/2.0,YMM-6.0)	PLR02010
CALL JJUST(2,2)	PLR02020
CALL JSIZE(2.0,2.0)	PLR02030
CALL J3STRG(XALPHA)	PLR02040
CALL JMOVE((XM+XMM)/2.0,YM+3.0)	PLR02050
CALL JJUST(2,2)	PLR02060
CALL JSIZE(2.0,2.0)	PLR02070
CALL J3STRG('X AXIS (FT)')	PLR02080
CALL JBASE(0.0,1.0,0.0)	PLR02090
CALL JMOVE(XM+3.0,(YM+YMM)/2.0)	PLR02100
CALL JJUST(2,2)	PLR02110
CALL JSIZE(2.0,2.0)	PLR02120
CALL J3STRG('Y AXIS (FT)')	PLR02130
CALL JCLOSE	PLR02140
CALL JPAUSE(1)	PLR02150
CALL JREVR(1)	PLR02160
CALL JDEND(1)	PLR02170
CALL JEND	PLR02180
STOP	PLR02190
END	PLR02200

APPENDIX B

PROGRAM INPUT DATA

1. LARGE DIAMETER BLASTHOLE BENCHING
METHOD
2. VERTICAL CRATER RETREAT METHOD
3. EXEC FILES FOR THE TWO GRAPHICS
PROGRAMS

1. LARGE DIAMETER BLASTHOLE BENCHING
METHOD

EXEC DISK000 TEK4107
EXEC LINEMODE ON
FILEDEF 07 TERMINAL
FILEDEF 08 DISK BCURV DATA B
FILEDEF 09 DISK BBLAST DATA B
FILEDEF 11 DISK VIBRAT DATA B
FILEDEF 12 DISK TOP DATA B
FILEDEF 51 DISK INCOSTOP DATA B
FILEDEF 61 DISK JUNK DATA B
FILEDEF 66 DISK INC062 DATA B
FILEDEF 70 DISK CHPLOT DATA B
FILEDEF 72 DISK OUTLINE DATA B
FILEDEF 06 DISK FRESULT LISTING B
FILEDEF 62 DISK PCH30 DATA B
EXEC EXECUTE LLL FORT77
EXEC LINEMODE OFF

FILE: EBLAST DATA B

ON/OF CONVERSATIONAL MONITOR SYSTEM

A119

4	
0.0	4.0
12.0	4.0
12.0	50.0
0.0	50.0

8

0.6000	0.1400
0.7100	0.2000
0.8300	0.2200
1.0700	0.2700
1.5900	0.3400
0.8700	0.5000
0.5200	0.4900
0.3600	0.6100

8

2.0000	0.1400
2.0200	0.2000
2.0300	0.2200
2.1300	0.2700
2.5000	0.3400
2.1000	0.5000
1.6700	0.4900
1.5000	0.6100

8

0.6000	0.1400
0.7100	0.2000
0.8300	0.2200
1.0700	0.2700
1.5900	0.3400
0.8700	0.5000
0.5200	0.4900
0.3600	0.6100

8

2.0000	0.1400
2.0200	0.2000
2.0300	0.2200
2.1300	0.2700
2.5000	0.3400
2.1000	0.5000
1.6700	0.4900
1.5000	0.6100

FILE: TOP

DATA

H

VN/SP CONVERSATIONAL MONITOR SYSTEM

A121

1				
40.0	4.0	40.0	60.0	

1	9	1	1	106.00
11340.70		13167.20		9443.98
11340.70		13167.20		9443.98
11340.78		13166.54		9453.96
11340.87		13165.92		9463.93
11341.04		13165.31		9473.91
11341.23		13164.82		9483.89
11341.43		13164.28		9493.87
11341.69		13163.69		9503.85
11341.92		13163.16		9513.83
11342.04		13162.65		9523.00
2	9	1	2	106.00
11331.80		13172.10		9444.03
11331.80		13172.10		9444.03
11331.84		13171.98		9454.03
11331.95		13171.44		9464.02
11332.09		13171.10		9474.01
11332.26		13170.75		9484.00
11332.40		13170.49		9493.99
11332.59		13170.12		9503.98
11332.79		13169.79		9513.97
11332.99		13169.50		9523.00
3	9	1	3	106.00
11323.00		13176.70		9444.00
11323.00		13176.70		9444.00
11323.25		13176.16		9453.98
11323.53		13175.76		9463.96
11323.82		13175.34		9473.95
11324.05		13174.93		9483.94
11324.28		13174.48		9493.92
11324.47		13173.94		9503.90
11324.71		13173.41		9513.88
11324.95		13172.93		9523.00
4	9	1	4	106.00
11315.00		13180.90		9444.63
11315.00		13180.90		9444.63
11315.00		13180.79		9454.62
11315.09		13180.49		9464.62
11315.15		13180.18		9474.61
11315.21		13179.87		9484.60
11315.28		13179.58		9494.59
11315.34		13179.27		9504.59
11315.48		13178.91		9514.58
11315.45		13178.65		9523.00
5	9	2	1	106.00
11344.60		13176.00		9444.63
11344.60		13176.00		9444.63
11344.76		13175.48		9454.61
11344.82		13175.10		9464.61
11344.90		13174.65		9474.59
11344.99		13174.21		9484.58
11345.08		13173.76		9494.57
11345.16		13173.37		9504.56
11345.32		13172.94		9514.55
11345.37		13172.47		9523.00

6	9	2	2	106.00
11337.00	13180.00			9444.63
11337.00	13180.00			9444.63
11337.09	13179.55			9454.62
11337.39	13179.08			9464.60
11337.62	13178.64			9474.59
11337.81	13178.18			9484.57
11337.90	13177.74			9494.56
11338.00	13177.31			9504.55
11338.09	13176.87			9514.54
11338.09	13176.45			9523.00
7	9	2	3	106.00
11327.90	13185.30			9444.63
11327.90	13185.30			9444.63
11328.09	13184.95			9454.62
11328.21	13184.56			9464.61
11328.26	13184.20			9474.60
11328.34	13183.82			9484.59
11328.42	13183.54			9494.58
11328.49	13183.19			9504.57
11328.59	13182.82			9514.57
11328.60	13182.49			9523.00
8	9	2	4	106.00
11319.60	13189.60			9444.63
11319.60	13189.60			9444.63
11319.65	13189.38			9454.62
11319.76	13189.05			9464.62
11319.81	13188.70			9474.61
11319.79	13188.42			9484.61
11319.70	13188.13			9494.60
11319.58	13187.82			9504.59
11319.54	13187.52			9514.58
11319.44	13187.26			9523.00
9	9	3	1	106.00
11349.40	13184.90			9444.63
11349.40	13184.90			9444.63
11349.61	13184.43			9454.61
11349.73	13184.09			9464.61
11349.84	13183.66			9474.59
11349.77	13183.27			9484.58
11349.67	13182.91			9494.57
11349.56	13182.56			9504.57
11349.43	13182.03			9514.55
11349.29	13181.56			9523.00
10	9	3	2	106.00
11341.00	13189.20			9444.63
11341.00	13189.20			9444.63
11341.12	13188.78			9454.62
11341.04	13188.31			9464.61
11340.96	13187.92			9474.59
11340.86	13187.55			9484.59
11340.71	13187.18			9494.57
11340.54	13186.77			9504.56
11340.42	13186.39			9514.55
11340.28	13186.03			9523.00

A124

11	9	3	3	106.00
11333.00	13193.90			9444.63
11333.00	13193.90			9444.63
11333.07	13193.52			9454.62
11332.94	13193.20			9464.61
11332.78	13192.79			9474.60
11332.54	13192.42			9484.59
11332.25	13192.07			9494.58
11332.01	13191.79			9504.57
11331.82	13191.53			9514.56
11331.64	13191.29			9523.00
12	9	3	4	106.00
11326.00	13197.00			9444.63
11326.00	13197.00			9444.63
11326.07	13196.62			9454.62
11325.94	13196.30			9464.61
11325.78	13195.89			9474.60
11325.54	13195.52			9484.59
11325.25	13195.17			9494.58
11325.01	13194.89			9504.57
11324.82	13194.63			9514.56
11324.64	13194.39			9523.00

2. VERTICAL CRATER RETREAT METHOD

*TRACE OFF

CLRSCHN

FILEDEF 07 TERM

FILEDEF 51 DISK INCCOSTOP DATA B

FILEDEF 61 DISK INCO61 DATA B

FILEDEF 62 DISK PCH3 DATA B

FILEDEF 08 DISK CRCURV DATA B

FILEDEF 10 DISK SEQB DATA B

FILEDEF 11 DISK VIBRAT DATA B

FILEDEF 06 DISK PRESULV LISTING B

FILEDEF 70 DISK CHLOC DATA B

FILEDEF 77 DISK PLBLD DATA B

EXEC EXECUTE VCR FORT77 (INCO

FILE: INCOSTOP DATA

B

VM/SP CONVERSATIONAL MONITOR SYSTEM

A127

SAMPLE STOPE FROM INCO

11343.00 13140.00 9444.00

70.00 50.00 200.00

62.50

12

KLF POINT

ST LEN MID DEP

ANGLE XNEW TO EAST

1	20	1	1	106.00
11340.70	13167.20			9443.98
11340.70	13167.20			9443.98
11340.78	13166.54			9453.96
11340.87	13165.92			9463.93
11341.04	13165.31			9473.91
11341.23	13164.82			9483.89
11341.43	13164.28			9493.87
11341.69	13163.69			9503.85
11341.92	13163.16			9513.83
11342.04	13162.65			9523.82
11342.16	13162.11			9533.80
11342.32	13161.55			9543.78
11342.49	13160.98			9553.76
11342.62	13160.46			9563.75
11342.75	13159.91			9573.73
11342.94	13159.35			9583.71
11343.09	13158.81			9593.70
11343.25	13158.35			9603.68
11343.38	13157.82			9613.66
11343.50	13157.51			9618.65
11343.55	13157.30			9624.64
2	10	1	2	106.00
11331.80	13172.10			9444.03
11331.80	13172.10			9444.03
11331.84	13171.88			9454.03
11331.95	13171.44			9464.02
11332.09	13171.10			9474.01
11332.26	13170.75			9484.00
11332.40	13170.48			9493.99
11332.59	13170.12			9503.98
11332.79	13169.79			9513.97
11332.99	13169.50			9523.96
11333.20	13169.18			9533.96
11333.43	13168.85			9543.95
11333.76	13168.59			9553.94
11334.04	13168.30			9563.93
11334.27	13167.97			9573.91
11334.54	13167.70			9583.91
11334.97	13167.43			9593.89
11335.39	13167.13			9603.87
11335.55	13166.96			9624.45
3	16	1	3	106.00
11323.00	13176.70			9444.00
11323.00	13176.70			9444.00
11323.25	13176.16			9453.98
11323.53	13175.76			9463.96
11323.82	13175.34			9473.95
11324.05	13174.93			9483.94
11324.28	13174.48			9493.92
11324.47	13173.94			9503.90
11324.71	13173.41			9513.88
11324.95	13172.93			9523.87
11325.17	13172.43			9533.85
11325.36	13172.00			9543.84

11325.60	13171.54	9553.82
11325.82	13170.95	9563.80
11326.11	13170.94	9573.78
11326.37	13169.75	9583.75
11327.47	13167.58	9624.45
4 19	1 4	106.00
11315.00	13180.90	9444.63
11315.00	13180.90	9444.63
11315.00	13180.79	9454.62
11315.09	13180.49	9464.62
11315.15	13180.18	9474.61
11315.21	13179.87	9484.60
11315.28	13179.58	9494.59
11315.34	13179.27	9504.59
11315.48	13178.91	9514.58
11315.45	13178.65	9524.57
11315.46	13178.34	9534.57
11315.49	13178.02	9544.56
11315.46	13177.73	9554.55
11315.41	13177.36	9564.54
11315.40	13176.98	9574.54
11315.43	13176.59	9584.53
11315.43	13176.24	9594.52
11315.38	13175.86	9604.51
11315.32	13175.51	9614.50
11315.33	13175.14	9624.50
5 19	2 1	106.00
11344.60	13176.00	9444.63
11344.60	13176.00	9444.63
11344.76	13175.48	9454.61
11344.82	13175.10	9464.61
11344.90	13174.65	9474.59
11344.99	13174.21	9484.58
11345.08	13173.76	9494.57
11345.16	13173.37	9504.56
11345.32	13172.94	9514.55
11345.37	13172.47	9524.54
11345.39	13172.00	9534.52
11345.43	13171.60	9544.51
11345.49	13171.14	9554.50
11345.50	13170.72	9564.49
11345.50	13170.18	9574.47
11345.60	13169.68	9584.46
11345.55	13169.23	9594.45
11345.53	13168.67	9604.43
11345.44	13168.30	9614.42
11345.40	13167.70	9624.40
6 19	2 2	106.00
11337.00	13180.00	9444.63
11337.00	13180.00	9444.63
11337.09	13179.55	9454.62
11337.39	13179.08	9464.60
11337.62	13178.64	9474.59
11337.81	13178.18	9484.57
11337.90	13177.74	9494.56

11338.00	13177.31	9504.55
11338.09	13176.87	9514.54
11338.09	13176.45	9524.52
11338.06	13176.09	9534.52
11338.03	13175.69	9544.50
11337.95	13175.24	9554.49
11337.87	13174.71	9564.48
11337.75	13174.09	9574.45
11337.64	13173.54	9584.44
11337.43	13173.00	9594.42
11337.21	13172.36	9604.39
11337.03	13171.75	9614.37
11336.79	13171.04	9624.34
7 19 2 3		106.00
11327.90	13185.30	9444.63
11327.90	13185.30	9444.63
11328.09	13184.95	9454.62
11328.21	13184.56	9464.61
11328.26	13184.20	9474.60
11328.34	13183.82	9484.59
11328.42	13183.54	9494.58
11328.49	13183.19	9504.57
11328.59	13182.82	9514.57
11328.60	13182.49	9524.56
11328.64	13182.20	9534.55
11328.75	13181.72	9544.54
11328.77	13181.42	9554.53
11328.75	13181.04	9564.52
11328.74	13180.56	9574.51
11328.75	13180.09	9584.50
11328.83	13179.61	9594.48
11328.84	13179.22	9604.47
11328.82	13178.78	9614.46
11328.83	13178.26	9624.45
8 19 2 4		106.00
11319.60	13189.60	9444.63
11319.60	13189.60	9444.63
11319.65	13189.38	9454.62
11319.76	13189.05	9464.62
11319.81	13188.70	9474.61
11319.79	13188.42	9484.61
11319.70	13188.13	9494.60
11319.58	13187.82	9504.59
11319.54	13187.52	9514.58
11319.44	13187.26	9524.58
11319.19	13186.86	9534.57
11318.95	13186.51	9544.55
11318.59	13186.10	9554.54
11318.24	13185.67	9564.52
11317.80	13185.22	9574.50
11317.40	13184.75	9584.48
11316.96	13184.33	9594.46
11316.45	13183.80	9604.43
11315.94	13183.32	9614.41
11315.39	13182.86	9624.38

9	19	3	1	106.00
11349.40	13184.90			9444.63
11349.40	13184.90			9444.63
11349.61	13184.43			9454.61
11349.73	13184.09			9464.61
11349.84	13183.66			9474.59
11349.77	13183.27			9484.58
11349.67	13182.91			9494.57
11349.56	13182.56			9504.57
11349.43	13182.03			9514.55
11349.29	13181.56			9524.54
11349.16	13181.18			9534.52
11349.00	13180.86			9544.52
11348.87	13180.43			9554.50
11348.72	13180.02			9564.49
11348.57	13179.70			9574.48
11348.41	13179.25			9584.47
11348.26	13178.89			9594.46
11348.11	13178.41			9604.45
11347.96	13178.05			9614.44
11347.83	13177.60			9624.43
10	19	3	2	106.00
11341.00	13189.20			9444.63
11341.00	13189.20			9444.63
11341.12	13188.78			9454.62
11341.04	13188.31			9464.61
11340.96	13187.92			9474.59
11340.86	13187.55			9484.59
11340.71	13187.18			9494.57
11340.54	13186.77			9504.56
11340.42	13186.39			9514.55
11340.28	13186.03			9524.54
11340.13	13185.65			9534.53
11340.03	13185.30			9544.52
11339.94	13184.90			9554.51
11339.79	13184.49			9564.50
11339.64	13184.15			9574.49
11339.60	13183.77			9584.48
11339.45	13183.45			9594.48
11339.31	13183.03			9604.46
11339.18	13182.69			9614.46
11339.12	13182.32			9624.45
11	19	3	3	106.00
11333.00	13193.90			9444.63
11333.00	13193.90			9444.63
11333.07	13193.52			9454.62
11332.94	13193.20			9464.61
11332.78	13192.79			9474.60
11332.54	13192.42			9484.59
11332.25	13192.07			9494.58
11332.01	13191.79			9504.57
11331.82	13191.53			9514.56
11331.64	13191.29			9524.55
11331.46	13191.08			9534.55
11331.23	13190.88			9544.54

11331.03	13190.59	9554.54
11330.80	13190.37	9564.53
11330.58	13190.20	9574.52
11330.38	13190.00	9584.52
11330.15	13189.80	9594.51
11329.98	13189.60	9604.51
11329.73	13189.47	9614.50
11329.41	13189.29	9624.50
12 19 3 4		106.00
11326.00	13197.00	9444.63
11326.00	13197.00	9444.63
11326.07	13196.62	9454.62
11325.94	13196.30	9464.61
11325.78	13195.89	9474.60
11325.54	13195.52	9484.59
11325.25	13195.17	9494.58
11325.01	13194.89	9504.57
11324.82	13194.63	9514.56
11324.64	13194.39	9524.55
11324.46	13194.18	9534.55
11324.23	13193.98	9544.54
11324.03	13193.70	9554.54
11323.90	13193.47	9564.53
11323.58	13193.30	9574.52
11323.38	13193.10	9584.52
11323.15	13192.91	9594.51
11322.98	13192.70	9604.51
11322.73	13192.57	9614.50
11322.41	13192.39	9624.50

8	
0.6000	0.1400
0.7100	0.2000
0.8300	0.2200
1.0700	0.2700
1.5900	0.3400
0.8700	0.5000
0.5200	0.4900
0.3600	0.6100
8	
2.0000	0.1400
2.0200	0.2000
2.0300	0.2200
2.1300	0.2700
2.5000	0.3400
2.1000	0.5000
1.6700	0.4900
1.5000	0.6100

3. EXEC FILES FOR THE TWO GRAPHICS
PROGRAMS

FILEDEF 07 TERMINAL
FILEDEF 77 DISK PLBLD DATA B
FILEDEF 61 DISK TEMF1 DATA B
FILEDEF 62 DISK BLAST DATA B
FILEDEF 51 DISK INCUSTOP DATA B
GLOBAL TXLIB
EXEC LINEMODE ON
EXEC D13000 TEK4107
LOAD PLBLAST (START NUNAP CLEAR NOAUDIO
EXEC LINEMODE OFF

FILE: GRAPH EXEC B

V6/SP CONVERSATIONAL MONITOR SYSTEM

A136

EXEC DI3000 TEK4107
EXEC LINEMODE ON
FILEDEF 05 TERM
FILEDEF 06 TERM
FILEDEF 51 DISK INCUSTOP DATA B
FILEDEF 61 DISK INC062 DATA B
FILEDEF 62 DISK PCH3 DATA B
FILEDEF 92 DISK P92 DATA B
EXEC EXECUTE PGRAPH FORT77 (INC77
EXEC LINEMODE OFF
AERASE P92 DATA B
8EXIT

APPENDIX C

PROGRAM OUTPUT FOR

1. LARGE DIAMETER BLASTHOLE BENCHING
METHOD
2. VERTICAL CRATER RETREAT METHOD

1. LARGE DIAMETER BLASTHOLE BENCHING
METHOD

P R O G R A M L D B B

WRITTEN FOR THE DESIGN OF THE
BLAST IN AN UNDERGROUND STOPE
USING THE LARGE DIAMETER
BLASTHOLE BENCHING METHOD

SAMPLE STOPE

EXPLOSIVE USED : AQUAMEX

DENSITY : 0.0540 LBS/CUB. INCH

DIAMETER : 6.5000 INCHES

INITIATION SEQUENCE IN LEVEL # 1

HOLE NUMBER

DELAY PERIOD

1	1
2	2
3	3
4	4
5	5
6	4
7	5
8	6
9	7
10	6
11	7
12	8

WEIGHT OF EXPLOSIVE DECKS IN LEVEL 4 1

HOLE NUMBER -----	WEIGHT (LBS) -----
1	122.
2	122.
3	122.
4	122.
5	122.
6	122.
7	146.
8	122.
9	122.
10	122.
11	122.
12	122.

INITIATION SEQUENCE IN LEVEL # 2
-----HOLE NUMBER
-----DELAY PERIOD

1	3
2	4
3	5
4	6
5	7
6	6
7	7
8	8
9	9
10	8
11	9
12	10

WEIGHT OF EXPLOSIVE DECKS IN LEVEL # 2

HOLE NUMBER -----	WEIGHT (LBS) -----
1	122.
2	122.
3	122.
4	122.
5	122.
6	122.
7	146.
8	122.
9	122.
10	122.
11	122.
12	122.



INITIATION SEQUENCE IN LEVEL # 3HOLE NUMBERDELAY PERIOD

1	5
2	6
3	7
4	8
5	9
6	8
7	9
8	10
9	11
10	10
11	11
12	12

WEIGHT OF EXPLOSIVE DECKS IN LEVEL # 3
-----HOLE NUMBER
-----WEIGHT (LBS)

1	122.
2	122.
3	122.
4	122.
5	122.
6	122.
7	146.
8	122.
9	122.
10	122.
11	122.
12	122.

A149



INITIATION SEQUENCE IN LEVEL # 4
-----HOLE NUMBER
-----DELAY PERIOD

1	7
2	8
3	9
4	10
5	11
6	10
7	11
8	12
9	13
10	12
11	13
12	14

WEIGHT OF EXPLOSIVE DECKS IN LEVEL # 4

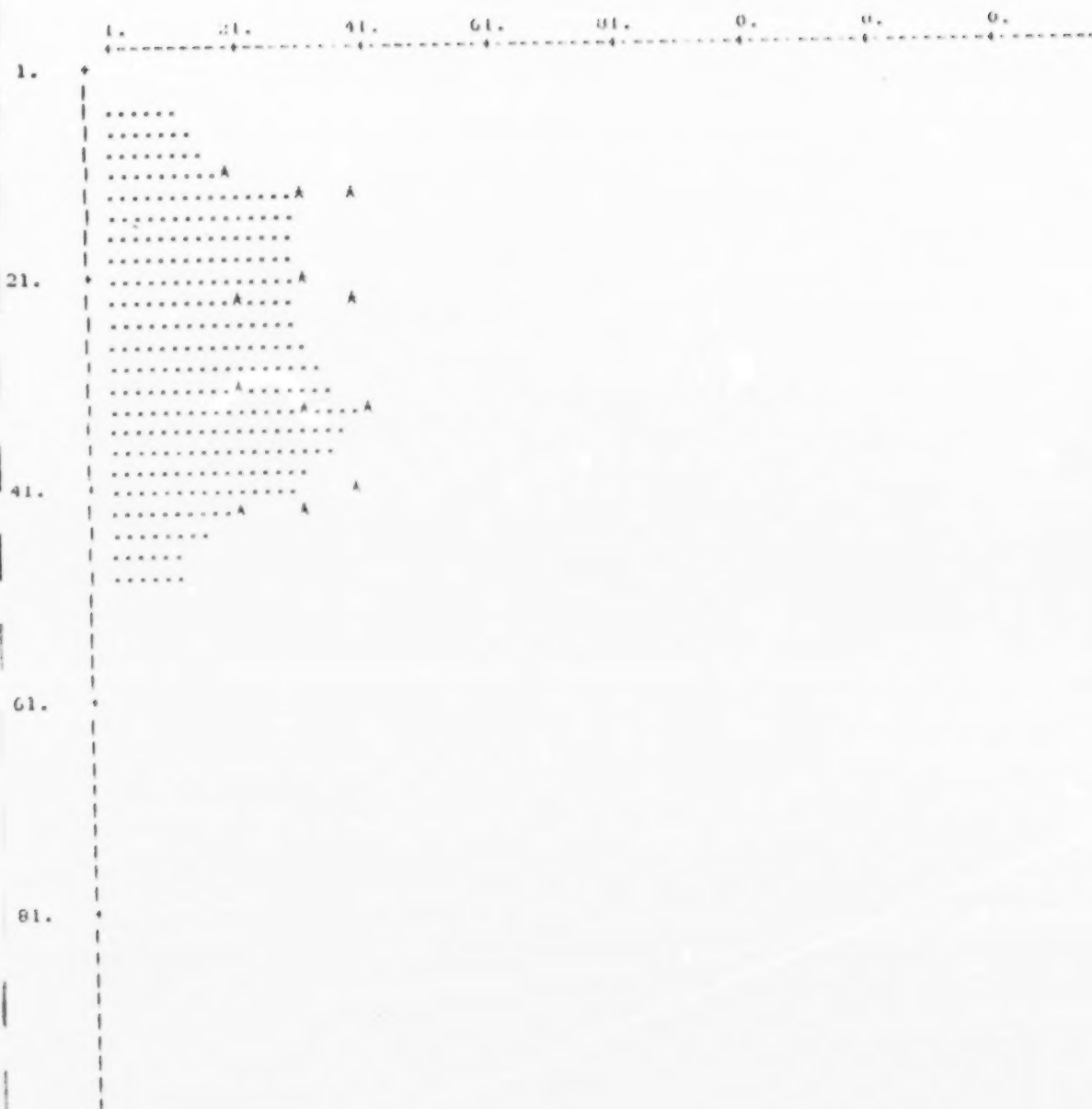
<u>HOLE NUMBER</u>	<u>WEIGHT (LBS)</u>
1	122.
2	122.
3	122.
4	122.
5	122.
6	122.
7	146.
8	122.
9	122.
10	122.
11	122.
12	122.

INITIATION SEQUENCE IN LEVEL # 5
-----HOLE NUMBER
-----DELAY PERIOD

1	9
2	10
3	11
4	12
5	13
6	12
7	13
8	14
9	15
10	14
11	15
12	16

WEIGHT OF EXPLOSIVE DECKS IN LEVEL # 5
-----HOLE NUMBER
-----WEIGHT (LBS)

1	122.
2	122.
3	122.
4	122.
5	122.
6	146.
7	126.
8	105.
9	0.
10	0.
11	146.
12	0.



SUMMARY

A156

TOTAL WEIGHT OF EXPLOSIVE : 7066. LBS

DELAY NUMBER

QUANTITY

1	1
2	1
3	2
4	3
5	4
6	5
7	6
8	6
9	6
10	6
11	5
12	5
13	4
14	3
15	2
16	1

INSTRUCTIONS FOR LOADING

A157

HOLE NUMBER	CHARGE LOCATION	CHARGE WEIGHT	DELAY NUMBER
1	79.	122.	1
	64.	122.	3
	49.	122.	5
	33.	122.	7
	19.	122.	9
2	79.	122.	2
	64.	122.	4
	48.	122.	6
	33.	122.	8
	18.	122.	10
3	79.	122.	3
	64.	122.	5
	48.	122.	7
	33.	122.	9
	18.	122.	11
4	79.	122.	4
	63.	122.	6
	48.	122.	8
	33.	122.	10
	17.	122.	12
5	79.	122.	5
	63.	122.	7
	48.	122.	9
	33.	122.	11
	17.	122.	13
6	79.	122.	4
	63.	122.	6
	48.	122.	8
	33.	122.	10
	18.	146.	12
7	79.	146.	5
	64.	146.	7
	48.	146.	9
	33.	146.	11
	18.	126.	13
8	79.	122.	6
	63.	122.	8
	48.	122.	10

6	17.	122.	13	A158
	78.	122.	4	
	63.	122.	6	
	48.	122.	8	
	33.	122.	10	
7	18.	146.	12	
	79.	146.	5	
	64.	146.	7	
	48.	146.	9	
	33.	146.	11	
8	18.	126.	13	
	78.	122.	6	
	63.	122.	8	
	48.	122.	10	
	33.	122.	12	
9	17.	105.	14	
	78.	122.	7	
	63.	122.	9	
	48.	122.	11	
	33.	122.	13	
10	15.	0.	15	
	78.	122.	6	
	63.	122.	8	
	48.	122.	10	
	33.	122.	12	
11	15.	0.	14	
	78.	122.	7	
	63.	122.	9	
	48.	122.	11	
	33.	122.	13	
12	18.	146.	15	
	78.	122.	8	
	63.	122.	10	
	48.	122.	12	
	33.	122.	14	
	15.	0.	16	

2. VERTICAL CRATER RETREAT METHOD

P R O G R A M V C R M

WRITTEN FOR THE DESIGN OF THE
BLAST IN AN UNDERGROUND STOPE
USING THE VERTICAL CRATER
RETREAT METHOD.

TITLE

DATE : 11/02/84

TIME : 16:16:25

EXPLOSIVE USED :Q

DENSITY :0.0540 LBS/CUB. INCH

DIAMETER :6.5000 INCHES

MODIFIED INITIATION SEQUENCE
-----HOLE NUMBER
-----DELAY PERIOD

1	1
2	2
3	3
4	5
5	2
6	3
7	5
8	6
9	2
10	4
11	4
12	6

WEIGHT OF CHARGES IN THE BLAST

A163

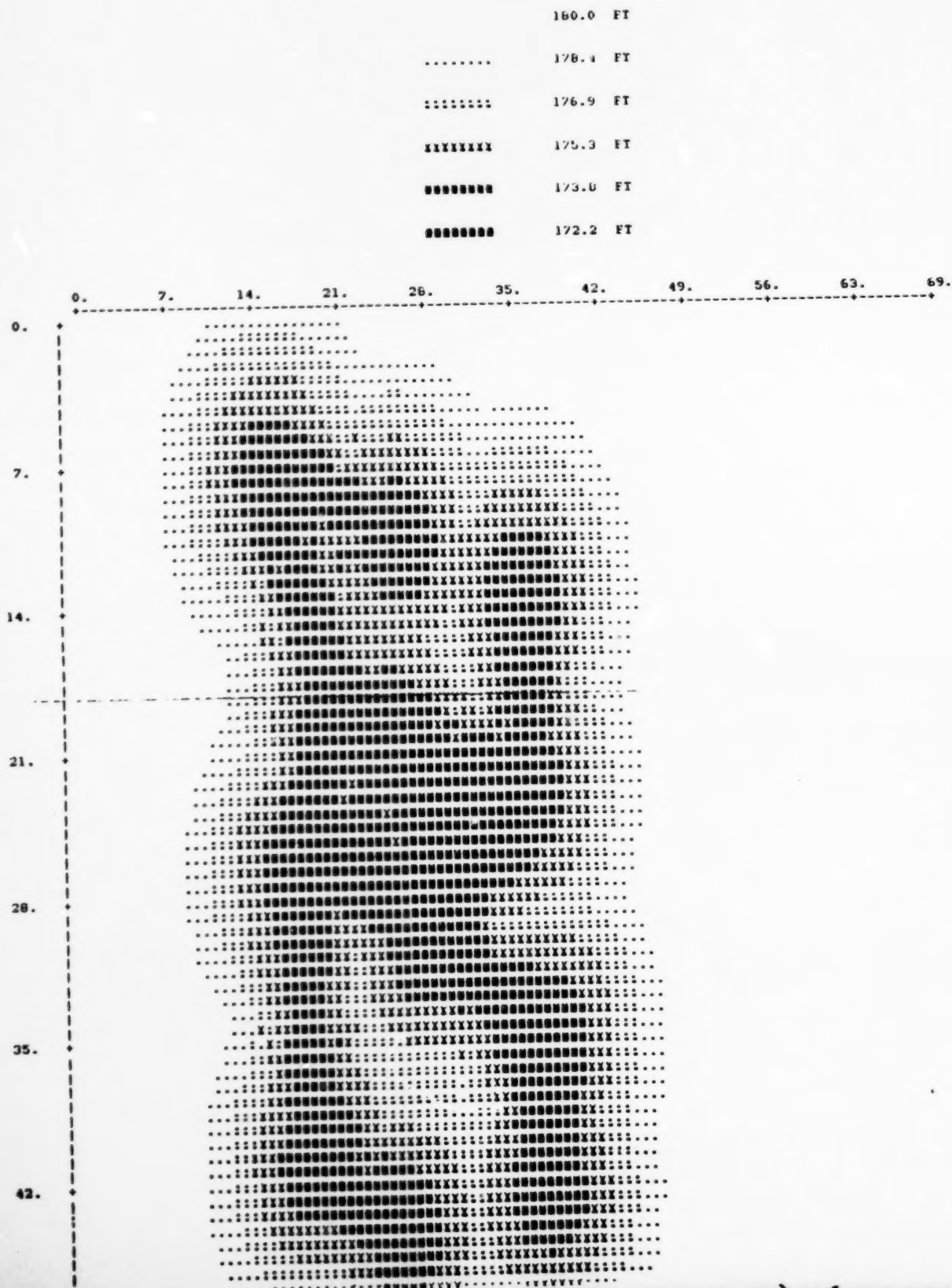
HOLE NUMBER

WEIGHT (LBS)

1	70.
2	70.
3	70.
4	70.
5	70.
6	70.
7	70.
8	70.
9	70.
10	70.
11	70.
12	70.

PLAN VIEW OF THE BLAST

ELEVATIONS REPRESENTED BY THE PRINTOUT



14.

21.

28.

35.

42.

49.

56.

PLAN VIEW OF THE BLAST

ELEVATIONS REPRESENTED BY THE NUMBERS OF THE PRINTOUT

NUMBER 0	180.0	FT
NUMBER 1	178.4	FT
NUMBER 2	176.9	FT
NUMBER 3	175.3	FT
NUMBER 4	173.8	FT
NUMBER 5	172.2	FT

[illegible]

SUMMARY

TOTAL WEIGHT OF EXPLOSIVE : 839.

DELAY NUMBERQUANTITY

1	1
2	3
3	2
4	2
5	2
6	2

INSTRUCTIONS FOR LOADING

A169

HOLE NUMBER	CHARGE LOCATION	CHARGE WEIGHT	DELAY NUMBER
1	174.	70.	1
2	174.	70.	2
3	174.	70.	3
4	173.	70.	5
5	173.	70.	2
6	173.	70.	3
7	173.	70.	5
8	173.	70.	6
9	173.	70.	2
10	173.	70.	4
11	173.	70.	4
12	173.	70.	6

**POOR
QUALITY
ORIGINAL**